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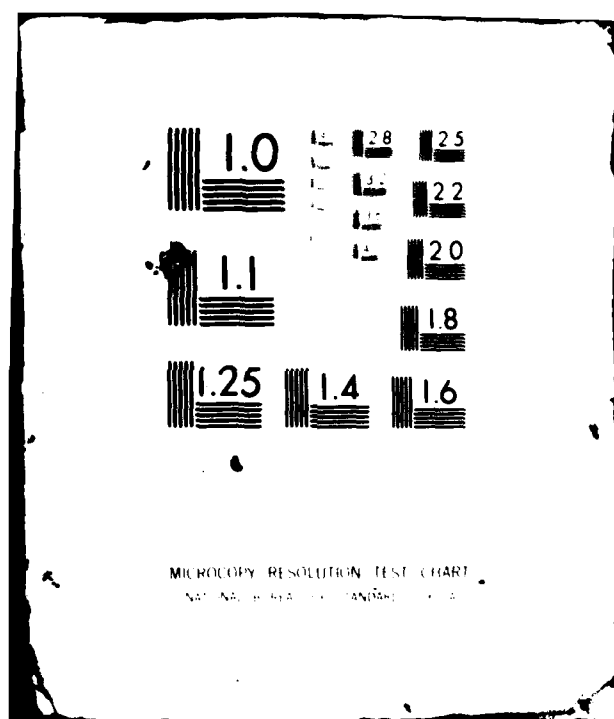
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NRL Report 3323

**NRL 324-m<sup>3</sup> Chamber Pressurization Experiment:  
Pressurant Concentration Histories With and  
Without Obstacles to Flow**

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March 15, 1982



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# **NRL 324-m<sup>3</sup> CHAMBER PRESSURIZATION EXPERIMENT: PRESSURANT CONCENTRATION HISTORIES WITH AND WITHOUT OBSTACLES TO FLOW**

## **INTRODUCTION**

Gas-mixing and scale-modeling studies continue in the new 324-m<sup>3</sup> fire-test facility at the Naval Research Laboratory (NRL). These studies extend previous studies conducted in the NRL 5-m<sup>3</sup> chamber and in its one-sixth-scale model at the University of Washington (UW). We explore further the concept of suppressing unwanted fires in pressurizable spaces by injection of nitrogen gas as proposed by Carhart and Fielding [1]. The chamber of this new facility is of sufficient size to allow realistic full-scale tests. Objectives of these tests were to place the new facility in operation, to infer pressurant gas-concentration histories from temperature (thermocouple) measurements during chamber pressurization from 1 to 2 atmospheres (101.3 to 202.6 kPa), and to present results in a convenient form consistent with the Corlett et al. scale-modeling hypothesis [2].

In this report, we describe the 324-m<sup>3</sup> chamber, its nitrogen pressure system, and experiments both with and without obstacles to flow, and we then present the reduced data.

## **DESCRIPTION OF EQUIPMENT**

Figure 1 shows a view of the 324-m<sup>3</sup> facility as one looks to the southwest. The steel pressure vessel lies horizontally on two concrete piers; design pressure is 5 atmospheres (507 kPa) according to the ASME Unfired Pressure Vessel Code. The chamber was tested hydrostatically at 7.65 atmospheres (775 kPa); 324.2 m<sup>3</sup> of water filled the vessel. Its inside diameter is 5.85 m and its length is 14.82 m. The cylindrical section is 8.35 m long. Installed in the center of the north hemispherical end is a 457-mm-diameter pressure-relief device. The disk design rupture pressure is 5 atmospheres for temperatures to 260°C. A catwalk attaches around the vessel on all sides but the north, providing convenient access to the seven viewports, three on the east and four on the west. Above these viewports, four nitrogen pressure cylinders are mounted symmetrically. Each cylinder is 8.534 m long and each has a 0.610-m diameter. Each has a volume of 2.088 m<sup>3</sup> and a design pressure of 122 atmospheres (12.36 MPa). A nitrogen tube trailer shown in the right foreground of Fig. 1 supplies nitrogen gas, beginning at 233 atmospheres (23.61 MPa), to the four pressure cylinders, which normally are charged to 100 atmospheres (10.13 MPa). Just west of the chamber, and behind the tube trailer, the instrument trailer appears. It houses all instruments, data collection devices, and control devices. Facing the instrument trailer, but not visible in Fig. 1, is a walk-in hatch, centered in the west side of the chamber, which provides chamber access.

### **Nitrogen Pressurization System**

Figure 2 is a schematic of the high-pressure piping system typical of each nitrogen pressure cylinder. For convenience, only one pressure cylinder and the north manifold are shown. Both cylinders on the west side connect to the north manifold, while the two cylinders on the east side connect to the south manifold. Flow is controlled from either or both ends of a cylinder to its manifold by a manual valve and an actuated 2-in. (5-cm) valve in series. Four pipes from each manifold extend into the chamber, so that a nozzle exit is located 1.170 m from the top inside surface of the chamber



Fig. 1 — The NRL 324-m<sup>3</sup> fire chamber facility

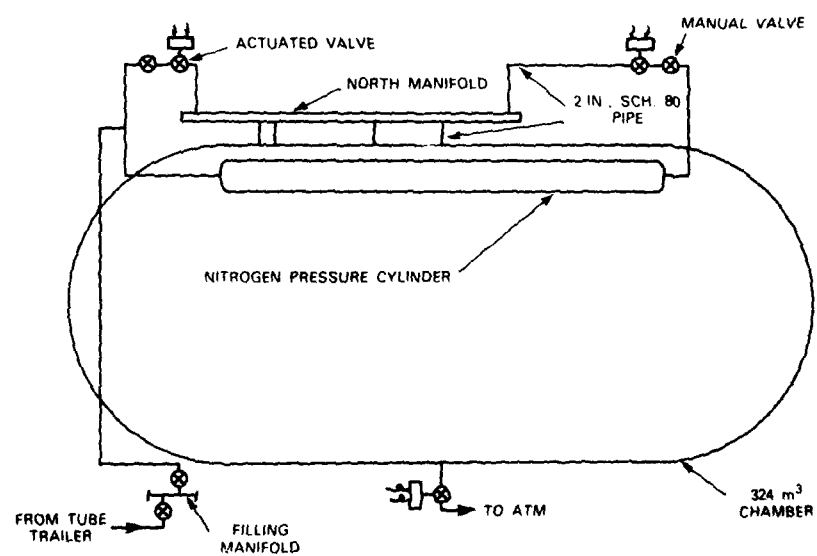


Fig. 2 — Typical high-pressure piping for each of the four nitrogen pressure cylinders

and is directed vertically downward on a line normal to the chamber axis. The four pipes from each manifold are located along the chamber length so that either a three-nozzle or a four-nozzle array (equally spaced) can be selected. Pipe extensions without nozzles are capped. The high-pressure steel pipe is 2-in. (5-cm), schedule 80. Nozzle flow calibration is possible since an ASTM, thin-plate, square-edged orifice [3] connects between the north and south manifold.

### Nozzles

Figure 3 shows a nozzle assembly view. Nozzles connect to the 2-in. pipe extensions. The high-density polyethylene liner minimizes heat flow to the nitrogen gas stream and thus maximizes the temperature difference between the injected pressurant gas and the chamber resident gas. In this system flow in each nozzle throat remains critical [4] during chamber pressurization.

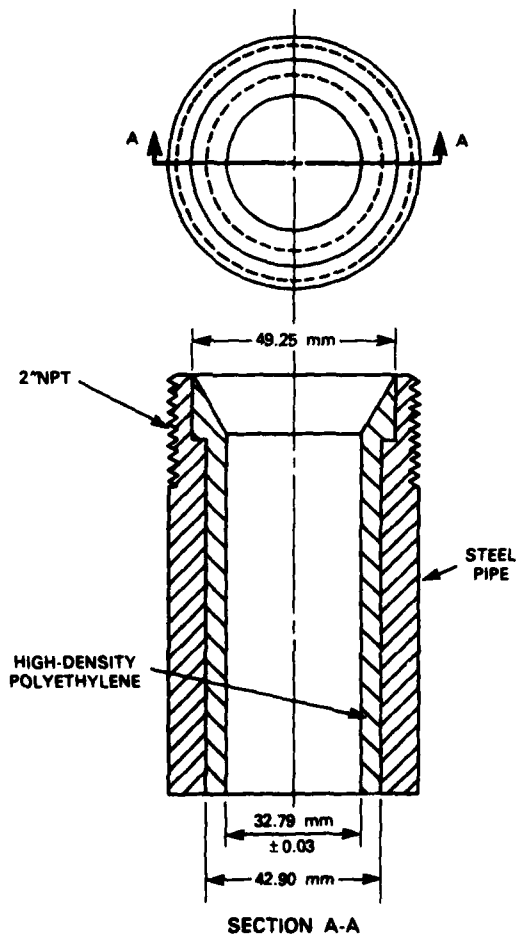


Fig. 3 - Sectional view of nozzle assembly



### Thermocouple and Nozzle Locations

In Fig. 4, we show the two positions of the 13-thermocouple array. Position 2 is along the chamber centerline, while position 1 is displaced laterally 0.6 of the distance to the chamber wall and is in the upper northwest quadrant of the chamber. If the  $z = 0$  plane bisects the chamber normal to its axis and positive  $z$ -values are to the north and negative ones to the south, then the cylindrical  $r$ - and  $\theta$ -coordinates for position 2 are 0.000 m and  $0^\circ$ , respectively; for position 1 they are 2.017 m and  $45^\circ$ , respectively. The  $z$ -coordinates for each of the 13 thermocouples remain the same for both positions, i.e.,  $z = z_l$ , where  $l = 1, \dots, 13$ , and the 13  $z$ -coordinates are, respectively,  $-0.586$ ,  $-0.293$ ,  $0.000$ ,  $0.293$ ,  $0.586$ ,  $0.878$ ,  $2.049$ ,  $2.342$ ,  $2.635$ ,  $2.928$ ,  $3.220$ ,  $3.513$ , and  $3.806$  m. The thermocouples are bare-wire chromel-alumel, 0.10 mm in diameter, with time constants of less than 0.2 s.

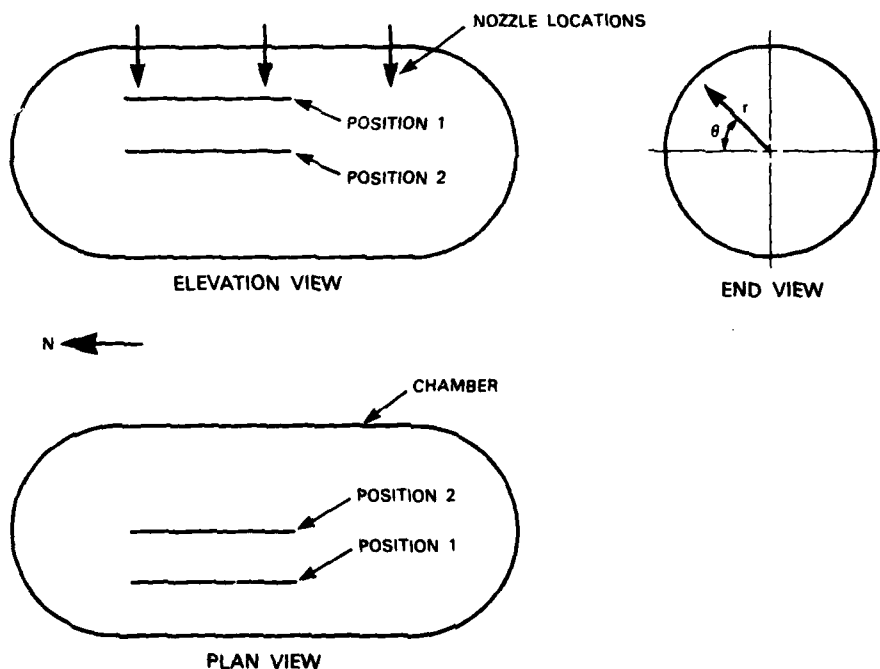


Fig. 4 — Schematic showing the two positions inside the chamber of the 13-thermocouple array: position 1 is off center; position 2 is along the chamber centerline. Three nozzle locations are also shown.

When three nozzles are used, they are located in the three vertical planes  $z = +1.216$ ,  $0.0$ , and  $-1.216$  m, with nozzle exits directed downward normal to the chamber axis and positioned 1.170 m below the top of the chamber wall. The south nozzle is in the plane  $z = -1.216$  m.

### Flow Obstacle

Figure 5 is a plan-view sketch that shows the location of the flow obstacle in the chamber. The obstacle is a metal cabinet, 1.216 m wide by 1.216 m deep by 2.667 m high, with the top, bottom, and three sides closed. The fourth side is covered with a screen wire that has 15 openings per 25.4 mm with 0.25 mm wire diameter; the screen side is shown in Fig. 5 facing to the west. In the experiments, it also faced to the north. The top of the cabinet extends 0.686 m above the chamber centerline, along which the 13 thermocouples are positioned.

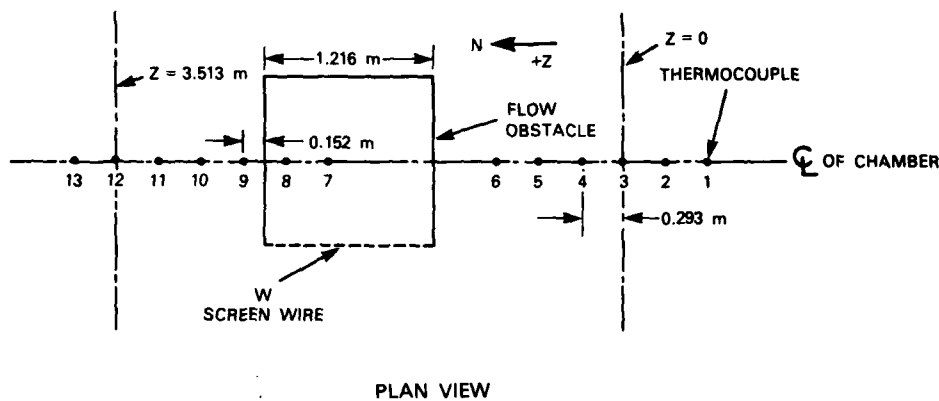


Fig. 5 — Plan-view schematic of chamber interior giving obstacle location and thermocouple / locations for position 2 relative to the vertical plane  $z = 0$

## EXPERIMENTAL PROCEDURE

The procedure used for experiments without the flow obstacle (uncluttered) and the procedure used with the flow obstacle (cluttered) are described as follows.

### Without Flow Obstacle (Uncluttered)

The same procedure was repeated in each of two sets of runs with no flow obstacle. There were seven replicate runs in set 1 and four in set 2 (see Table 1). For set 1, the thermocouple array was in position 1; for set 2, it was in position 2. Three pressure cylinders charged to about 100 atmospheres were used in each set. The two west cylinders fed nitrogen gas to the north manifold, and one east cylinder fed the south manifold. Flow was from both ends of each cylinder. The north manifold fed two nozzles (north and center) while the south fed the third (south). The  $z$ -coordinates for the north, center, and south nozzles were 3.513, 0.000, and  $-3.413$  m, respectively.

Table 1 — Description of Experiments

Experimental Set Number	Scaling Run Numbers	Number of Runs	Thermocouple Position Number	Nozzles Used	Clutter Condition	Obstacle Screen Position	Numbers of A- and B-Tables
1	230-236	7	1	3	Unclut.	—	2-8
2	237-240	4	2	3	Unclut.	—	9-12
3	241-244	4	2	1 (South)	Cluttered	West	13-16
4	245-248	4	2	1 (South)	Cluttered	North	17-20

Data collection was started 30 s prior to the start of a run. A run was started by the simultaneous opening of the appropriate six activated valves. Nitrogen gas flowed into the chamber until its pressure increased from 1 to 2 atmospheres, requiring about 12 s. The valves were then closed. Data collection continued for a total of 300 s. Seventeen channels of data were recorded by two data loggers (Doric-Digitrend 200) as follows:

- 13 channels for the thermocouple array,
- 2 channels for pressurant gas supply temperatures,

- 1 channel for chamber pressure, and
- 1 channel for nitrogen cylinder pressures.

Data loggers scanned each channel twice per second. Loggers were controlled in parallel so that each agreed in time.

#### **With Flow Obstacle (Cluttered)**

Two sets (3 and 4), of four replicate runs each, were made with an obstacle (see Table 1). The same procedure was used as described above, with the following exceptions. The thermocouple array was used only in position 1 and only the south nozzle was used. The south manifold was fed nitrogen by three pressure cylinders, the two east cylinders and one west cylinder. The chamber was pressurized to 2 atmospheres in about 30 s. For set 3, the screened side of the obstacle faced west; for set 4, it faced north.

### **EXPERIMENTAL RESULTS**

Detailed data for the four sets of experiments listed in Table 1 are presented in a comprehensive series of five tables, A, B, C, D, and E. The information found in each comprehensive table is described below prior to discussion of the data.

#### **A-Tables**

Tables 2A to 20A, called A-tables, present temperature histories at 1-s intervals, as determined by the 13-thermocouple array at each *I*-Location, 1 through 13. Interior chamber coordinates of each *I*-location are given by the subtable located in the upper right-hand corner of the A-tables. In addition, the first four columns in the A-tables, respectively, give:

- (1) Time in seconds with  $t = 0$  corresponding to the time the activated-valve switch is thrown to open.
- (2) Nitrogen pressure cylinder pressures in atmospheres.
- (3) Pressurant gas supply temperature at nozzle exit in K.
- (4) Chamber pressure in atmospheres.

Each A-table is programmatically produced (see Appendix A) from the two magnetic data tapes obtained during the experimental run. Accordingly, A-tables are produced for all the runs in each set.

Table 2A — Scaling Run 230: Uncluttered 324-m<sup>3</sup> Chamber, Three 3.279-cm Nozzles

Time t (s)	Press Cyl P (atm)	T <sub>c</sub> (K)	Chamber P (atm)	Chamber Absolute Temperatures (K) at Locations /													COORDINATES		
				1	2	3	4	5	6	7	8	9	10	11	12	13	I	R (M)	THETA (DEC) (°)
-3	0.002	0.002	0.002	285.2	284.0	283.9	285.0	285.0	285.1	283.2	283.2	284.2	284.2	284.2	284.2	283.2	1	1.756	45 -0.586
-4	0.002	0.002	0.002	285.2	284.0	283.9	285.0	285.0	285.1	283.2	283.2	284.2	284.2	284.2	284.2	283.2	2	1.756	45 -0.293
-3	0.002	0.002	0.002	285.2	284.0	283.9	285.0	285.0	285.1	283.2	283.2	284.2	284.2	284.2	284.2	283.2	3	1.756	45 0.000
-2	0.002	0.002	0.002	285.2	284.0	283.9	285.0	285.0	285.1	283.2	283.2	284.2	284.2	284.2	284.2	283.2	4	1.756	45 0.293
-1	0.002	0.002	0.002	285.2	284.0	283.9	285.0	285.0	285.1	283.2	283.2	284.2	284.2	284.2	284.2	283.2	5	1.756	45 0.586
0	1.035	1.035	1.035	292.9	290.6	289.2	291.2	292.4	293.6	285.7	287.2	288.2	287.2	288.2	287.2	286.7	6	1.756	45 0.878
1	1.185	1.185	1.185	298.4	296.3	295.7	297.5	298.5	299.6	291.2	292.2	294.2	293.2	294.2	293.2	293.2	7	1.756	45 2.049
2	1.304	1.304	1.304	301.5	299.5	299.4	300.8	301.5	301.9	296.2	296.2	297.2	296.7	297.2	297.2	297.2	8	1.756	45 2.342
3	1.413	1.413	1.413	303.5	301.3	301.6	302.6	303.1	302.7	299.2	299.2	300.2	300.2	300.2	299.2	299.2	9	1.756	45 2.635
4	1.509	1.509	1.509	303.9	302.8	302.4	303.7	304.0	304.1	300.2	300.7	301.7	301.7	302.2	301.2	301.2	10	1.756	45 2.928
5	1.597	1.597	1.597	305.1	303.5	303.6	304.5	304.9	304.9	303.2	303.2	303.2	303.2	303.2	303.2	302.2	11	1.756	45 3.220
6	1.678	1.678	1.678	305.5	305.0	304.8	305.5	305.4	305.4	303.2	303.2	303.2	303.2	303.2	303.2	303.2	12	1.756	45 3.513
7	1.753	1.753	1.753	305.8	304.5	304.7	305.3	305.2	305.4	303.2	303.2	304.2	304.2	304.2	304.2	303.2	13	1.756	45 3.806
8	1.798	1.798	1.798	306.2	304.7	304.9	305.3	305.3	305.3	303.2	303.2	304.2	304.2	304.2	304.2	303.2			
9	1.863	1.863	1.863	306.2	304.7	304.3	305.7	305.6	305.5	303.7	302.7	304.2	304.2	304.2	304.2	303.2			
10	1.922	1.922	1.922	305.5	304.5	304.5	305.4	304.9	304.9	303.2	303.2	304.2	304.2	304.2	304.2	304.2			
11	1.966	1.966	1.966	304.8	303.4	303.7	304.5	304.2	304.4	301.7	301.7	302.7	302.7	302.7	302.7	302.7			
12	1.976	1.976	1.976	303.5	301.9	302.1	303.0	302.8	302.8	301.2	301.2	302.2	302.2	302.2	302.2	302.2			
13	1.975	1.975	1.975	302.5	300.9	300.9	302.1	302.0	302.0	300.2	300.2	302.2	302.2	302.2	302.2	302.2			
14	1.973	1.973	1.973	302.4	301.0	301.0	302.2	301.7	302.0	300.2	300.2	301.2	301.2	301.2	301.2	301.2			
15	1.971	1.971	1.971	302.3	300.9	300.9	301.8	301.4	301.6	300.2	300.2	301.2	301.2	301.2	301.2	301.2			
16	1.970	1.970	1.970	301.7	300.2	300.4	301.4	301.2	301.2	300.2	300.2	301.2	301.2	301.2	301.2	301.2			
17	1.969	1.969	1.969	301.0	300.0	300.0	301.0	300.6	300.9	300.2	300.2	301.2	301.2	301.2	301.2	301.2			
18	1.967	1.967	1.967	300.9	299.7	299.9	301.0	300.6	300.1	299.2	299.2	300.2	300.2	300.2	300.2	300.2			
19	1.966	1.966	1.966	300.2	299.3	299.2	300.2	300.2	299.8	298.2	299.2	300.2	300.2	301.2	300.2	300.2			
20	1.965	1.965	1.965	299.8	298.6	298.4	299.3	299.6	299.3	299.2	299.2	299.2	299.2	299.2	299.2	299.2			
21	1.960	1.960	1.960	299.2	298.0	298.2	299.5	299.5	299.5	297.2	297.2	299.2	299.2	299.2	299.2	298.2			
22	1.956	1.956	1.956	299.1	298.0	298.0	299.0	298.9	298.9	297.2	297.2	298.2	298.2	299.2	299.2	298.2			
23	1.953	1.953	1.953	298.7	297.5	297.5	298.5	298.5	298.7	297.2	297.2	299.2	299.2	299.2	299.2	298.2			
24	1.950	1.950	1.950	298.1	296.9	297.3	298.2	298.2	298.4	297.2	297.2	298.7	298.7	299.2	299.2	298.2			
25	1.945	1.945	1.945	297.7	296.8	297.0	298.0	298.0	298.1	297.2	297.2	298.2	298.2	298.2	298.2	297.2			
26	1.942	1.942	1.942	297.7	296.8	296.5	297.7	297.7	297.8	296.2	296.2	297.2	297.2	298.2	298.2	297.2			
27	1.940	1.940	1.940	297.8	296.7	296.0	297.3	297.4	297.5	296.2	296.2	297.2	297.2	298.2	298.2	297.2			
28	1.938	1.938	1.938	297.7	296.4	296.1	296.7	297.2	296.9	296.2	296.2	297.2	297.2	298.2	298.2	297.2			
29	1.936	1.936	1.936	297.4	296.1	295.4	296.8	296.9	296.9	296.2	296.2	297.2	297.2	298.2	298.2	297.2			
30	1.933	1.933	1.933	296.7	295.2	295.1	296.2	296.2	296.4	295.2	295.2	296.2	296.2	296.2	296.2	295.2			
31	1.931	1.931	1.931	295.7	294.6	294.5	295.6	295.6	295.6	294.2	294.2	295.2	295.2	295.2	295.2	294.2			
32	1.929	1.929	1.929	296.0	294.7	294.6	295.6	295.7	295.7	294.2	294.2	295.2	295.2	295.2	295.2	294.2			
33	1.927	1.927	1.927	295.9	294.6	294.6	295.5	295.5	295.5	294.2	294.2	295.2	295.2	295.2	295.2	294.2			
34	1.925	1.925	1.925	295.7	294.4	294.5	295.5	295.5	295.5	294.2	294.2	295.2	295.2	295.2	295.2	294.2			
35	1.923	1.923	1.923	295.4	294.2	294.3	295.3	295.3	295.3	294.2	294.2	295.2	295.2	295.2	295.2	294.2			
36	1.921	1.921	1.921	295.1	293.9	294.0	295.2	295.2	295.2	294.2	294.2	295.2	295.2	295.2	295.2	294.2			
37	1.920	1.920	1.920	295.0	293.8	293.9	294.8	294.8	294.8	293.2	293.2	294.2	294.2	294.2	294.2	293.2			
38	1.918	1.918	1.918	294.8	293.5	293.4	294.3	294.3	294.3	293.2	293.2	294.2	294.2	294.2	294.2	293.2			
39	1.917	1.917	1.917	294.2	293.1	293.2	294.2	294.2	294.2	293.2	293.2	294.2	294.2	294.2	294.2	293.2			
40	1.915	1.915	1.915	294.3	292.9	293.2	294.1	294.1	294.1	292.2	292.2	293.2	293.2	293.2	293.2	292.2			
41	1.914	1.914	1.914	294.1	292.8	292.9	293.9	293.9	293.9	292.2	292.2	293.2	293.2	293.2	293.2	292.2			
42	1.913	1.913	1.913	293.8	292.8	292.8	293.7	293.7	293.7	292.2	292.2	293.2	293.2	293.2	293.2	292.2			

Table 3A — Scaling Run 231: Unclogged 324-m<sup>3</sup> Chamber, Three 3.279-cm Nozzles

Time (s)	Press Cyl P (atm)	T <sub>i</sub> (K)	Chamber P (atm)	Chamber Absolute Temperatures (K) at Locations 1													COORDINATES	
				1	2	3	4	5	6	7	8	9	10	11	12	13	R (m)	Theta (deg)
-3	0.003	0.003	0.003	286.5	285.6	285.6	286.5	286.4	286.5	286.2	286.2	287.2	287.2	287.2	286.2	286.2	1	1.756
-4	0.003	0.003	0.003	286.6	285.6	285.6	286.5	286.5	286.5	286.2	286.2	287.2	287.2	287.2	286.2	286.2	2	1.756
-3	0.003	0.003	0.003	286.5	285.6	285.6	286.5	286.5	286.5	286.2	286.2	287.2	287.2	287.2	286.2	286.2	3	1.756
-2	0.003	0.003	0.003	286.5	285.6	285.6	286.5	286.5	286.5	286.2	286.2	287.2	287.2	287.2	286.2	286.2	4	1.756
-1	0.003	0.003	0.003	286.5	285.6	285.6	286.5	286.5	286.5	286.2	286.2	287.2	287.2	287.2	286.2	286.2	5	1.756
0	0.483	367.1	0.003	287.3	285.5	285.5	286.7	286.7	287.5	286.2	286.2	287.2	287.2	287.2	286.7	286.2	6	1.756
1	0.503	261.2	1.065	294.8	292.4	290.7	292.7	293.5	294.4	293.2	293.2	291.2	290.2	291.2	289.2	289.2	7	1.756
2	0.497	237.1	1.195	299.5	298.1	297.8	298.8	299.0	298.4	293.7	295.2	296.2	294.7	295.2	294.7	295.2	8	1.756
3	0.490	234.2	1.313	302.9	301.5	301.4	302.0	302.5	302.4	298.2	298.2	300.2	299.2	300.2	300.2	300.2	9	1.756
4	0.490	231.8	1.418	304.5	303.6	303.2	303.8	304.3	304.8	301.2	301.2	301.7	302.2	302.7	301.7	301.7	10	1.756
5	0.482	230.1	1.513	305.9	304.5	303.9	305.2	305.4	305.1	303.2	304.2	304.2	303.2	303.2	303.2	304.2	11	1.756
6	0.483	247.4	1.600	306.8	304.7	304.7	305.2	305.4	305.5	304.2	304.2	305.2	305.2	305.2	304.7	305.2	12	1.756
7	0.483	244.5	1.681	306.7	304.5	305.1	305.9	305.8	305.3	304.2	304.2	305.2	305.2	305.2	305.2	305.2	13	1.756
8	0.480	240.5	1.754	306.3	304.5	305.5	306.4	306.0	305.3	305.2	305.2	306.2	305.2	305.2	305.2	305.2		
9	0.476	238.3	1.822	306.1	305.2	304.9	305.9	305.0	305.5	306.2	304.2	305.2	305.2	305.2	305.2	306.2		
10	0.476	235.8	1.884	305.7	304.7	304.7	305.7	304.0	306.2	305.2	304.7	305.2	305.2	305.2	304.7	305.2		
11	0.429	229.1	1.941	305.9	304.6	304.6	305.1	304.7	304.5	305.2	304.2	305.2	305.2	305.2	306.2	304.2		
12	0.429	186.2	1.976	303.8	303.5	303.8	304.6	304.4	304.4	304.2	303.7	304.7	304.7	304.7	304.2	304.2		
13	0.429	163.0	1.982	303.5	302.5	302.5	303.7	302.5	303.2	303.2	303.2	304.2	305.2	305.2	305.2	304.2		
14	0.000	0.000	1.980	303.8	301.8	302.1	303.5	302.9	302.9	303.2	303.2	304.2	304.2	304.2	304.2	303.7		
15	0.000	0.000	1.978	303.2	301.4	301.8	302.8	302.1	301.9	302.2	302.2	304.2	304.2	304.2	304.2	303.2		
16	0.000	0.000	1.977	303.0	301.6	301.6	302.4	302.3	301.7	301.7	302.2	303.2	303.2	303.2	303.2	303.2		
17	0.000	0.000	1.975	302.9	301.7	301.8	302.4	302.4	302.1	302.2	302.2	303.2	303.2	303.2	303.2	302.2		
18	0.000	0.000	1.974	302.2	301.3	301.5	302.6	302.2	302.0	301.2	302.2	302.2	303.2	303.2	303.2	302.2		
19	0.000	0.000	1.973	301.9	301.0	301.5	302.4	302.1	302.1	301.2	301.2	302.2	302.2	302.2	302.2	301.2		
20	0.000	0.000	1.971	301.5	300.6	301.2	302.0	301.9	302.1	301.2	301.2	302.2	302.2	302.2	302.2	301.2		
21	0.000	0.000	1.970	301.2	300.2	300.6	301.5	301.4	301.7	301.2	301.2	302.2	302.2	302.2	302.2	301.2		
22	0.000	0.000	1.966	300.8	299.5	299.3	300.1	300.0	299.9	300.2	300.2	300.2	301.2	301.2	301.2	300.2		
23	0.000	0.000	1.962	299.9	298.9	299.2	300.0	299.5	300.0	300.2	300.2	301.2	301.2	301.2	301.2	301.2		
24	0.000	0.000	1.959	299.5	298.8	298.8	299.7	299.5	299.5	300.2	300.2	301.2	301.2	301.2	301.2	300.2		
25	0.000	0.000	1.956	299.7	298.8	298.9	299.6	299.5	299.5	299.2	299.2	300.2	300.2	300.2	300.2	299.2		
26	0.000	0.000	1.954	299.4	298.4	298.5	299.2	299.5	299.5	298.2	298.2	299.2	299.2	299.2	299.2	298.2		
27	0.000	0.000	1.952	299.3	298.4	298.5	299.1	299.0	299.1	298.2	298.2	299.2	299.2	299.2	299.2	298.2		
28	0.000	0.000	1.950	299.1	298.3	298.1	298.6	298.6	298.9	298.2	298.2	300.2	300.2	300.2	300.2	298.2		
29	0.000	0.000	1.948	298.6	297.7	297.7	298.8	298.8	299.0	298.2	298.2	299.2	299.2	299.2	299.2	298.2		
30	0.000	0.000	1.946	298.6	297.4	297.4	298.5	298.6	298.7	298.2	298.2	299.2	299.2	299.2	299.2	298.2		
31	0.000	0.000	1.945	298.4	297.4	297.5	298.5	298.6	298.7	298.2	298.2	299.2	299.2	299.2	299.2	298.2		
32	0.000	0.000	1.942	298.1	297.3	297.3	298.1	298.1	298.3	297.2	296.7	298.2	298.2	298.2	297.2	298.2		
33	0.000	0.000	1.940	298.0	296.5	297.1	298.0	297.4	297.4	297.2	296.2	297.2	297.2	297.2	297.2	297.2		
34	0.000	0.000	1.938	297.4	296.5	296.6	297.4	297.1	297.1	297.2	296.2	297.2	297.2	297.2	296.2	297.2		
35	0.000	0.000	1.936	296.9	296.2	296.4	297.2	297.2	297.2	297.2	296.2	297.2	297.2	297.2	296.2	297.2		
36	0.000	0.000	1.934	297.1	295.8	295.8	297.0	297.0	297.1	296.2	296.2	297.2	297.2	297.2	296.2	297.2		
37	0.000	0.000	1.932	296.9	295.7	295.5	296.7	296.7	296.9	296.2	296.2	297.2	297.2	297.2	296.2	297.2		
38	0.000	0.000	1.930	296.6	295.5	295.5	296.4	296.4	296.4	296.2	296.2	297.2	297.2	297.2	296.2	297.2		
39	0.000	0.000	1.929	296.4	295.2	295.4	296.2	296.2	296.9	296.2	296.2	297.2	297.2	297.2	296.2	297.2		
40	0.000	0.000	1.927	295.9	295.0	295.2	296.0	296.0	296.1	296.2	296.2	297.2	297.2	297.2	296.2	297.2		
41	0.000	0.000	1.926	296.0	294.6	294.8	296.0	295.9	295.8	296.2	296.2	297.2	297.2	297.2	296.2	297.2		
42	0.000	0.000	1.924	295.9	294.5	294.5	295.9	295.9	295.8	296.2	296.2	297.2	297.2	297.2	296.2	297.2		
43	0.000	0.000	1.923	295.7	294.5	294.5	295.2	295.1	295.7	295.2	295.2	296.2	296.2	296.2	295.2	296.2		
44	0.000	0.000	1.922	295.4	294.3	294.3	295.1	295.0	295.2	295.2	295.2	296.2	296.2	296.2	295.2	296.2		

Table 4A — Scaling Run 232: Uncluttered 324—m<sup>3</sup> Chamber, Three 3.279-cm Nozzles

Press			Chamber			Chamber Absolute Temperatures (K) at Locations /													COORDINATES			
Time	Cyl	P	T <sub>c</sub>	P	T <sub>c</sub>	1	2	3	4	5	6	7	8	9	10	11	12	13	R	THETA	Z	
(s)	(atm)	(atm)	(K)	(atm)	(K)														(M)	(DEG)	(M)	
-5	000	000	000	1.005	281.6	280.7	280.6	281.6	281.4	281.5	281.2	281.2	281.2	282.2	282.2	282.2	282.2	281.2	1	1.756	45	-0.586
-4	000	000	000	1.005	281.6	280.7	280.6	281.6	281.4	281.5	281.2	281.2	281.2	282.2	282.2	282.2	282.2	281.2	2	1.756	45	-0.293
-3	000	000	000	1.005	281.5	280.7	280.7	281.6	281.4	281.5	281.2	281.2	281.2	282.2	282.2	282.2	282.2	281.2	3	1.756	45	0.000
-2	000	000	000	1.005	281.5	280.7	280.7	281.6	281.4	281.5	281.2	281.2	281.2	282.2	282.2	282.2	282.2	281.2	4	1.756	45	0.293
-1	000	000	000	1.005	281.5	280.7	280.6	281.6	281.4	281.5	281.2	281.2	281.2	282.2	282.2	282.2	282.2	281.2	5	1.756	45	0.586
0	097.061	279.6	103.695	1.066	282.7	281.4	280.9	282.1	282.4	283.3	281.3	281.2	281.2	282.2	282.2	282.2	282.2	281.2	6	1.756	45	0.878
1	103.695	286.9	1.227	1.096	289.9	287.6	285.6	289.4	290.1	289.4	290.1	286.2	287.7	286.7	287.2	285.7	285.7	285.7	7	1.756	45	2.049
2	276.365	282.1	1.307	1.227	295.3	293.6	292.5	294.0	294.9	294.9	291.2	291.2	292.2	291.2	292.2	291.2	292.2	292.2	8	1.756	45	2.342
3	371.952	248.4	1.367	1.367	298.4	297.3	296.7	297.1	297.9	297.7	294.2	295.2	296.2	294.2	295.2	294.2	294.2	294.2	9	1.756	45	2.635
4	465.932	246.2	1.415	1.415	298.4	298.5	298.0	298.9	299.3	299.7	299.3	299.2	299.2	299.2	299.2	299.2	299.2	299.2	10	1.756	45	2.928
5	560.497	241.3	1.516	1.516	300.7	299.4	299.0	300.4	300.0	300.9	298.2	298.2	299.2	299.2	299.2	299.2	299.2	298.2	11	1.756	45	3.220
6	635.755	241.3	1.604	1.604	300.9	300.1	300.0	300.0	300.0	301.0	299.7	298.7	299.7	299.7	299.7	299.7	299.7	299.7	12	1.756	45	3.513
7	731.442	238.3	1.687	1.687	300.8	300.0	300.2	301.0	301.5	301.2	300.2	300.2	301.2	300.2	300.2	300.2	300.2	300.2	13	1.756	45	3.806
8	847.602	236.7	1.762	1.762	301.4	300.0	300.6	301.3	301.7	300.9	300.2	299.7	299.7	299.7	299.7	299.7	299.7	299.7				
9	1040.973	231.3	1.894	1.894	301.3	300.4	301.1	302.0	301.6	300.2	299.7	298.7	300.7	300.7	300.7	300.7	300.7	300.7				
10	1130.776	219.3	1.932	1.932	301.1	300.0	300.6	300.0	300.3	300.0	299.2	298.2	299.2	299.2	299.2	299.2	299.2	299.2				
11	1239.265	172.3	1.974	1.974	299.9	299.3	299.0	300.5	299.9	299.5	299.2	298.2	298.2	298.2	298.2	298.2	298.2	298.2				
12	1339.606	169.8	1.979	1.979	299.4	298.0	298.6	298.9	298.7	298.7	298.2	298.2	298.7	298.7	298.7	298.7	298.7	298.7				
13	14	000	1.978	1.978	298.6	297.4	297.5	298.0	297.6	298.0	298.2	297.2	298.2	298.2	298.2	298.2	298.2	298.2				
14	15	000	1.976	1.976	298.6	296.8	296.7	297.9	297.5	297.5	297.0	297.7	297.2	298.2	297.2	297.2	297.2	297.2				
15	16	000	1.975	1.975	297.6	296.9	296.7	297.6	297.1	297.0	297.2	297.2	298.2	297.2	297.2	297.2	297.2	297.2				
16	17	000	1.973	1.973	296.7	295.7	295.6	296.4	296.0	296.4	296.8	297.2	297.2	298.2	297.2	297.2	297.2	297.2				
17	18	000	1.972	1.972	296.9	295.5	295.5	296.0	296.7	296.0	296.7	297.2	297.2	298.2	297.2	297.2	297.2	297.2				
18	19	000	1.970	1.970	297.2	295.6	295.7	296.0	296.6	296.5	296.7	296.7	297.2	297.2	297.2	297.2	297.2	297.2				
19	20	000	1.969	1.969	297.2	296.0	295.8	296.0	296.6	296.5	296.6	296.6	297.2	297.2	297.2	297.2	297.2	297.2				
20	21	000	1.968	1.968	296.5	295.5	295.7	296.4	295.9	295.9	295.5	296.2	296.2	297.2	297.2	297.2	297.2	297.2				
21	22	000	1.966	1.966	296.5	295.4	295.5	296.4	295.9	295.9	295.5	296.2	296.2	297.2	297.2	297.2	297.2	297.2				
22	23	000	1.963	1.963	296.4	295.4	295.5	296.4	295.9	295.9	295.5	296.2	296.2	297.2	297.2	297.2	297.2	297.2				
23	24	000	1.959	1.959	295.7	295.0	294.5	295.2	295.1	295.1	295.2	295.2	296.2	296.2	296.2	296.2	296.2	296.2				
24	25	000	1.956	1.956	295.2	294.3	294.0	295.0	295.0	295.0	295.2	295.2	296.2	296.2	296.2	296.2	296.2	296.2				
25	26	000	1.954	1.954	295.3	294.0	293.0	294.2	294.0	294.1	294.2	294.2	295.2	295.2	295.2	295.2	295.2	295.2				
26	27	000	1.951	1.951	294.2	293.2	293.1	293.8	293.7	293.6	294.2	294.2	295.2	295.2	295.2	295.2	294.2	294.2				
27	28	000	1.949	1.949	293.8	292.9	292.9	293.0	293.0	293.0	293.2	293.2	294.2	294.2	294.2	294.2	293.2	293.2				
28	29	000	1.946	1.946	293.6	292.4	292.8	293.2	293.7	293.5	293.2	293.2	294.2	294.2	294.2	294.2	293.2	293.2				
29	30	000	1.944	1.944	293.5	292.4	292.6	293.2	293.4	293.3	293.2	293.2	294.2	294.2	294.2	294.2	293.2	293.2				
30	31	000	1.942	1.942	293.2	292.3	292.4	293.2	293.3	293.3	293.3	293.3	294.2	294.2	294.2	294.2	293.2	293.2				
31	32	000	1.941	1.941	293.2	292.0	292.0	292.7	292.7	292.5	293.0	292.2	292.2	292.2	292.2	292.2	292.2	292.2				
32	33	000	1.939	1.939	293.0	291.8	291.9	292.7	292.8	292.6	292.2	292.2	292.2	292.2	292.2	292.2	292.2	292.2				
33	34	000	1.938	1.938	292.8	291.3	291.0	292.2	292.2	292.2	292.2	292.2	292.2	292.2	292.2	292.2	292.2	292.2				
34	35	000	1.935	1.935	292.8	291.3	291.0	292.2	292.2	292.2	292.2	292.2	292.2	292.2	292.2	292.2	292.2	292.2				
35	36	000	1.933	1.933	292.8	291.3	291.0	292.2	292.2	292.2	292.2	292.2	292.2	292.2	292.2	292.2	292.2	292.2				
36	37	000	1.930	1.930	291.7	290.0	290.7	291.6	291.5	291.5	291.3	291.2	292.2	292.2	292.2	292.2	292.2	292.2				
37	38	000	1.927	1.927	291.7	290.0	290.7	291.6	291.5	291.5	291.3	291.2	292.2	292.2	292.2	292.2	292.2	292.2				
38	39	000	1.925	1.925	291.5	290.4	290.4	291.3	291.3	291.2	291.2	291.2	292.2	292.2	292.2	292.2	292.2	292.2				
39	40	000	1.923	1.923	290.9	290.9	290.7	291.0	291.0	291.0	290.2	290.2	291.2	291.2	291.2	291.2	290.2	290.2				
40	41	000	1.921	1.921	290.5	290.9	290.7	291.0	291.0	290.5	290.5	290.2	290.2	291.2	291.2	291.2	290.2	290.2				
41	42	000	1.921	1.921	290.5	290.9	290.6	290.5	290.5	290.3	290.2	290.2	291.2	291.2	291.2	291.2	290.2	290.2				
42	43	000	1.920	1.920	290.4	290.5	290.6	290.5	290.5	290.3	290.2	290.2	291.2	291.2	291.2	291.2	290.2	290.2				
43	44	000	1.918	1.918	290.4	290.5	290.6	290.5	290.5	290.3	290.2	290.2	291.2	291.2	291.2	291.2	290.2	290.2				
44	45	000	1.917	1.917	289.9	289.1	289.2	289.9	289.8	289.9	289.2	289.2	290.2	290.2	290.2	290.2	289.2	289.2				
45	46	000	1.915	1.915	289.7	288.8	288.9	289.6	289.7	289.2	289.2	289.2	290.2	290.2	290.2	290.2	289.2	289.2				
46	47	000	1.914	1.914	289.5	288.6	288.9	289.2	289.2	289.1	289.2	289.2	290.2	290.2	290.2	290.2	289.2	289.2				

Table 5A -- Scaling Run 233: Uncluttered 324-m<sup>3</sup> Chamber, Three 3.279-cm Nozzles

Time t (s)	Press P (atm)	Chamber P (atm)	T <sub>i</sub> (K)	Chamber Absolute Temperatures (K) at Locations /													COORDINATES			
				1	2	3	4	5	6	7	8	9	10	11	12	13	R (cm)	THETA Z (DEG)	Z	
-5	0.00	1.000	000	285.6	284.5	284.5	285.5	285.4	285.4	285.2	285.2	286.2	286.2	285.2	285.2	285.2	1	1.756	45	-0.386
-3	0.00	1.000	000	285.6	284.5	284.4	285.5	285.4	285.4	285.2	285.2	286.2	286.2	285.2	285.2	285.2	2	1.756	45	-0.293
-2	0.00	1.000	000	285.6	284.5	284.4	285.5	285.4	285.4	285.2	285.2	286.2	286.2	285.2	285.2	285.2	3	1.756	45	0.000
-2	0.00	1.000	000	285.6	284.5	284.5	285.5	285.4	285.4	285.2	285.2	286.2	286.2	285.2	285.2	285.2	4	1.756	45	0.293
-1	0.00	1.000	000	285.6	284.5	284.5	285.5	285.4	285.4	285.2	285.2	286.2	286.2	285.2	285.2	285.2	5	1.756	45	0.586
0	483 305.1	1.000	000	286.7	285.6	284.5	285.5	286.4	287.5	288.4	288.2	288.2	288.2	288.2	288.2	288.2	6	1.756	45	0.878
1	497 262.4	1.060	000	292.6	290.0	287.9	289.6	291.2	292.4	287.2	287.2	290.2	289.2	289.2	288.2	288.2	7	1.756	45	2.042
2	497 256.5	1.195	000	298.0	296.0	294.9	296.1	296.3	296.9	292.7	292.7	294.2	295.2	294.2	294.2	294.2	8	1.756	45	2.342
3	496 250.8	1.312	000	301.2	299.6	298.7	299.7	300.3	299.9	296.2	297.2	298.2	297.2	298.2	297.2	297.2	9	1.756	45	2.633
4	486 236.1	1.416	000	303.1	301.5	301.2	302.4	303.0	303.0	303.0	299.7	299.7	301.2	300.7	299.7	299.7	10	1.756	45	2.924
5	483 247.7	1.511	000	304.5	303.0	302.3	303.3	303.5	304.1	302.2	302.2	302.2	302.2	302.2	301.2	302.2	11	1.756	45	3.220
6	483 244.7	1.597	000	304.5	303.3	303.5	304.2	304.5	304.9	304.0	302.7	303.2	304.2	303.7	304.2	303.2	12	1.756	45	3.513
7	476 243.3	1.676	000	305.4	303.8	303.8	304.2	304.6	305.3	304.2	304.2	304.2	305.2	304.2	304.2	303.2	13	1.756	45	3.806
8	476 240.7	1.748	000	305.2	303.9	303.8	304.9	305.0	305.6	304.2	304.2	304.2	305.2	304.7	304.2	304.2				
9	476 237.9	1.815	000	305.4	303.6	304.0	304.6	304.7	305.2	304.2	304.2	304.2	305.2	304.2	304.2	304.2				
10	476 235.4	1.877	000	305.5	303.7	303.9	304.6	304.5	305.2	303.7	303.2	304.2	304.2	304.2	303.7	304.2				
11	429 231.7	1.934	000	304.3	302.7	303.4	304.2	304.7	304.6	303.2	303.2	304.2	304.2	304.2	304.2	304.2				
12	429 186.5	1.972	000	302.7	301.7	302.1	302.3	303.3	303.5	302.5	302.7	302.2	303.2	303.2	302.2	303.7				
13	429 169.7	1.979	000	302.8	301.5	301.9	302.8	302.5	302.5	302.2	302.2	303.2	303.2	302.2	302.2	302.2				
14	000	1.978	000	302.8	301.6	301.8	302.4	302.6	302.5	302.2	302.2	303.2	303.2	302.2	302.2	302.2				
15	000	1.976	000	302.3	301.2	301.2	302.2	301.9	301.8	302.2	301.2	302.2	302.2	302.2	302.2	302.2				
16	000	1.974	000	301.7	300.4	300.5	301.4	300.8	300.7	300.7	300.7	302.2	302.2	302.2	302.2	301.7				
17	000	1.973	000	301.0	299.6	299.5	300.8	300.4	300.6	300.2	300.2	302.2	302.2	302.2	302.2	302.2				
18	000	1.971	000	300.5	298.3	299.2	300.0	299.5	300.0	300.2	300.2	302.2	302.2	302.2	302.2	301.2				
19	000	1.970	000	300.1	298.7	299.0	300.2	300.2	300.3	300.2	300.3	302.2	302.2	302.2	302.2	301.2				
20	000	1.969	000	300.0	299.3	299.3	300.3	300.2	299.6	300.2	299.6	302.2	302.2	302.2	302.2	300.7				
21	000	1.968	000	300.6	299.5	299.5	300.3	299.9	299.9	299.8	299.8	302.2	302.2	302.2	302.2	300.2				
22	000	1.963	000	299.7	298.6	298.7	300.0	300.0	300.0	299.2	299.2	301.2	301.2	301.2	301.2	300.2				
31	000	1.960	000	299.0	298.1	298.3	298.5	299.3	299.3	298.7	298.2	299.2	299.2	299.2	298.2	298.2				
36	000	1.956	000	298.5	297.8	297.9	298.9	299.0	299.1	298.2	298.2	299.2	299.2	299.2	298.2	298.2				
41	000	1.954	000	298.5	297.2	297.5	298.5	298.3	298.6	298.2	298.2	299.2	299.2	299.2	298.2	298.2				
46	000	1.951	000	298.5	297.4	297.5	298.5	298.4	298.3	297.2	297.2	299.2	299.2	299.2	298.2	298.2				
51	000	1.949	000	298.2	297.2	297.3	298.3	298.1	298.0	297.2	297.2	298.7	298.7	298.2	298.2	298.2				
56	000	1.947	000	297.9	296.7	296.8	297.7	297.8	297.8	298.0	297.2	297.2	298.2	298.2	298.2	298.2				
61	000	1.945	000	297.0	296.5	296.7	297.5	297.6	297.6	297.8	297.2	297.2	298.2	298.2	298.2	297.2				
66	000	1.944	000	298.0	296.4	296.4	297.3	297.3	297.3	297.5	297.2	297.2	298.2	298.2	298.2	297.2				
71	000	1.942	000	297.0	296.4	296.7	297.0	297.2	297.4	297.2	297.2	298.2	298.2	298.2	298.2	297.2				
81	000	1.940	000	297.4	296.2	296.2	297.4	297.2	297.2	296.2	296.2	297.2	297.2	297.2	297.2	296.2				
91	000	1.937	000	296.0	295.9	296.0	297.1	297.1	296.9	296.2	296.2	297.2	297.2	297.2	297.2	296.2				
101	000	1.935	000	296.3	295.2	295.6	296.7	296.7	296.5	296.2	296.2	297.2	297.2	297.2	297.2	296.2				
111	000	1.933	000	296.6	295.9	295.4	296.5	296.5	296.3	296.2	296.2	297.2	297.2	297.2	297.2	296.2				
121	000	1.931	000	296.1	296.9	294.8	295.8	296.0	295.8	295.2	295.2	296.2	296.2	296.2	296.2	295.2				
131	000	1.929	000	296.2	295.0	295.0	295.7	295.6	295.7	295.2	295.2	296.2	296.2	296.2	296.2	295.2				
141	000	1.927	000	295.9	294.7	294.6	295.3	295.3	295.3	295.2	295.2	296.2	296.2	296.2	296.2	295.2				
151	000	1.926	000	295.0	294.5	294.5	294.8	295.2	295.2	295.2	295.2	296.2	296.2	296.2	296.2	295.2				
161	000	1.924	000	295.4	294.2	294.2	295.3	295.1	295.0	294.8	294.8	296.2	296.2	296.2	296.2	295.2				
171	000	1.922	000	295.1	293.5	294.2	295.0	295.0	295.0	294.7	295.2	296.2	296.2	296.2	296.2	294.2				
181	000	1.921	000	294.7	293.6	293.8	295.0	295.0	295.0	294.6	294.2	296.2	296.2	296.2	296.2	294.2				
191	000	1.920	000	294.6	293.4	293.0	294.9	294.7	294.5	294.7	294.5	296.2	296.2	296.2	296.2	293.2				
201	000	1.919	000	294.5	293.1	293.1	294.2	294.4	294.5	294.2	293.2	295.2	295.2	295.2	295.2	293.2				

Table 6A — Scaling Run 234: Uncluttered 324-m<sup>3</sup> Chamber, Three 3.279-cm Nozzles

Press Cyl P (atm)	Chamber P (atm)	T <sub>c</sub> (K)	Chamber Absolute Temperatures (K) at Locations /													COORDINATES R THETA Z (M) (DEC) (M)		
1	2	3	4	5	6	7	8	9	10	11	12	13	I	R (M)	THETA Z (DEC) (M)			
-9	1.001	201.9	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	1	1.756	45 -0.506			
-8	1.001	201.9	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	2	1.756	45 -0.253			
-7	1.001	201.9	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	3	1.756	45 0.000			
-6	1.001	201.9	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	4	1.756	45 0.253			
-5	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	5	1.756	45 0.506			
-4	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	6	1.756	45 0.759			
-3	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	7	1.756	45 1.012			
-2	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	8	1.756	45 1.265			
-1	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	9	1.756	45 1.518			
0	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	10	1.756	45 1.771			
1	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	11	1.756	45 2.024			
2	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	12	1.756	45 2.277			
3	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	13	1.756	45 2.530			
4	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	14	1.756	45 2.783			
5	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	15	1.756	45 3.036			
6	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	16	1.756	45 3.289			
7	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	17	1.756	45 3.542			
8	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	18	1.756	45 3.795			
9	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	19	1.756	45 4.048			
10	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	20	1.756	45 4.301			
11	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	21	1.756	45 4.554			
12	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	22	1.756	45 4.807			
13	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	23	1.756	45 5.060			
14	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	24	1.756	45 5.313			
15	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	25	1.756	45 5.566			
16	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	26	1.756	45 5.819			
17	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	27	1.756	45 6.072			
18	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	28	1.756	45 6.325			
19	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	29	1.756	45 6.578			
20	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	30	1.756	45 6.831			
21	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	31	1.756	45 7.084			
22	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	32	1.756	45 7.337			
23	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	33	1.756	45 7.590			
24	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	34	1.756	45 7.843			
25	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	35	1.756	45 8.096			
26	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	36	1.756	45 8.349			
27	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	37	1.756	45 8.602			
28	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	38	1.756	45 8.855			
29	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	39	1.756	45 9.108			
30	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	40	1.756	45 9.361			
31	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	41	1.756	45 9.614			
32	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	42	1.756	45 9.867			
33	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	43	1.756	45 10.120			
34	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	44	1.756	45 10.373			
35	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	45	1.756	45 10.626			
36	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	46	1.756	45 10.879			
37	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	47	1.756	45 11.132			
38	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	48	1.756	45 11.385			
39	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	49	1.756	45 11.638			
40	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	50	1.756	45 11.891			
41	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	51	1.756	45 12.144			
42	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	52	1.756	45 12.397			
43	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	53	1.756	45 12.650			
44	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	54	1.756	45 12.903			
45	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	55	1.756	45 13.156			
46	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	56	1.756	45 13.409			
47	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	57	1.756	45 13.662			
48	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	58	1.756	45 13.915			
49	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	59	1.756	45 14.168			
50	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	60	1.756	45 14.421			
51	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	61	1.756	45 14.674			
52	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	62	1.756	45 14.927			
53	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	63	1.756	45 15.180			
54	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	64	1.756	45 15.433			
55	1.001	202.0	200.9	200.9	201.9	201.9	201.2	201.2	202.2	202.2	202.2	201.2	65	1.756	45 15.686			
56																		



### Table 7A — Scaling Run 235: Uncluttered 324-m<sup>3</sup> Chamber, Three 3.279-cm Nozzles

Time <i>t</i>	Press <i>P</i>	Chamber <i>P</i>	Chamber Absolute Temperatures (K) at Locations /													COORDINATES					
			1	2	3	4	5	6	7	8	9	10	11	12	13	<i>R</i> (M)	THETA 2 (DEG)				
-5	0.001	0.001	203.5	203.0	202.9	203.0	203.0	203.9	203.2	203.2	203.2	203.2	203.2	203.2	203.2	203.2	203.2	1	1.756	45	-0.506
-4	1.001	1.001	203.5	203.0	202.9	203.0	203.0	203.9	203.2	203.2	203.2	203.2	203.2	203.2	203.2	203.2	203.2	2	1.756	45	-0.293
-3	0.001	0.001	203.5	203.0	202.9	203.0	203.0	203.9	203.2	203.2	203.2	203.2	203.2	203.2	203.2	203.2	203.2	3	1.756	45	0.000
-2	1.001	1.001	203.5	203.0	202.9	203.0	203.0	203.9	203.2	203.2	203.2	203.2	203.2	203.2	203.2	203.2	203.2	4	1.756	45	0.293
-1	0.001	0.001	203.5	203.0	202.9	203.0	203.0	203.9	203.2	203.2	203.2	203.2	203.2	203.2	203.2	203.2	203.2	5	1.756	45	0.506
0.94	0.53	360.0	204.5	203.5	202.9	203.0	203.0	203.9	203.2	203.2	203.2	203.2	203.2	203.2	203.2	203.2	203.2	6	1.756	45	0.678
1.03	367	263.2	291.8	289.5	288.0	289.7	290.3	291.8	286.2	288.2	288.2	287.2	288.7	288.7	286.7	287.2	287.2	7	1.756	45	2.049
2.76	313	256.3	297.1	295.6	295.2	296.1	296.9	297.1	293.2	292.2	293.2	293.2	293.2	295.2	295.2	292.2	292.2	8	1.756	45	2.342
3.69	867	234.9	300.2	299.2	298.6	299.4	299.6	299.4	295.2	295.2	295.2	296.2	296.2	296.2	296.2	295.2	295.2	9	1.756	45	2.635
4.63	959	233.8	302.2	300.8	299.6	301.6	302.1	301.8	297.2	298.2	299.2	299.2	299.2	299.2	298.2	297.2	297.2	10	1.756	45	2.923
5.98	772	248.5	303.4	303.1	301.9	302.5	302.8	303.0	300.7	301.2	302.2	302.2	302.2	302.2	302.2	302.2	302.2	11	1.756	45	3.220
6.94	661	245.7	304.0	302.1	301.9	302.6	302.7	302.7	302.4	302.2	302.2	302.2	302.2	302.2	302.2	302.2	302.2	12	1.756	45	3.513
7.81	306	243.1	303.4	302.4	302.4	303.1	303.3	303.3	303.3	303.2	302.2	302.2	302.2	302.2	302.2	302.2	302.2	13	1.756	45	3.806
9.47	486	240.2	304.5	302.7	302.5	303.8	303.6	303.6	303.6	303.5	302.2	301.7	302.2	302.2	302.2	302.2	302.2				
10.40	095	235.2	304.4	302.1	302.7	303.9	303.5	303.5	303.3	303.7	301.7	302.2	302.2	302.2	302.2	302.2	302.2				
11.28	020	231.5	303.4	302.2	303.1	303.6	303.3	302.7	303.2	303.2	301.2	302.2	302.2	302.2	302.2	302.2	302.2				
12.37	160	182.0	302.5	301.3	301.7	302.2	302.0	301.9	300.7	300.7	301.7	301.7	301.7	301.7	301.7	300.7	300.7				
13.37	680	164.5	301.5	300.6	300.9	301.8	301.6	301.6	300.2	300.2	301.2	301.2	301.2	301.2	301.2	300.2	300.2				
14	0.00	0.00	301.4	300.1	300.3	301.2	301.0	300													

Table 8A — Scaling Run 236: Uncluttered 324-m<sup>3</sup> Chamber, Three 3.279-cm Nozzles

Time t (s)	Press Cyl P (atm)	T <sub>c</sub> (K)	Chamber P (atm)	Chamber Absolute Temperatures (K) at Locations /																COORDINATES				
				1	2	3	4	5	6	7	8	9	10	11	12	13	1	R (M)	THETA (DEG)	Z (M)				
-5	...	...	...	290.1	288.8	288.0	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	1	1.756	45	-0.586
-4	...	...	...	290.1	288.8	288.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	2	1.756	45	-0.293
-3	...	...	...	290.0	288.9	288.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	3	1.756	45	0.000
-2	...	...	...	290.0	288.9	288.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	4	1.756	45	0.293
-1	...	...	...	290.1	288.9	288.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	289.8	5	1.756	45	0.586
0.33	816	286.3	...	292.0	291.2	290.0	291.7	292.2	293.0	293.0	293.0	293.0	293.0	293.0	293.0	293.0	293.0	293.0	293.0	293.0	6	1.756	45	0.878
1.77	442	286.8	1.086	300.4	298.2	296.2	298.2	299.5	300.3	299.3	299.2	299.2	299.4	299.4	299.2	299.2	299.2	299.2	299.2	299.2	7	1.756	45	2.049
2.72	673	285.1	1.219	303.9	302.4	301.3	302.6	302.7	302.9	302.9	302.9	302.9	302.9	302.9	302.9	302.9	302.9	302.9	302.9	302.9	8	1.756	45	2.342
3.66	622	281.7	1.334	307.2	305.2	305.1	305.8	306.3	306.6	306.2	306.2	306.2	306.2	306.2	306.2	306.2	306.2	306.2	306.2	306.2	9	1.756	45	2.635
4.61	279	259.8	1.441	309.7	307.6	307.9	308.7	308.5	308.4	308.4	308.4	308.4	308.4	308.4	308.4	308.4	308.4	308.4	308.4	308.4	10	1.756	45	2.928
5.58	427	257.2	1.566	310.3	308.9	308.9	309.7	309.6	309.5	309.2	309.2	309.2	309.2	309.2	309.2	309.2	309.2	309.2	309.2	309.2	11	1.756	45	3.220
6.53	524	252.2	1.594	311.3	309.6	309.6	310.0	310.0	310.0	310.0	310.0	310.0	310.0	310.0	310.0	310.0	310.0	310.0	310.0	310.0	12	1.756	45	3.513
7.49	517	249.5	1.675	311.3	309.8	309.8	310.5	310.5	310.5	310.5	310.5	310.5	310.5	310.5	310.5	310.5	310.5	310.5	310.5	310.5	13	1.756	45	3.806
8.45	965	247.1	1.749	310.2	310.0	310.1	311.1	311.1	311.1	311.0	309.2	308.2	308.7	308.7	308.7	308.7	308.7	308.7	308.7	308.7	14	1.756	45	4.099
9.42	592	244.4	1.818	311.0	309.5	309.6	310.4	310.4	310.4	310.4	309.2	308.2	310.2	309.2	309.2	309.2	309.2	309.2	309.2	309.2	15	1.756	45	4.392
10.39	646	241.7	1.881	310.5	309.3	309.9	310.5	310.5	310.5	310.5	308.7	308.7	308.7	310.2	309.2	309.2	309.2	309.2	309.2	309.2	16	1.756	45	4.685
11.37	857	236.8	1.937	309.8	308.9	309.2	309.8	309.8	309.8	310.2	308.2	308.2	308.2	309.2	309.2	309.2	309.2	309.2	309.2	309.2	17	1.756	45	4.978
12.38	308	176.7	1.964	309.0	307.9	308.0	308.7	308.7	308.7	308.7	308.7	308.7	308.7	308.7	308.7	308.7	308.7	308.7	308.7	308.7	18	1.756	45	5.271
13.30	514	165.8	1.969	307.6	306.9	307.3	308.1	308.0	308.0	308.0	308.0	308.0	308.0	308.0	308.0	308.0	308.0	308.0	308.0	308.0	19	1.756	45	5.564
14	...	...	1.968	306.3	305.5	306.5	307.5	306.9	306.8	306.8	306.8	306.8	306.8	306.8	306.8	306.8	306.8	306.8	306.8	306.8	20	1.756	45	5.857
15	...	...	1.966	305.9	304.7	305.9	307.1	306.7	306.4	306.4	306.4	306.4	306.4	306.4	306.4	306.4	306.4	306.4	306.4	306.4	21	1.756	45	6.150
16	...	...	1.964	306.1	303.8	305.3	306.6	306.4	306.4	306.4	306.4	306.4	306.4	306.4	306.4	306.4	306.4	306.4	306.4	306.4	22	1.756	45	6.443
17	...	...	1.963	306.1	304.8	305.3	306.6	306.4	306.4	306.4	306.4	306.4	306.4	306.4	306.4	306.4	306.4	306.4	306.4	306.4	23	1.756	45	6.736
18	...	...	1.961	305.9	304.4	304.6	305.5	305.3	305.3	305.3	305.2	305.2	305.2	305.2	305.2	305.2	305.2	305.2	305.2	305.2	24	1.756	45	7.029
19	...	...	1.960	305.5	304.0	304.1	305.2	305.0	305.0	305.0	305.2	305.2	305.2	305.2	305.2	305.2	305.2	305.2	305.2	305.2	25	1.756	45	7.322
20	...	...	1.958	305.0	302.8	304.0	305.0	304.9	304.9	304.9	305.2	305.2	305.2	305.2	305.2	305.2	305.2	305.2	305.2	305.2	26	1.756	45	7.615
21	...	...	1.957	305.0	302.8	303.4	304.5	304.7	305.1	304.2	304.2	304.2	304.2	304.2	304.2	304.2	304.2	304.2	304.2	304.2	27	1.756	45	7.908
22	...	...	1.952	305.0	302.8	303.0	303.8	303.8	303.7	303.2	303.2	303.2	303.2	303.2	303.2	303.2	303.2	303.2	303.2	303.2	28	1.756	45	8.201
23	...	...	1.949	304.5	302.4	303.0	303.8	303.8	303.8	303.7	303.2	303.2	303.2	303.2	303.2	303.2	303.2	303.2	303.2	303.2	29	1.756	45	8.494
24	...	...	1.946	304.2	302.1	303.1	303.8	303.8	303.8	303.8	303.4	303.2	303.2	303.2	303.2	303.2	303.2	303.2	303.2	303.2	30	1.756	45	8.787
25	...	...	1.943	303.9	302.6	302.6	303.5	303.5	303.5	303.5	303.2	303.2	303.2	303.2	303.2	303.2	303.2	303.2	303.2	303.2	31	1.756	45	9.080
26	...	...	1.941	303.5	302.4	302.4	303.1	303.1	303.1	303.1	303.2	303.2	303.2	303.2	303.2	303.2	303.2	303.2	303.2	303.2	32	1.756	45	9.373
27	...	...	1.939	302.6	301.8	301.8	302.7	302.7	302.7	302.7	302.9	302.9	302.9	302.9	302.9	302.9	302.9	302.9	302.9	302.9	33	1.756	45	9.666
28	...	...	1.936	302.6	301.5	301.6	302.5	302.5	302.5	302.5	302.7	302.7	302.7	302.7	302.7	302.7	302.7	302.7	302.7	302.7	34	1.756	45	9.959
29	...	...	1.935	302.6	301.2	301.0	301.5	302.4	302.9	301.2	301.2	301.2	301.2	301.2	301.2	301.2	301.2	301.2	301.2	301.2	35	1.756	45	10.252
30	...	...	1.933	302.4	300.9	300.2	300.5	302.2	302.2	302.2	302.2	302.2	302.2	302.2	302.2	302.2	302.2	302.2	302.2	302.2	36	1.756	45	10.545
31	...	...	1.932	302.4	300.9	300.8	301.6	302.2	302.2	302.2	302.2	302.2	302.2	302.2	302.2	302.2	302.2	302.2	302.2	302.2	37	1.756	45	10.838
32	...	...	1.929	302.2	301.2	301.0	301.4	302.1	302.1	302.1	302.1	302.1	302.1	302.1	302.1	302.1	302.1	302.1	302.1	302.1	38	1.756	45	11.131
33	...	...	1.926	302.3	300.8	300.7	301.4	301.6	301.8	301.2	301.2	301.2	301.2	301.2	301.2	301.2	301.2	301.2	301.2	301.2	39	1.756	45	11.424
34	...	...	1.924	301.7	300.4	300.3	301.3	301.5	301.6	300.2	300.2	300.2	300.2	300.2	300.2	300.2	300.2	300.2	300.2	300.2	40	1.756	45	11.717
35	...	...	1.922	301.2	299.5	300.1	301.2	301.2	301.2	301.2	300.2	300.2	300.2	300.2	300.2	300.2	300.2	300.2	300.2	300.2	41	1.756	45	12.010
36	...	...	1.920	300.9	299.0	300.0	301.0	301.0	301.0	300.2	300.2	300.2	300.2	300.2	300.2	300.2	300.2	300.2	300.2	300.2	42	1.756	45	12.303
37	...	...	1.919	300.5	298.1	299.0	300.8	300.9	300.9	300.9	300.2	300.2	300.2	300.2	300.2	300.2	300.2	300.2	300.2	300.2	43	1.756	45	12.596
38	...	...	1.917	300.5	298.1	299.1	300.2	300.3	300.3	300.9	300.9	300.9	300.9	300.9	300.9	300.9	300.9	300.9	300.9	300.9	44	1.756	45	12.889
39	...	...	1.915	300.4	298.0	299.0	300.9	300.9	300.9	300.9	300.9	300.9	300.9	300.9	300.9	300.9	300.9	300.9	300.9	300.9	45	1.756	45	13.182
40	...	...	1.913	300.2	298.9	299.0	300.9	300.9	300.9	300.9	300.9	300.9	300.9	300.9	300.9	300.9	300.9	300.9	300.9	300.9	46	1.756	45	13.475
41	...	...	1.912	300.1	298.8	299.0	300.9	300.9	300.9	300.9	300.9	300.9	300.9	300.9	300.9	300.9	300.9	300.9	300.9	300.9	47	1.756	45	13.768
42	...	...	1.910	299.9	298.7	299.6	300.5	300.5	300.5	300.5	300.5	300.5	300.5	300.5	300.5	300.5	300.5	300.5	300.5	300.5	48	1.756	45	14.061
43	...	...	1.909	299.7	298.5	299.4	300.3	300.3	300.3	300.3	300.3	300.3	300.3	300.3	300.3	300.3	300.3	300.3	300.3	300.3	49	1.756	45	14.354
44	...	...	1.908	299.5	298.1	299.0	300.3	300.3	300.3	300.3	300.3	300.3	300.3	300.3	300.3	300.3	300.3	300.3	300.3	300.3	50	1.756	45	14.647

Table 9A – Scaling Run 237: Uncluttered 324-m<sup>3</sup> Chamber, Three 3.279-cm Nozzles[illegible]

Table 10A — Scaling Run 238: Uncluttered 324–m<sup>3</sup> Chamber, Three 3.279-cm Nozzles

Time	Press	Chamber	Chamber Absolute Temperatures (K) at Locations /													COORDINATES		
T	P	P	1	2	3	4	5	6	7	8	9	10	11	12	13	R	THETA	Z
(s)	(atm)	(atm)	(K)	(K)	(K)	(K)	(K)	(K)	(K)	(K)	(K)	(K)	(K)	(K)	(K)	(m)	(deg)	(m)
-5	0.000	0.000	280.1	279.1	279.1	280.0	280.0	280.0	280.2	280.2	280.2	280.2	280.2	280.2	279.2	1	0.000	0.000
-4	0.000	0.000	280.2	279.1	279.1	280.0	280.0	280.0	280.2	279.2	280.2	280.2	280.2	280.2	279.2	2	0.000	0.000
-3	0.000	0.000	280.1	279.1	279.1	280.0	280.0	280.0	280.2	279.2	280.2	280.2	280.2	280.2	279.2	3	0.000	0.000
-2	0.000	0.000	280.1	279.1	279.1	280.0	280.0	280.0	280.2	280.2	280.2	280.2	280.2	280.2	279.2	4	0.000	0.000
-1	0.000	0.000	280.1	279.1	279.1	280.0	280.0	280.0	280.2	279.2	280.2	280.2	280.2	280.2	279.2	5	0.000	0.000
0	0.000	0.000	280.1	279.1	279.1	280.0	280.0	280.0	280.2	279.2	280.2	280.2	280.2	280.2	279.2	6	0.000	0.000
1	0.000	0.000	280.1	279.1	279.1	280.0	280.0	280.0	280.2	279.2	280.2	280.2	280.2	280.2	279.2	7	0.000	0.000
2	0.000	0.000	280.1	279.1	279.1	280.0	280.0	280.0	280.2	279.2	280.2	280.2	280.2	280.2	279.2	8	0.000	0.000
3	0.000	0.000	280.1	279.1	279.1	280.0	280.0	280.0	280.2	279.2	280.2	280.2	280.2	280.2	279.2	9	0.000	0.000
4	0.000	0.000	280.1	279.1	279.1	280.0	280.0	280.0	280.2	279.2	280.2	280.2	280.2	280.2	279.2	10	0.000	0.000
5	0.000	0.000	280.1	279.1	279.1	280.0	280.0	280.0	280.2	279.2	280.2	280.2	280.2	280.2	279.2	11	0.000	0.000
6	0.000	0.000	280.1	279.1	279.1	280.0	280.0	280.0	280.2	279.2	280.2	280.2	280.2	280.2	279.2	12	0.000	0.000
7	0.000	0.000	280.1	279.1	279.1	280.0	280.0	280.0	280.2	279.2	280.2	280.2	280.2	280.2	279.2	13	0.000	0.000
8	0.000	0.000	280.1	279.1	279.1	280.0	280.0	280.0	280.2	279.2	280.2	280.2	280.2	280.2	279.2	14	0.000	0.000
9	0.000	0.000	280.1	279.1	279.1	280.0	280.0	280.0	280.2	279.2	280.2	280.2	280.2	280.2	279.2	15	0.000	0.000
10	0.000	0.000	280.1	279.1	279.1	280.0	280.0	280.0	280.2	279.2	280.2	280.2	280.2	280.2	279.2	16	0.000	0.000
11	0.000	0.000	280.1	279.1	279.1	280.0	280.0	280.0	280.2	279.2	280.2	280.2	280.2	280.2	279.2	17	0.000	0.000
12	0.000	0.000	280.1	279.1	279.1	280.0	280.0	280.0	280.2	279.2	280.2	280.2	280.2	280.2	279.2	18	0.000	0.000
13	0.000	0.000	280.1	279.1	279.1	280.0	280.0	280.0	280.2	279.2	280.2	280.2	280.2	280.2	279.2	19	0.000	0.000
14	0.000	0.000	280.1	279.1	279.1	280.0	280.0	280.0										

Table 11A — Sealing Run 239: Uncluttered 324-m<sup>3</sup> Chamber, Three 3.279-cm Nozzles

Time t (s)	Press Cyl P (atm)	T <sub>i</sub> (K)	Chamber P (atm)	Chamber Absolute Temperatures (K) at Locations /													I	COORDINATES R (M)    THEIA 2 (DEG)	
1	2	3	4	5	6	7	8	9	10	11	12	13							
274.2	273.2	273.2	274.3	274.2	274.1	274.2	274.2	275.2	275.2	275.2	274.2	273.2	1	0.000	00				
274.2	273.2	273.2	274.3	274.2	274.1	274.2	274.2	275.2	275.2	275.2	274.2	273.2	2	0.000	04				
274.2	273.2	273.2	274.3	274.2	274.1	274.2	274.2	275.2	275.2	275.2	274.2	273.2	3	0.000	00				
274.2	273.2	273.2	274.3	274.2	274.1	274.2	274.2	275.2	275.2	275.2	274.2	273.2	4	0.000	00				
274.2	273.2	273.2	274.3	274.2	274.1	274.2	274.2	275.2	275.2	275.2	274.2	273.2	5	0.000	00				
276.5	273.9	271.4	274.7	276.4	277.3	274.2	274.7	275.2	275.2	275.2	270.7	273.7	6	0.000	00				
283.6	278.1	267.2	278.7	281.5	282.1	277.2	279.2	279.2	279.2	279.2	271.2	275.2	7	0.000	00				
288.5	282.9	271.3	283.4	286.3	286.9	282.2	284.2	284.2	284.2	283.2	272.7	279.7	8	0.000	00				
291.0	287.2	273.9	285.2	288.6	288.1	286.2	287.2	288.2	287.2	286.2	273.2	283.2	9	0.000	00				
293.1	285.6	273.9	287.5	290.2	289.9	289.2	289.7	290.7	290.7	290.7	273.7	286.2	10	0.000	00				
292.0	287.5	272.8	288.9	290.9	290.7	290.2	290.2	292.2	292.2	291.2	273.2	289.2	11	0.000	00				
294.6	289.2	272.6	290.7	291.6	291.5	291.2	291.7	293.2	293.2	292.2	274.2	287.7	12	0.000	00				
294.9	290.5	272.9	291.0	293.7	293.5	293.2	293.2	293.2	293.2	293.2	274.2	289.2	13	0.000	00				
294.0	290.4	272.3	292.7	293.5	291.6	291.2	292.2	293.2	293.2	292.2	273.2	289.2							
294.2	290.3	272.1	291.3	293.2	292.0	291.2	292.2	293.2	293.2	292.2	274.2	289.2							
294.4	290.4	272.2	291.3	293.2	292.1	291.2	292.2	293.2	293.2	292.2	273.2	289.2							
294.5	290.5	272.5	291.5	291.6	291.5	292.2	292.2	293.2	293.2	292.2	273.2	289.2							
292.8	287.4	272.8	291.2	291.3	290.4	292.2	292.2	293.2	293.2	292.2	273.2	289.2							
285.8	286.5	280.8	290.4	290.5	290.6	291.2	290.7	291.7	291.7	290.2	274.2	285.7							
290.4	288.2	285.8	290.2	290.1	289.9	290.2	290.2	291.2	291.2	290.2	286.2	288.2							
289.6	288.5	287.3	289.9	289.6	289.7	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
289.5	288.2	287.4	289.6	289.6	289.7	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
289.4	288.1	287.6	289.6	289.5	289.5	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.0	287.7	287.7	289.4	289.3	289.3	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.2	287.0	287.0	288.5	288.4	288.5	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.4	286.4	287.0	288.5	288.4	288.5	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.9	287.4	287.2	288.3	288.2	288.1	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.5	287.4	287.2	288.3	288.2	288.1	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.6	287.3	287.2	288.3	288.2	288.1	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.5	287.2	287.1	288.2	288.1	288.0	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.4	286.4	287.0	288.5	288.4	288.5	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.9	287.4	287.2	288.3	288.2	288.1	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.5	287.3	287.2	288.3	288.2	288.1	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.6	287.2	287.1	288.2	288.1	288.0	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.4	286.4	287.0	288.5	288.4	288.5	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.9	287.4	287.2	288.3	288.2	288.1	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.5	287.3	287.2	288.3	288.2	288.1	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.6	287.2	287.1	288.2	288.1	288.0	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.5	287.1	287.0	288.2	288.1	288.0	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.4	286.4	287.0	288.5	288.4	288.5	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.9	287.4	287.2	288.3	288.2	288.1	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.5	287.3	287.2	288.3	288.2	288.1	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.6	287.2	287.1	288.2	288.1	288.0	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.5	287.1	287.0	288.2	288.1	288.0	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.4	286.4	287.0	288.5	288.4	288.5	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.9	287.4	287.2	288.3	288.2	288.1	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.5	287.3	287.2	288.3	288.2	288.1	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.6	287.2	287.1	288.2	288.1	288.0	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.5	287.1	287.0	288.2	288.1	288.0	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.4	286.4	287.0	288.5	288.4	288.5	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.9	287.4	287.2	288.3	288.2	288.1	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.5	287.3	287.2	288.3	288.2	288.1	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.6	287.2	287.1	288.2	288.1	288.0	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.5	287.1	287.0	288.2	288.1	288.0	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.4	286.4	287.0	288.5	288.4	288.5	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.9	287.4	287.2	288.3	288.2	288.1	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.5	287.3	287.2	288.3	288.2	288.1	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.6	287.2	287.1	288.2	288.1	288.0	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.5	287.1	287.0	288.2	288.1	288.0	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.4	286.4	287.0	288.5	288.4	288.5	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.9	287.4	287.2	288.3	288.2	288.1	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.5	287.3	287.2	288.3	288.2	288.1	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.6	287.2	287.1	288.2	288.1	288.0	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.5	287.1	287.0	288.2	288.1	288.0	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.4	286.4	287.0	288.5	288.4	288.5	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.9	287.4	287.2	288.3	288.2	288.1	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.5	287.3	287.2	288.3	288.2	288.1	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.6	287.2	287.1	288.2	288.1	288.0	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.5	287.1	287.0	288.2	288.1	288.0	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.4	286.4	287.0	288.5	288.4	288.5	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.9	287.4	287.2	288.3	288.2	288.1	289.2	289.2	290.2	290.2	290.2	287.2	289.2							
288.5	287.3	2																	

Table 12A — Scaling Run 240: Uncluttered 324-m<sup>3</sup> Chamber, Three 3.279-cm Nozzles

Time t (s)	Press Cyl P (atm)	T <sub>1</sub> (K)	Chamber P (atm)	Chamber Absolute Temperatures (K) at Locations /													COORDINATES		
				1	2	3	4	5	6	7	8	9	10	11	12	13	I	R	THETA Z (M) (DEC) (M)
-5	0.00	0.00	0.993	275.3	274.3	274.2	275.2	275.2	275.3	274.2	274.2	275.2	275.2	275.2	275.2	274.2	1	0.000	00 -0.586
-4	0.00	0.00	0.993	275.3	274.2	274.2	275.2	275.2	275.3	274.2	274.2	275.2	275.2	275.2	275.2	274.2	2	0.000	00 -0.293
-3	0.00	0.00	0.993	275.3	274.2	274.2	275.2	275.2	275.3	274.2	274.2	275.2	275.2	275.2	275.2	274.2	3	0.000	00 0.000
-2	0.00	0.00	0.993	275.3	274.2	274.2	275.2	275.2	275.3	274.2	274.2	275.2	275.2	275.2	275.2	274.2	4	0.000	00 0.293
-1	0.00	0.00	0.993	275.3	274.2	274.2	275.2	275.2	275.3	274.2	274.2	275.2	275.2	275.2	275.2	274.2	5	0.000	00 0.586
0.04	0.07	274.2	0.993	275.7	274.7	275.7	275.5	275.5	276.0	274.2	274.7	275.7	275.7	275.7	275.7	274.2	6	0.000	00 0.878
0.08	0.07	274.2	1.045	282.9	278.3	276.2	278.4	281.7	282.4	277.2	279.2	280.2	279.2	278.2	277.2	275.2	7	0.000	00 2.049
0.12	0.07	274.2	1.170	288.3	284.7	271.2	283.3	288.1	288.8	283.2	284.2	285.2	284.2	284.2	273.2	277.7	8	0.000	00 2.342
0.16	0.07	274.2	1.285	292.4	287.3	274.7	289.9	292.2	292.0	289.2	287.2	289.2	289.2	288.2	273.2	281.2	9	0.000	00 2.635
0.20	0.07	274.2	1.387	294.2	287.3	274.7	289.9	292.2	292.0	289.2	287.2	289.2	289.2	288.2	274.2	283.7	10	0.000	00 2.928
0.24	0.07	274.2	1.479	295.3	290.3	275.0	291.5	293.1	293.1	291.2	291.2	293.2	292.2	290.2	276.2	285.2	11	0.000	00 3.220
0.28	0.07	274.2	1.564	295.9	290.6	274.6	291.6	293.8	293.8	291.7	292.2	293.2	293.2	293.2	273.2	284.7	12	0.000	00 3.513
0.32	0.07	274.2	1.641	295.7	290.2	274.3	292.9	294.0	293.2	291.2	293.2	294.2	293.2	291.2	274.2	289.2	13	0.000	00 3.806
0.36	0.07	274.2	1.713	295.9	289.9	274.1	292.9	294.1	294.2	292.2	292.2	294.2	294.2	294.2	275.2	290.2			
0.40	0.07	274.2	1.770	296.0	289.3	274.0	293.0	294.3	293.1	292.2	292.2	293.2	293.2	293.2	274.2	290.2			
0.44	0.07	274.2	1.819	296.3	291.9	274.7	293.4	294.2	293.8	292.2	292.2	293.2	293.2	292.2	274.2	292.2			
0.48	0.07	274.2	1.875	295.2	291.5	273.9	293.2	293.6	294.4	292.2	292.2	294.2	294.2	294.2	275.2	289.7			
0.52	0.07	274.2	1.927	294.7	290.0	274.5	293.9	294.3	293.4	291.2	292.2	293.2	293.2	293.2	274.2	287.2			
0.56	0.07	274.2	1.950	293.7	290.6	279.9	293.3	293.3	293.5	292.2	291.7	292.7	292.7	291.2	281.2	288.2			
0.60	0.07	274.2	1.952	293.1	291.0	288.6	293.1	292.4	291.7	290.2	292.2	291.2	291.2	291.2	286.2	289.2			
0.64	0.07	274.2	1.931	292.2	290.0	289.6	292.4	291.7	291.5	290.2	290.2	291.2	291.2	291.2	289.2	289.2			
0.68	0.07	274.2	1.949	291.7	290.4	289.6	291.7	291.5	291.3	290.2	290.2	291.2	291.2	291.2	289.2	290.2			
0.72	0.07	274.2	1.947	291.5	290.0	289.3	291.3	290.9	290.9	290.2	290.2	291.2	291.2	291.2	289.2	290.2			
0.76	0.07	274.2	1.946	291.2	289.7	289.5	291.7	290.7	290.8	290.2	290.2	291.2	291.2	291.2	289.2	290.2			
0.80	0.07	274.2	1.945	291.0	289.5	289.4	290.4	290.0	290.6	290.2	290.2	291.2	291.2	291.2	288.2	290.2			
0.84	0.07	274.2	1.944	290.7	289.4	289.4	290.4	290.0	290.6	290.2	290.2	291.2	291.2	291.2	288.2	290.2			
0.88	0.07	274.2	1.943	290.5	289.2	289.3	290.0	289.9	290.2	289.2	289.2	290.2	290.2	290.2	288.2	289.2			
0.92	0.07	274.2	1.942	290.2	289.0	289.0	289.5	289.6	289.7	289.2	289.2	290.2	290.2	290.2	289.2	290.2			
0.96	0.07	274.2	1.938	289.8	287.7	287.8	289.3	288.8	288.9	289.2	289.2	290.2	290.2	290.2	289.2	289.2			
1.00	0.07	274.2	1.934	289.0	288.1	288.1	288.0	289.1	289.0	289.2	289.2	290.2	290.2	290.2	288.2	289.2			
1.04	0.07	274.2	1.931	288.4	287.3	287.2	288.7	288.6	288.9	289.2	289.2	290.2	290.2	290.2	287.2	288.2			
1.08	0.07	274.2	1.929	288.3	286.9	287.2	288.1	288.6	288.9	289.2	289.2	290.2	290.2	290.2	286.7	288.2			
1.12	0.07	274.2	1.927	288.5	285.7	285.5	288.0	288.5	288.7	289.2	289.2	290.2	290.2	290.2	285.2	287.2			
1.16	0.07	274.2	1.925	287.7	285.2	285.1	286.4	287.0	286.6	287.2	287.2	288.2	288.2	288.2	284.2	287.2			
1.20	0.07	274.2	1.923	287.3	284.6	284.9	286.6	287.0	286.3	286.2	286.2	287.2	287.2	287.2	283.2	286.2			
1.24	0.07	274.2	1.921	287.2	284.7	285.0	285.9	285.8	285.5	287.2	287.2	287.2	287.2	287.2	283.2	286.2			
1.28	0.07	274.2	1.920	286.5	284.7	284.8	285.9	285.8	285.6	286.2	286.2	286.2	286.2	286.2	283.2	285.2			
1.32	0.07	274.2	1.916	286.4	283.1	283.0	286.1	286.3	286.0	286.2	286.2	286.2	286.2	286.2	283.2	285.2			
1.36	0.07	274.2	1.916	286.5	283.5	283.4	286.3	286.3	286.3	286.2	286.2	286.2	286.2	286.2	283.2	285.2			
1.40	0.07	274.2	1.913	286.5	283.5	283.4	286.4	286.2	285.9	285.2	285.2	286.2	286.2	286.2	283.2	285.2			
1.44	0.07	274.2	1.911	286.1	284.9	284.8	286.0	286.0	286.0	286.0	286.0	286.2	286.2	286.2	283.2	285.2			
1.48	0.07	274.2	1.909	285.9	284.0	284.0	285.8	285.8	285.8	285.8	285.8	286.2	286.2	286.2	283.2	285.2			
1.52	0.07	274.2	1.907	285.3	284.3	284.3	285.3	285.3	285.3	285.2	285.2	286.2	286.2	286.2	283.2	285.2			
1.56	0.07	274.2	1.906	285.2	284.1	284.2	285.3	285.3	285.3	285.2	285.2	286.2	286.2	286.2	283.2	285.2			
1.60	0.07	274.2	1.904	284.9	283.9	283.9	285.0	285.0	285.0	285.0	285.0	286.2	286.2	286.2	283.2	285.2			
1.64	0.07	274.2	1.902	284.8	283.8	283.7	284.9	284.9	284.9	284.9	284.9	286.2	286.2	286.2	283.2	285.2			
1.68	0.07	274.2	1.901	284.5	283.5	283.5	284.3	284.3	284.4	284.2	284.2	286.2	286.2	286.2	283.2	285.2			
1.72	0.07	274.2	1.899	284.2	283.1	283.0	284.3	284.2	284.2	284.2	284.2	286.2	286.2	286.2	283.2	285.2			
1.76	0.07	274.2	1.897	283.7	282.7	282.7	283.0	283.0	283.0	283.0	283.0	286.2	286.2	286.2	283.2	285.2			
1.80	0.07	274.2	1.897	283.7	282.7	282.7	283.0	283.0	283.0	283.0	283.0	286.2	286.2	286.2	283.2	285.2			

Table 13A — Scaling Run 241: Cluttered 324-m<sup>3</sup> Chamber, South 3.279-cm Nozzle

Press Time	Cyl P	T <sub>i</sub> (K)	Chamber P (atm)	Chamber Absolute Temperatures (K) at Locations /													COORDINATES			
(s)	(atm)	(K)		1	2	3	4	5	6	7	8	9	10	11	12	13	R	THEIA	Z	
				(atm)													(M)	(DEC)	(M)	
-5	...	...	1.009	289.6	289.1	289.5	289.6	289.5	290.2	290.2	290.2	290.2	290.2	290.2	290.2	290.2	1	0.000	00	-0.586
-4	...	...	1.009	289.6	289.2	289.0	289.6	289.5	290.2	290.2	290.2	290.2	290.2	290.2	290.2	290.2	2	0.000	00	-0.293
-3	...	...	1.009	289.6	289.1	289.0	289.6	289.5	290.2	290.2	290.2	290.2	290.2	290.2	290.2	290.2	3	0.000	00	0.000
-2	...	...	1.009	289.6	289.1	289.0	289.6	289.5	290.2	290.2	290.2	290.2	290.2	290.2	290.2	290.2	4	0.000	00	0.293
-1	...	...	1.009	289.6	289.1	289.0	289.6	289.5	290.2	290.2	290.2	290.2	290.2	290.2	290.2	290.2	5	0.000	00	0.586
0	0.004	259	230.6	289.7	289.2	289.1	289.6	289.5	290.2	290.2	290.2	290.2	290.2	290.2	290.2	290.2	6	0.000	00	0.878
1	1.036	260	301.8	293.6	292.4	291.0	292.1	292.5	293.8	290.2	291.2	291.2	291.2	291.2	290.2	290.2	7	0.000	00	2.049
2	2.025	275.6	1.091	297.8	296.9	296.5	296.9	297.5	298.1	293.2	293.2	294.7	294.2	294.7	293.2	293.2	8	0.000	00	2.342
3	3.019	288.4	1.143	300.5	299.7	299.4	299.9	300.4	300.5	299.2	299.2	299.2	299.2	299.2	299.2	299.2	9	0.000	00	2.635
4	4.013	298.6	1.192	302.6	301.0	301.7	302.3	302.4	302.6	299.2	299.7	299.7	299.7	299.7	299.7	299.2	10	0.000	00	2.928
5	5.017	308.8	1.237	302.6	302.5	303.1	303.0	303.4	303.5	302.2	302.2	301.2	302.2	302.2	301.2	302.2	11	0.000	00	3.220
6	6.021	318.0	1.281	303.6	303.7	304.2	304.0	303.4	303.9	303.7	304.2	303.7	304.7	303.7	303.7	303.2	12	0.000	00	3.513
7	7.025	328.2	1.323	304.9	305.0	304.9	305.9	306.1	305.9	306.2	306.2	306.2	306.2	306.2	305.2	305.2	13	0.000	00	3.806
8	8.029	338.4	1.363	305.0	305.2	304.5	306.4	306.1	307.2	306.7	307.2	307.2	307.2	307.2	306.7	306.2				
9	9.033	348.6	1.402	307.4	306.7	307.0	307.3	307.3	307.4	309.2	308.2	308.2	308.2	308.2	307.2	306.2				
10	10.037	358.8	1.442	306.9	306.3	307.5	307.0	306.6	306.6	306.2	306.2	306.2	306.2	306.2	306.2	306.2				
11	11.041	369.0	1.483	307.3	307.3	307.3	308.1	307.9	307.8	310.7	310.2	309.2	308.2	311.2	309.2	307.2				
12	12.045	379.2	1.498	308.7	308.3	308.9	309.1	308.6	308.2	311.2	311.2	309.2	309.2	309.2	309.2	307.2				
13	13.049	389.4	1.531	307.0	307.0	307.8	307.5	306.6	306.1	312.2	311.2	3								

Table 14A — Scaling Run 242: Cluttered 324-m<sup>3</sup> Chamber, South 3.279-cm Nozzle[illegible]



Table 15A -- Scaling Run 243: Cluttered 324-m<sup>3</sup> Chamber, South 3.279-cm Nozzle[illegible]

Table 16A — Scaling Run 244: Cluttered 324-m<sup>3</sup> Chamber, South 3.279-cm Nozzle

Time	Cyl P (s)	Press P (atm)	T <sub>i</sub> (K)	Chamber P (atm)	Chamber Absolute Temperatures (K) at Locations /													COORDINATES		
					1	2	3	4	5	6	7	8	9	10	11	12	13	1	R (M)	THETA (DEC) (M)
-5	...	...	...	...	290	4	290	1	290	3	290	4	291	2	291	2	291	1	0.000	00 -0.586
-4	...	...	...	...	290	4	290	1	290	5	290	4	291	2	291	2	291	2	0.000	00 -0.293
-3	...	...	...	...	290	4	290	1	290	5	290	3	290	4	291	2	291	2	0.000	00 0.000
-2	...	...	...	...	290	4	290	1	290	5	290	3	290	4	291	2	291	2	0.000	00 0.293
-1	...	...	...	...	290	4	290	1	290	5	290	4	291	2	291	2	291	2	0.000	00 0.586
0	...	...	...	...	290	6	290	1	290	5	290	4	291	2	291	2	291	2	0.000	00 0.878
1	...	...	...	...	294	4	293	3	292	1	293	0	293	7	294	2	292	2	0.000	00 2.049
2	...	...	...	...	298	7	298	1	297	8	298	0	298	6	299	2	295	2	0.000	00 2.342
3	...	...	...	...	301	4	300	9	300	9	301	2	301	7	302	0	298	2	0.000	00 2.635
4	...	...	...	...	303	9	303	3	302	7	303	1	303	5	303	0	299	7	0.000	00 2.928
5	...	...	...	...	304	8	304	5	304	1	304	7	304	8	305	2	303	2	0.000	00 3.220
6	...	...	...	...	305	3	305	4	305	4	305	6	306	0	305	7	305	7	0.000	00 3.513
7	...	...	...	...	307	7	307	2	306	8	307	3	307	1	308	1	307	2	0.000	00 3.806
8	...	...	...	...	308	5	308	0	308	0	308	1	308	5	309	2	308	7	0.000	00 4.099
9	...	...	...	...	308	4	307	7	308	0	308	5	308	5	309	3	311	2	0.000	00 4.392
10	...	...	...	...	309	4	308	7	308	8	309	5	310	0	309	7	311	2	0.000	00 4.685
11	...	...	...	...	309	5	309	2	308	8	309	4	309	3	308	5	312	7	0.000	00 4.978
12	...	...	...	...	309	7	310	4	310	4	310	4	310	4	310	4	311	2	0.000	00 5.271
13	...	...	...	...	309	9	309	4	310	6	310	6	310	6	311	2	312	7	0.000	00 5.564
14	...	...	...	...	310	4	309	5	309	5	310	0	309	4	309	3	314	2	0.000	00 5.857
15	...	...	...	...	310	4	309	5	309	5	310	0	309	4	309	3	314	2	0.000	00 6.150
16	...	...	...	...	309	3	309	1	309	0	309	3	309	7	311	0	316	2	0.000	00 6.443
17	...	...	...	...	308	7	308	0	309	7	310	3	310	6	311	2	315	2	0.000	00 6.736
18	...	...	...	...	310	1	309	8	309	1	310	2	311	1	311	7	316	2	0.000	00 7.029
19	...	...	...	...	310	4	309	5	310	2	310	2	310	6	310	2	312	2	0.000	00 7.322
20	...	...	...	...	310	7	310	2	310	2	310	2	310	6	310	2	312	2	0.000	00 7.615
21	...	...	...	...	311	0	310	4	310	5	310	2	310	4	310	7	316	2	0.000	00 7.908
22	...	...	...	...	311	6	310	9	310	6	311	0	311	7	316	2	313	2	0.000	00 8.201
23	...	...	...	...	312	2	312	3	311	6	312	0	312	2	312	2	312	2	0.000	00 8.494
24	...	...	...	...	310	8	310	3	310	5	310	3	309	8	308	3	315	2	0.000	00 8.787
25	...	...	...	...	309	6	309	0	309	0	309	4	308	3	307	9	314	7	0.000	00 9.080
26	...	...	...	...	308	7	308	5	308	1	308	5	308	0	307	6	313	2	0.000	00 9.373
27	...	...	...	...	308	9	308	5	307	5	307	9	307	4	308	0	313	2	0.000	00 9.666
28	...	...	...	...	309	1	308	7	308	6	308	0	308	5	308	9	313	2	0.000	00 9.959
29	...	...	...	...	309	2	308	8	309	1	308	9	308	7	309	0	313	2	0.000	00 10.252
30	...	...	...	...	309	3	309	3	309	3	309	3	309	3	309	3	312	2	0.000	00 10.545
31	...	...	...	...	308	4	308	2	308	5	308	9	308	5	308	1	312	2	0.000	00 10.838
32	...	...	...	...	306	6	307	5	308	1	308	2	307	8	307	5	312	2	0.000	00 11.131
33	...	...	...	...	306	4	307	3	307	3	307	3	307	4	311	2	309	7	0.000	00 11.424
34	...	...	...	...	306	6	306	6	307	3	307	3	307	0	311	2	310	2	0.000	00 11.717
35	...	...	...	...	305	7	306	4	307	3	307	5	306	6	307	0	310	2	0.000	00 12.010
36	...	...	...	...	306	0	306	2	306	3	306	7	306	5	310	2	309	2	0.000	00 12.303
37	...	...	...	...	306	1	306	0	306	4	306	2	306	1	310	2	309	2	0.000	00 12.596
38	...	...	...	...	305	7	305	3	304	9	305	0	304	8	304	2	306	2	0.000	00 12.889
39	...	...	...	...	303	0	302	6	302	7	303	2	303	3	303	2	305	2	0.000	00 13.182
40	...	...	...	...	302	4	301	9	302	0	302	3	302	4	302	3	304	2	0.000	00 13.475
41	...	...	...	...	302	0	301	4	301	5	302	1	301	6	302	1	303	2	0.000	00 13.768
42	...	...	...	...	302	4	301	9	302	2	302	0	302	6	301	8	304	2	0.000	00 14.061
43	...	...	...	...	302	3	301	5	302	1	302	1	302	2	302	2	303	2	0.000	00 14.354
44	...	...	...	...	302	3	301	5	302	0	302	0	302	0	302	0	302	0	0.000	00 14.647
45	...	...	...	...	302	3	301	7	301	6	301	5	301	8	301	8	303	2	0.000	00 14.940
46	...	...	...	...	302	3	301	3	301	5	301	5	301	5	301	5	303	2	0.000	00 15.233
47	...	...	...	...	302	3	301	3	301	5	301	5	301	5	301	5	303	2	0.000	00 15.526
48	...	...	...	...	302	3	301	3	301	5	301	5	301	5	301	5	303	2	0.000	00 15.819
49	...	...	...	...	302	3	301	3	301	5	301	5	301	5	301	5	303	2	0.000	00 16.112
50	...	...	...	...	302	3	301	3	301	5	301	5	301	5	301	5	303	2	0.000	00 16.405
51	...	...	...	...	302	3	301	3	301	5	301	5	301	5	301	5	303	2	0.000	00 16.698
52	...	...	...	...	302	3	301	3	301	5	301	5	301	5	301	5	303	2	0.000	00 16.991
53	...	...	...	...	302	3	301	3	301	5	301	5	301	5	301	5	303	2	0.000	00 17.284
54	...	...	...	...	302	3	301	3	301	5	301	5	301	5	301	5	303	2	0.000	00 17.577
55	...	...	...	...	302	3	301	3	301	5	301	5	301	5	301	5	303	2	0.000	00 17.870
56	...	...	...	...	302	3	301	3	301	5	301	5	301	5	301	5	303	2	0.000	00 18.163
57	...	...	...	...	302	3	301	3	301	5	301	5	301	5	301	5	303	2	0.000	00 18.456
58	...	...	...	...	302	3	301	3	301	5	301	5	301	5	301	5	303	2	0.000	00 18.749
59	...	...	...	...	302	3	301	3	301	5	301	5	301	5	301	5	303	2	0.000	00 19.042
60	...	...	...	...	302	3	301	3	301	5	301	5	301	5	301	5	303	2	0.000	00 19.335
61	...	...	...	...	302	3	301	3	301	5	301	5	301	5	301	5	303	2	0.000	00 19.628
62	...	...	...	...	302	3	301	3	301	5	301	5	301	5	301	5	303	2	0.000	00 19.921
63	...	...	...	...	302	3	301	3	301	5	301	5	301	5	301	5	303	2	0.000	00 20.214
64	...	...	...	...	302	3	301	3	301	5	301	5	301	5	301	5	303	2	0.000	00 20.507
65	...	...	...	...	302	3	301	3	301	5	301	5	301	5	301	5	303	2	0.000	00 20.800
66	...	...	...	...	302	3	301	3	301	5	301	5	301	5	301	5	303	2	0.000	00 21.093
67	...	...	...	...	302	3	301	3	301	5	301	5	301	5	301	5	303	2	0.000	00 21.386
68	...	...	...	...	302	3	301	3	301	5	301	5	301	5	301	5	303	2	0.000	00 21.679
69	...	...	...	...	302	3	301	3	301	5	301	5	301	5	301	5	303	2	0.000	00 21.972
70	...	...	...	...	302	3	301	3	301	5	301	5	301	5	301	5	303	2	0.000	00 22.265
71	...	...	...	...	302	3	301	3	301	5	301	5	301	5	301	5	303	2	0.000	00 22.558

Table 17A — Scaling Run 245: Cluttered 324-m<sup>3</sup> Chamber, South 3.279-cm Nozzle

Press P (atm)	Time t (s)	Chamber P (atm)	T <sub>c</sub> (K)	Chamber Absolute Temperatures (K) at Locations /													COORDINATES R (m)    THETA Z (deg)		
-5	0.006	298.6	298.1	298.6	298.5	298.4	300.2	299.2	300.2	300.2	300.2	300.2	300.2	300.2	299.2	13	0.000	0.0	
-4	0.006	298.6	298.1	298.6	298.5	298.4	300.2	299.2	300.2	299.2	300.2	300.2	300.2	300.2	300.2	299.2	12	0.000	0.0
-3	0.006	298.6	298.1	298.6	298.5	298.4	300.2	299.2	300.2	299.2	300.2	300.2	300.2	300.2	300.2	299.2	11	0.000	0.0
-2	0.006	298.6	298.1	298.6	298.5	298.4	300.2	299.2	300.2	299.2	300.2	300.2	300.2	300.2	300.2	299.2	10	0.000	0.0
-1	0.006	298.6	298.1	298.6	298.5	298.4	300.2	299.2	300.2	299.2	300.2	300.2	300.2	300.2	300.2	299.2	9	0.000	0.0
0	0.006	298.6	298.1	298.6	298.5	298.4	300.2	299.2	300.2	299.2	300.2	300.2	300.2	300.2	300.2	299.2	8	0.000	0.0
1	0.027	303.0	302.7	301.5	302.4	303.1	303.8	300.2	300.2	300.2	301.2	301.2	301.2	301.2	300.2	300.2	7	0.000	0.0
2	0.093	308.2	307.2	305.2	306.0	306.5	306.4	304.2	304.2	304.2	304.2	304.2	304.2	304.2	303.2	303.2	6	0.000	0.0
3	0.146	310.8	310.0	308.4	309.6	310.2	310.2	306.2	306.2	306.2	306.2	306.2	306.2	306.2	306.2	306.2	5	0.000	0.0
4	0.195	312.4	312.0	311.5	311.1	311.0	312.2	312.0	312.0	308.7	311.2	311.7	311.7	311.7	309.7	309.7	4	0.000	0.0
5	0.233	314.5	313.1	314.3	313.8	313.8	313.5	311.0	310.5	311.2	313.5	313.2	313.5	313.2	311.0	310.5	3	0.000	0.0
6	0.286	315.6	313.0	314.4	314.7	315.2	315.2	314.2	314.2	312.7	315.7	315.7	315.7	315.7	312.7	312.7	2	0.000	0.0
7	0.329	316.5	315.9	316.2	316.3	316.7	316.8	315.2	314.2	314.2	317.2	317.2	317.2	317.2	314.2	314.2	1	0.000	0.0
8	0.356	316.5	316.1	316.7	316.5	315.9	315.6	315.2	315.2	317.2	318.2	318.2	318.2	318.2	316.2	316.2			
9	0.356	316.2	316.0	316.6	316.9	316.9	316.9	316.9	317.2	316.7	316.7	316.7	316.7	316.7	316.7	316.7			
10	0.434	317.0	316.5	316.9	317.0	316.9	316.9	316.9	317.2	316.7	316.7	316.7	316.7	316.7	316.7	316.7			
11	0.471	318.5	317.7	317.3	317.9	318.1	317.8	323.2	318.2	320.7	320.7	320.7	320.7	320.7	316.7	316.7			
12	0.506	318.7	318.1	318.0	317.9	318.2	318.0	323.2	319.2	321.2	321.2	321.2	321.2	321.2	319.2	319.2			
13	0.540	318.7	318.2	318.7	319.5	319.2	319.2	323.2	321.2	323.2	321.2	321.2	321.2	321.2	319.2	319.2			
14	0.573	319.4	319.0	319.3	319.6	319.1	319.0	323.2	321.2	323.2	321.2	321.2	321.2	321.2	319.2	319.2			
15	0.594	319.4	319.0	319.3	319.6	319.1	319.0	323.2	321.2	323.2	321.2	321.2	321.2	321.2	319.2	319.2			
16	0.635	316.8	317.3	318.1	318.6	319.2	319.5	323.2	322.2	322.2	322.2	322.2	322.2	322.2	320.2	320.2			
17	0.685	317.3	318.1	318.5	319.3	320.0	319.7	326.7	324.2	323.2	323.2	323.2	323.2	323.2	320.2	320.2			
18	0.713	319.8	319.4	319.7	319.4	319.9	319.6	322.2	324.2	322.2	323.2	323.2	323.2	323.2	322.2	322.2			
19	0.741	319.0	319.9	319.3	319.2	318.1	317.1	322.2	325.7	323.2	323.2	323.2	323.2	323.2	320.2	320.2			
20	0.767	318.3	317.9	317.9	318.2	317.8	317.7	322.2	325.7	323.2	323.2	323.2	323.2	323.2	320.2	320.2			
21	0.784	318.1	317.7	317.3	317.8	317.6	317.3	328.2	327.2	323.2	324.2	322.2	322.2	322.2	321.2	321.2			
22	0.810	317.3	317.3	318.5	318.2	317.8	317.8	317.8	328.2	327.2	323.2	324.2	322.2	322.2	321.2	321.2			
23	0.834	317.8	318.1	317.9	318.6	318.6	319.0	324.2	326.2	324.2	324.2	323.2	323.2	323.2	320.2	320.2			
24	0.858	318.2	318.0	318.5	318.8	317.5	317.3	326.2	325.2	323.2	324.2	322.2	322.2	322.2	320.2	320.2			
25	0.881	318.0	317.8	317.9	318.4	318.0	319.0	326.2	324.2	323.2	324.2	322.2	322.2	322.2	320.2	320.2			
26	0.903	317.6	318.6	318.7	319.4	319.8	320.9	323.2	324.2	323.2	324.2	322.2	322.2	322.2	320.2	320.2			
27	0.924	315.6	315.6	316.6	317.4	319.0	318.8	324.2	324.2	323.2	324.2	322.2	322.2	322.2	320.2	320.2			
28	0.938	316.0	316.3	317.3	317.8	317.5	317.4	324.2	323.2	323.2	324.2	322.2	322.2	322.2	320.2	320.2			
29	0.953	316.4	316.2	316.6	318.0	317.8	317.7	323.7	323.7	323.2	322.2	322.2	322.2	322.2	320.2	320.2			
30	0.962	315.3	315.4	316.0	316.9	316.5	316.9	323.2	323.2	323.2	320.2	320.2	319.2	317.2	317.2	317.2			
31	0.966	315.4	314.9	315.1	316.3	316.5	315.9	322.7	321.7	319.7	319.7	319.2	317.2	317.2	317.2	317.2			
32	0.968	315.3	314.6	314.7	315.6	315.4	315.3	321.2	320.2	319.2	319.2	318.2	317.2	317.2	317.2	317.2			
33	0.968	315.1	314.7	314.5	315.3	315.1	315.2	319.7	319.7	318.7	318.7	318.2	317.2	317.2	317.2	317.2			
34	0.969	314.7	314.3	314.4	314.9	314.7	314.6	320.2	319.2	318.7	318.7	318.2	317.2	317.2	317.2	317.2			
35	0.969	314.3	313.8	314.3	314.6	314.4	314.9	319.2	318.2	318.2	318.2	318.2	316.2	316.2	316.2	316.2			
36	0.969	314.4	313.8	313.5	314.5	314.4	314.3	319.2	318.2	318.2	318.2	318.2	316.2	316.2	316.2	316.2			
37	0.969	314.3	313.8	313.5	314.5	314.4	314.3	319.2	318.2	318.2	318.2	318.2	316.2	316.2	316.2	316.2			
38	0.968	314.3	313.8	313.5	314.5	314.4	314.3	319.2	318.2	318.2	318.2	318.2	316.2	316.2	316.2	316.2			
39	0.968	314.3	313.8	313.5	314.5	314.4	314.3	319.2	318.2	318.2	318.2	318.2	316.2	316.2	316.2	316.2			
40	0.964	312.3	311.7	311.8	312.4	312.3	312.2	317.7	316.2	316.2	316.2	316.2	314.2	314.2	314.2	314.2			
41	0.961	312.0	310.9	311.1	311.1	311.3	310.8	316.2	313.7	316.2	315.5	314.7	311.5	312.0	312.0	312.0			
42	0.959	311.6	310.7	310.1	310.0	310.2	310.0	315.2	313.2	313.2	314.2	313.2	312.2	311.2	311.2	311.2			
43	0.956	310.7	310.3	310.2	309.8	310.1	310.4	314.2	312.2	312.2	313.2	313.2	312.2	311.2	311.2	311.2			
44	0.955	310.5	309.6	309.9	309.8	310.1	310.0	313.2	312.2	312.2	313.2	313.2	312.2	311.2	311.2	311.2			
45	0.953	310.0	309.6	309.9	310.0	310.2	309.6	312.2	311.2	311.2	312.2	312.2	311.2	311.2	311.2	311.2			
46	0.951	310.2	309.5	309.5	309.7	309.8	309.5	312.2	311.2	311.2	312.2	312.2	311.2	311.2	311.2	311.2			
47	0.950	310.2	309.5	309.5	309.7	309.8	309.5	312.2	311.2	311.2	312.2	312.2	311.2	311.2	311.2	311.2			
48	0.949	310.2	309.7	309.7	309.8	309.9	309.6	312.2	311.2	311.2	312.2	312.2	311.2	311.2	311.2	311.2			
49	0.947	310.5	310.0	310.0	310.2	310.0	309.9	311.2	310.2	310.2	311.2	311.2	310.2	310.2	310.2	310.2			
50	0.945	310.6	309.8	309.6	309.4	310.2	310.1	311.2	310.2	311.2	311.2	311.2	310.2	310.2	310.2	310.2			

Table 18A — Scaling Run 246: Cluttered 324-m<sup>3</sup> Chamber, South 3.279-cm Nozzle

Time t (s)	Press P (atm)	Cyl P (atm)	T <sub>1</sub> (K)	Chamber P (atm)	Chamber Absolute Temperatures (K) at Locations /													COORDINATES		
					1	2	3	4	5	6	7	8	9	10	11	12	13	I	R (CM)	THETA (DEG)
-5	...	...	...	1.005	289.0	288.6	288.5	288.9	288.9	288.8	289.0	289.2	289.2	289.0	289.2	289.2	1	0.000	00	-0.586
-4	...	...	...	1.005	289.0	288.6	288.5	288.9	288.9	288.8	289.0	289.2	289.2	289.0	289.2	289.2	2	0.000	00	-0.293
-3	...	...	...	1.005	289.0	288.6	288.5	288.9	288.9	288.8	289.0	289.2	289.2	289.0	289.2	289.2	3	0.000	00	0.000
-2	...	...	...	1.005	289.0	288.6	288.5	288.9	288.9	288.8	289.0	289.2	289.2	289.0	289.2	289.2	4	0.000	00	0.293
-1	...	...	...	1.005	289.0	288.6	288.5	288.9	288.9	288.8	289.0	289.2	289.2	289.0	289.2	289.2	5	0.000	00	0.586
0.02	412	230.4	...	1.005	289.1	288.6	288.5	288.9	288.9	288.8	289.0	289.2	289.2	289.0	289.2	289.2	6	0.000	00	0.878
1.03	361	239.6	...	1.031	292.9	291.6	290.5	291.3	291.7	292.1	290.2	291.2	291.2	291.2	291.2	290.2	7	0.000	00	2.049
2.03	319	235.0	...	1.005	297.1	295.9	294.7	295.6	296.3	295.7	293.2	292.7	294.7	294.7	294.7	293.2	8	0.000	00	2.342
3.00	284	248.4	...	1.136	299.8	298.7	298.5	299.2	299.2	299.9	296.2	296.2	298.2	298.2	298.2	297.2	9	0.000	00	2.635
4.00	264	249.9	...	1.183	302.2	301.2	301.1	301.5	301.7	301.5	299.7	297.7	300.2	300.7	301.2	299.2	10	0.000	00	2.928
5.00	249	252.9	...	1.228	303.1	302.4	302.1	302.4	303.0	303.5	301.2	300.2	302.2	302.2	303.2	303.2	11	0.000	00	3.220
6.00	230	253.1	...	1.270	304.9	304.0	304.0	304.2	304.2	304.2	303.7	302.2	304.7	304.7	304.7	302.2	12	0.000	00	3.513
7.00	215	261.1	...	1.312	305.1	304.4	304.8	305.3	305.7	305.3	305.2	305.7	306.2	306.2	307.2	307.2	13	0.000	00	3.606
8.00	200	261.7	...	1.351	305.1	304.5	304.6	305.2	305.7	305.3	306.2	305.7	307.7	307.7	307.2	305.2				
9.00	185	259.8	...	1.389	305.4	305.4	305.2	305.1	306.4	306.4	306.4	308.2	307.2	308.2	308.2	305.2				
10.00	169	258.5	...	1.425	305.2	305.3	305.7	307.1	307.1	307.5	310.7	308.2	307.2	308.2	308.2	306.2				
11.00	154	258.2	...	1.460	306.8	306.3	306.8	307.4	307.8	308.4	311.2	310.2	309.2	309.2	309.2	307.2				
12.00	138	257.7	...	1.482	307.9	307.0	306.7	307.7	308.5	309.4	313.2	313.2	310.2	310.2	310.2	308.2				
13.00	122	256.7	...	1.515	309.4	308.7	308.5	308.9	309.5	310.0	313.2	312.7	310.7	310.2	310.2	308.7				
14.00	106	255.6	...	1.547	309.7	307.7	307.8	308.7	309.8	310.9	315.2	313.2	311.2	311.2	311.2	310.2				
15.00	90	255.1	...	1.578	308.5	307.6	307.1	308.0	307.9	307.6	314.7	314.2	311.7	311.2	311.2	309.7				
16.00	74	254.3	...	1.608	307.7	306.7	307.1	307.6	307.0	306.8	314.2	313.2	311.2	311.2	311.2	309.2				
17.00	58	254.0	...	1.636	307.4	307.0	306.8	307.9	307.3	306.8	314.7	313.2	311.2	310.7	310.2	308.7				
18.00	42	253.4	...	1.664	307.8	307.2	306.8	307.8	308.1	308.0	313.2	312.2	311.2	311.2	311.2	309.2				
19.00	26	253.6	...	1.682	308.0	307.8	308.1	308.2	308.5	308.0	313.2	312.2	311.2	311.2	311.2	309.2				
20.00	10	251.5	...	1.709	309.3	308.3	308.6	308.9	309.1	309.2	314.2	312.2	312.2	312.2	312.2	309.7				
21.00	210	250.4	...	1.735	308.4	308.8	309.2	308.8	309.3	309.1	315.2	313.2	312.2	312.2	311.2	310.2				
22.00	52	250.4	...	1.760	307.8	308.7	309.5	309.5	308.1	308.1	315.7	312.2	312.2	311.7	311.2	309.7				
23.00	21	249.3	...	1.784	307.3	306.8	307.2	307.4	307.0	306.9	315.2	315.2	312.2	312.2	310.2	309.2				
24.00	351	248.3	...	1.807	306.6	306.4	306.4	307.1	306.8	306.6	316.7	316.2	312.2	312.2	310.7	309.2				
25.00	374	247.9	...	1.830	307.0	306.8	307.3	307.7	307.8	307.5	318.2	315.2	312.2	311.2	310.2	309.2				
26.00	626	247.5	...	1.845	306.5	305.9	306.1	306.3	306.7	308.1	318.2	314.2	311.2	311.2	310.2	308.2				
27.00	375	246.9	...	1.868	307.9	307.0	306.8	307.1	307.1	306.6	317.7	314.2	311.7	311.7	311.7	308.2				
28.00	537	246.4	...	1.889	308.5	307.7	307.7	307.5	307.9	308.0	317.2	314.2	311.2	311.2	312.2	310.2				
29.00	591	245.1	...	1.910	305.5	305.7	306.6	307.5	307.1	305.3	315.7	312.7	312.2	311.7	311.2	310.2				
30.00	558	244.0	...	1.930	306.4	306.0	306.1	306.8	306.8	306.6	315.2	313.2	311.2	311.2	312.2	310.2				
31.00	519	243.6	...	1.947	305.5	305.2	306.2	306.5	306.7	305.4	315.2	312.7	311.7	311.2	311.7	310.2				
32.00	461	243.2	...	1.957	304.9	304.9	305.1	305.3	305.6	305.5	315.2	311.2	310.2	310.2	310.2	308.2				
33.00	...	...	...	1.961	304.9	304.5	304.9	305.5	306.1	305.7	313.2	310.2	309.2	309.2	310.2	309.2				
34.00	...	...	...	1.964	304.5	304.0	304.3	304.8	304.8	304.9	313.2	310.7	309.7	309.2	309.2	307.7				
35.00	...	...	...	1.966	303.8	303.6	304.0	304.7	304.6	305.2	312.2	310.2	309.2	308.2	308.2	307.2				
36.00	...	...	...	1.967	303.5	303.1	303.1	303.7	303.9	303.9	311.2	309.2	308.2	308.2	307.7	306.2				
37.00	...	...	...	1.967	303.8	303.1	303.0	303.3	303.2	303.3	309.7	309.2	308.2	307.2	306.7	304.7				
38.00	...	...	...	1.966	303.8	303.1	302.9	303.0	303.1	303.1	309.2	309.2	308.2	307.2	306.2	303.2				
39.00	...	...	...	1.966	303.7	303.1	302.9	303.0	303.1	303.1	309.2	309.2	308.2	307.2	306.2	303.2				
40.00	...	...	...	1.966	302.3	302.2	301.8	303.0	303.1	302.7	306.2	305.7	304.2	305.2	304.2	302.2				
41.00	...	...	...	1.963	302.3	302.2	301.8	303.0	303.1	302.7	306.2	305.7	304.2	305.2	304.2	302.2				
42.00	...	...	...	1.960	300.4	300.0	300.1	300.3	300.9	300.4	304.2	304.2	304.2	304.2	305.2	303.2				
43.00	...	...	...	1.958	300.2	299.4	299.4	299.5	300.2	299.5	304.2	304.2	304.2	304.2	305.2	303.2				
44.00	...	...	...	1.956	300.4	299.9	299.8	300.0	299.9	299.7	304.2	304.2	304.2	304.2	305.2	303.2				
45.00	...	...	...	1.954	300.9	300.4	300.3	300.4	300.2	299.9	303.2	303.2	303.2	303.2	303.2	302.2				
46.00	...	...	...	1.954	300.6	300.6	300.6	300.7	300.4	300.3	302.2	302.2	302.2	302.2	302.2	301.2				
47.00	...	...	...	1.953	300.6	300.6	300.6	300.7	300.4	300.3	302.2	302.2	302.2	302.2	302.2	301.2				
48.00	...	...	...	1.951	300.2	300.0	299.9	300.0	300.5	300.3	302.2	301.2	302.2	301.2	302.2	301.2				
49.00	...	...	...	1.950	300.0	299.7	299.7	299.8	299.7	300.2	302.2	301.2	302.2	301.2	302.2	301.2				
50.00	...	...	...	1.949	299.9	299.7	299.7	299.7	299.6	299.7	302.2	301.2	302.2	301.2	302.2	301.2				

Table 19A – Scaling Run 247: Cluttered 324--m<sup>3</sup> Chamber, South 3.279-cm Nozzle

Time t (s)	Press P (atm)	Chamber P (atm)	T <sub>1</sub> (K)	Chamber Absolute Temperatures (K) at Locations /													COORDINATES					
				1	2	3	4	5	6	7	8	9	10	11	12	13	R (M)	THETA (DEG)	Z (M)			
-5	...	1.000	...	291.0	291.4	291.3	291.7	291.7	291.5	292.2	291.2	291.2	293.2	293.2	292.2	292.2	292.2	292.2	1	0.000	00	-0.586
-4	...	1.000	...	291.8	291.4	291.3	291.7	291.7	291.5	292.2	291.2	291.2	293.2	293.2	292.2	292.2	292.2	292.2	2	0.000	00	-0.293
-3	...	1.000	...	291.9	291.4	291.3	291.7	291.7	291.5	292.2	291.2	291.2	293.2	293.2	292.2	292.2	292.2	292.2	3	0.000	00	0.000
-2	...	1.000	...	291.8	291.4	291.3	291.7	291.7	291.5	292.2	291.2	291.2	293.2	293.2	292.2	292.2	292.2	292.2	4	0.000	00	0.293
-1	...	1.000	...	292.1	291.5	291.3	291.7	291.7	291.5	292.2	291.2	291.2	293.2	293.2	292.2	292.2	292.2	292.2	5	0.000	00	0.586
0	...	1.016	...	295.0	293.0	293.0	293.0	293.0	294.4	295.0	292.2	292.2	293.2	293.2	292.2	292.2	292.2	292.2	6	0.000	00	0.878
1	...	1.073	...	299.0	297.0	297.1	296.6	297.6	298.3	299.4	296.2	296.2	295.7	295.7	296.7	295.2	295.2	295.2	7	0.000	00	2.049
2	...	1.126	...	302.5	301.6	301.6	301.3	302.6	302.3	302.6	299.7	299.7	300.2	300.2	301.2	299.2	298.2	298.2	8	0.000	00	2.342
3	...	1.175	...	305.1	304.2	303.6	304.2	304.8	305.1	306.7	305.7	305.7	302.2	302.2	302.7	301.2	300.7	300.7	9	0.000	00	2.635
4	...	1.221	...	306.1	305.7	305.8	306.1	306.4	306.5	307.2	306.2	306.2	303.2	303.2	304.2	303.2	303.2	303.2	10	0.000	00	2.928
5	...	1.266	...	306.8	306.0	306.6	307.5	308.5	308.1	304.7	304.7	306.2	306.2	306.2	306.7	305.7	304.7	304.7	11	0.000	00	3.220
6	...	1.311	...	307.9	307.1	306.9	308.4	309.8	308.1	307.2	306.2	308.2	308.2	308.2	308.2	307.2	306.2	306.2	12	0.000	00	3.513
7	...	1.355	...	309.0	308.5	308.8	309.3	309.8	309.5	308.2	307.2	309.2	309.2	309.2	309.2	307.2	306.2	306.2	13	0.000	00	3.806
8	...	1.374	...	310.0	310.1	310.2	310.6	311.0	311.2	310.2	308.7	310.2	310.2	310.2	310.7	307.7	307.7	307.7				
9	...	1.412	...	311.2	309.6	309.0	309.4	309.6	309.5	312.2	310.2	312.2	312.2	312.2	312.2	309.2	309.2	309.2				
10	...	1.449	...	309.5	309.2	309.2	310.1	310.8	310.2	312.0	312.7	311.2	312.7	312.7	312.7	309.2	309.2	309.2				
11	...	1.483	...	309.7	309.3	310.4	310.4	311.2	311.0	314.2	312.7	311.2	312.7	312.7	312.7	309.2	309.2	309.2				
12	...	1.517	...	309.7	308.8	310.0	310.7	312.0	311.7	316.2	313.7	313.7	313.7	313.7	314.2	311.2	311.7	311.7				
13	...	1.550	...	311.2	310.7	310.7	311.2	312.0	312.0	312.0	313.2	313.2	313.2	313.2	314.2	313.2	313.2	313.2				
14	...	1.582	...	314.0	312.0	312.6	311.6	311.4	311.5	318.7	316.7	314.7	314.7	313.7	314.7	313.7	311.7	311.7				
15	...	1.613	...	310.7	309.7	310.0	311.2	311.0	312.0	321.2	317.2	315.2	314.2	314.2	314.2	311.2	310.2	310.2				
16	...	1.632	...	310.4	310.2	310.3	311.4	313.1	314.2	321.2	316.2	315.2	315.2	315.2	314.2	310.2	310.2	310.2				
17	...	1.661	...	311.6	311.2	310.2	312.7	314.1	314.0	321.2	318.2	315.2	315.2	315.2	314.2	311.2	311.2	311.2				
18	...	1.689	...	310.0	311.1	311.4	311.0	311.5	311.5	321.2	320.2	316.2	315.2	315.2	316.2	314.2	314.2	314.2				
19	...	1.717	...	312.0	311.7	312.4	312.0	311.5	311.3	321.7	317.2	314.7	314.7	314.7	314.2	312.7	312.2	312.2				
20	...	1.743	...	312.4	311.3	310.9	311.2	310.5	311.2	320.2	313.2	314.2	313.2	313.2	313.2	312.2	311.2	311.2				
21	...	1.769	...	311.6	311.2	310.9	311.3	311.6	311.3	320.7	315.7	314.2	313.2	313.2	312.7	310.7	310.7	310.7				
22	...	1.794	...	309.7	310.0	309.5	310.6	310.1	310.2	321.2	315.2	314.2	313.2	313.2	313.2	310.2	311.2	311.2				
23	...	1.810	...	310.9	310.8	310.2	310.9	310.7	311.0	320.2	315.2	313.2	313.2	313.2	313.2	312.2	312.2	312.2				
24	...	1.834	...	309.3	309.4	309.4	310.1	309.5	309.0	320.2	316.7	314.2	314.2	314.2	314.2	312.7	313.2	313.2				
25	...	1.857	...	309.7	308.9	308.5	310.2	310.2	309.5	320.2	318.2	315.2	315.2	315.2	316.2	314.2	313.2	313.2				
26	...	1.880	...	310.2	309.5	309.6	309.7	310.0	310.0	319.7	318.7	315.7	314.7	314.7	314.7	313.2	312.7	312.7				
27	...	1.902	...	311.6	311.0	310.9	310.7	310.5	310.3	320.2	317.2	315.2	314.2	314.2	314.2	313.2	311.2	311.2				
28	...	1.917	...	311.7	311.7	311.3	311.7	311.9	312.1	320.2	317.2	314.2	314.2	314.2	314.2	313.2	312.2	311.2				
29	...	1.937	...	311.0	310.5	310.5	311.2	310.9	309.4	319.2	317.2	314.2	313.2	313.2	313.2	312.7	309.7	309.7				
30	...	1.952	...	310.7	310.4	310.6	310.3	308.8	309.1	320.2	315.2	314.2	313.2	313.2	313.2	312.2	310.2	309.2				
31	...	1.960	...	310.5	310.2	309.6	309.3	308.5	308.7	317.2	314.2	313.2	312.2	312.2	312.2	309.7	309.7	309.7				
32	...	1.966	...	309.0	309.4	309.3	309.2	308.7	308.5	314.2	313.2	312.2	312.2	312.2	311.2	310.2	310.2	310.2				
33	...	1.966	...	309.0	308.7	308.8	308.8	308.4	308.1	313.2	312.7	312.2	312.2	312.2	310.7	309.2	310.2	310.2				
34	...	1.967	...	308.6	308.3	308.3	308.5	308.4	308.2	313.2	312.2	312.2	312.2	312.2	311.2	309.2	309.2	309.2				
35	...	1.968	...	308.3	308.1	308.1	308.3	308.2	308.1	313.2	312.2	312.2	312.2	312.2	311.2	309.2	308.2	308.2				
36	...	1.968	...	308.0	307.6	307.9	308.1	307.9	307.8	312.7	311.7	310.7	311.2	311.2	311.2	309.2	309.2	309.2				
37	...	1.967	...	308.0	307.7	307.7	308.0	307.6	307.6	311.2	310.2	310.2	310.2	310.2	310.2	309.2	308.2	308.2				
38	...	1.967	...	307.5	307.5	307.6	307.6	307.3	307.3	307.2	311.2	310.2	310.2	310.2	310.2	309.2	308.2	308.2				
39	...	1.966	...	306.7	306.7	306.8	307.2	306.7	306.7	306.1	311.2	310.2	310.2	310.2	310.2	309.7	308.7	308.2				
40	...	1.963	...	306.7	306.7	306.8	307.2	306.7	306.7	306.1	311.2	310.2	310.2	310.2	310.2	309.7	308.7	308.2				
41	...	1.960	...	305.4	305.2	304.6	305.3	305.1	305.1	307.2	307.2	305.2	305.2	305.2	306.2	303.2	305.2	305.2				
42	...	1.958	...	304.2	303.4	303.2	303.8	303.4	303.3	307.2	306.2	306.2	306.2	306.2	306.2	306.2	303.2	305.2				
43	...	1.956	...	303.4	302.9	302.8	302.9	302.9	302.9	306.2	305.2	305.2	305.2	305.2	305.2	305.2	303.2	305.2				
44	...	1.954	...	303.1	302.7	302.9	302.9	302.9	302.9	306.2	305.2	305.2	305.2	305.2	305.2	305.2	303.2	305.2				
45	...	1.953	...	303.1	302.6	302.7	303.1	303.1	303.1	306.2	305.2	305.2	305.2	305.2	305.2	305.2	303.2	305.2				
46	...	1.951	...	303.2	302.7	302.7	303.1	303.1	303.1	306.2	305.2	305.2	305.2	305.2	305.2	305.2	303.2	305.2				
47	...	1.950	...	303.5	302.9	302.8	303.1	303.0	303.0	306.2	305.2	305.2	305.2	305.2	305.2	305.2	303.2	305.2				
48	...	1.949	...	303.9	303.1	303.1	303.0	302.7	302.5	304.2	304.2	304.2	304.2	304.2	304.2	304.2	302.2	305.2				
49	...	1.947	...	303.8	303.3	303.0	303.1	302.5	302.5	304.2	304.2	304.2	304.2	304.2	304.2	304.2	302.2	305.2				

Table 20A — Scaling Run 248: Cluttered 324—m<sup>3</sup> Chamber, South 3.279-cm Nozzle

Time T (s)	Cyl P (atm)	Press P (atm)	Chamber P (atm)	T (K)	Chamber Absolute Temperatures (K) at Locations /													COORDINATES		
					1	2	3	4	5	6	7	8	9	10	11	12	13	I	R	THETA Z (M) (DEG) (M)
-5	...	...	...	...	295.7	295.2	295.2	295.6	295.5	295.4	296.2	295.2	296.2	296.2	296.2	296.2	295.2	1	0.000	00 -0.586
-4	...	...	...	...	295.7	295.2	295.2	295.6	295.5	295.4	296.2	295.2	296.2	296.2	296.2	296.2	295.2	2	0.000	00 -0.293
-3	...	...	...	...	295.7	295.2	295.2	295.6	295.5	295.4	296.2	295.2	296.2	296.2	296.2	296.2	295.2	3	0.000	00 0.000
-2	...	...	...	...	295.7	295.2	295.2	295.6	295.5	295.4	296.2	295.2	296.2	296.2	296.2	296.2	295.2	4	0.000	00 0.293
-1	...	...	...	...	295.7	295.2	295.2	295.6	295.5	295.4	296.2	295.2	296.2	296.2	296.2	296.2	295.2	5	0.000	00 0.586
0.000	...	...	...	...	296.4	295.6	295.2	295.7	295.9	303.1	296.7	296.2	296.2	296.2	296.2	296.2	295.2	6	0.000	00 0.878
0.090	...	...	...	...	303.1	302.3	301.3	302.0	302.9	303.1	296.7	296.2	297.2	297.2	297.2	296.2	296.2	7	0.000	00 2.049
0.180	...	...	...	...	305.1	304.5	304.2	304.4	305.1	305.1	299.2	298.2	301.2	301.2	302.2	300.2	300.2	8	0.000	00 2.342
0.270	...	...	...	...	306.7	305.9	305.9	306.1	307.1	307.1	301.7	301.7	303.7	304.2	304.2	302.7	302.7	9	0.000	00 2.635
0.360	...	...	...	...	309.5	308.6	308.4	309.7	309.3	309.3	304.2	304.2	306.2	306.2	306.2	305.2	305.2	10	0.000	00 2.928
0.450	...	...	...	...	310.5	309.5	309.5	309.6	309.8	310.2	307.2	306.2	308.7	309.2	309.2	308.2	308.2	11	0.000	00 3.220
0.540	...	...	...	...	311.6	310.9	310.4	311.3	311.7	311.6	309.2	308.2	310.2	311.2	312.2	310.2	311.2	12	0.000	00 3.513
0.630	...	...	...	...	312.2	311.8	311.5	312.3	313.0	313.0	311.7	310.7	312.7	313.2	313.7	312.7	312.2	13	0.000	00 3.806
0.720	...	...	...	...	312.9	312.9	313.5	314.2	314.6	314.2	313.2	311.2	313.2	314.2	314.2	314.2	313.2			
0.810	...	...	...	...	313.6	313.5	313.8	314.4	314.9	314.7	314.2	313.2	316.2	316.2	316.2	314.2	313.2			
0.900	...	...	...	...	314.3	314.0	314.7	314.9	314.9	314.9	314.2	313.2	316.2	316.2	316.2	314.2	313.2			
0.990	...	...	...	...	314.9	313.2	314.7	314.7	314.3	314.3	314.2	313.2	316.2	316.2	316.2	314.2	313.2			
1.080	...	...	...	...	315.2	314.0	313.9	314.7	314.6	315.1	316.7	315.7	316.2	316.2	317.2	317.2	314.2			
1.170	...	...	...	...	314.6	314.3	314.5	315.1	315.6	315.4	316.2	316.2	316.2	316.2	317.2	317.2	315.2			
1.260	...	...	...	...	315.2	314.5	313.8	314.4	314.9	314.7	316.7	316.7	317.2	317.2	317.2	316.2	314.2			
1.350	...	...	...	...	315.1	314.9	314.0	314.2	313.6	315.2	320.2	317.2	318.2	317.2	316.2	315.2	315.2			
1.440	...	...	...	...	316.1	315.6	315.4	315.5	315.5	315.5	320.2	316.2	318.2	317.2	316.2	315.2	316.2			
1.530	...	...	...	...	315.2	316.4	316.6	316.7	316.7	317.2	320.2	317.2	318.2	317.2	317.2	315.2	316.2			
1.620	...	...	...	...	315.0	313.4	313.2	313.4	313.5	313.7	322.7	319.7	318.7	317.7	316.7	315.7	316.2			
1.710	...	...	...	...	315.2	314.6	314.1	313.8	313.2	314.2	322.7	319.7	318.7	317.7	316.7	315.7	316.2			
1.800	...	...	...	...	314.7	313.8	313.8	314.0	314.0	313.1	324.2	321.2	320.2	319.2	318.2	318.2	317.2			
1.890	...	...	...	...	315.0	314.2	313.8	314.0	314.0	313.1	323.2	320.2	319.2	318.2	318.2	318.2	317.2			
1.980	...	...	...	...	315.8	315.6	315.5	315.1	315.2	315.8	322.2	319.2	319.2	318.2	319.2	318.2	317.2			
2.070	...	...	...	...	316.1	315.2	315.1	315.1	314.5	314.5	321.2	319.2	318.2	317.2	317.2	316.2	315.2			
2.160	...	...	...	...	315.2	314.5	316.5	315.5	315.5	315.6	320.7	319.2	318.2	317.2	317.2	317.2	317.2			
2.250	...	...	...	...	314.6	314.5	314.4	315.1	314.6	314.6	319.2	319.2	319.2	319.2	319.2	318.2	318.2			
2.340	...	...	...	...	314.6	314.2	314.6	315.2	315.2	315.3	320.2	319.2	319.2	319.2	319.2	318.2	316.2			
2.430	...	...	...	...	314.4	313.6	313.4	313.8	313.4	314.0	320.2	319.2	318.2	318.2	319.2	318.2	316.2			
2.520	...	...	...	...	312.0	312.3	312.8	313.4	314.0	314.6	321.2	319.2	318.2	318.2	319.2	317.2	315.2			
2.610	...	...	...	...	312.9	313.6	314.4	314.6	315.2	315.4	321.2	319.2	318.2	318.2	317.2	317.2	314.2			
2.700	...	...	...	...	312.7	312.3	313.5	313.7	313.8	314.1	322.2	319.2	318.2	318.2	318.2	316.2	316.2			
2.790	...	...	...	...	312.9	312.3	312.4	312.2	313.2	313.1	321.2	318.2	318.2	317.2	317.2	315.2	315.2			
2.880	...	...	...	...	313.1	312.6	312.7	313.0	312.3	312.0	321.2	318.2	318.2	317.2	317.2	315.2	315.2			
2.970	...	...	...	...	313.3	312.5	312.6	312.7	312.5	311.9	321.2	317.2	316.7	316.2	316.2	315.2	315.2			
3.060	...	...	...	...	313.0	312.3	312.5	312.8	312.8	312.6	321.2	317.2	316.2	316.2	315.2	315.2	314.2			
3.150	...	...	...	...	311.9	311.6	311.5	311.8	311.8	312.2	316.7	315.7	315.2	315.2	315.2	314.2	314.2			
3.240	...	...	...	...	310.8	310.6	310.7	311.4	311.1	312.3	315.2	314.2	314.2	314.2	314.2	313.2	312.2			
3.330	...	...	...	...	310.9	310.5	311.1	311.6	311.6	311.8	316.2	315.2	314.2	314.2	313.2	312.2	312.2			
3.420	...	...	...	...	310.9	310.7	310.8	311.5	311.2	311.6	316.2	315.2	314.2	314.2	313.2	312.2	312.2			
3.510	...	...	...	...	310.2	309.9	309.3	310.2	310.0	309.5	313.7	312.2	312.7	312.7	312.7	311.2	311.2			
3.600	...	...	...	...	308.4	308.0	307.8	308.0	307.6	307.6	312.2	310.2	310.7	311.7	311.2	310.2	309.2			
3.690	...	...	...	...	308.1	307.3	307.6	307.0	306.9	307.1	311.2	310.2	309.2	311.2	310.2	309.2	308.2			
3.780	...	...	...	...	307.5	307.2	307.2	307.3	307.5	306.7	310.2	309.2	309.2	309.2	309.2	308.2	308.2			
3.870	...	...	...	...	307.3	306.9	306.6	306.8	307.0	306.9	309.2	308.2	308.2	308.2	308.2	306.2	306.2			
3.960	...	...	...	...	306.8	306.2	306.6	307.0	306.6	307.0	308.2	307.2	308.2	308.2	307.2	306.2	306.2			
4.050	...	...	...	...	307.0	306.1	305.9	306.4	307.1	307.0	308.2	306.2	308.2	308.2	307.2	305.2	306.2			
4.140	...	...	...	...	306.7	306.6	306.1	306.2	306.3	306.7	307.2	306.2	308.2	308.2	308.2	306.2	306.2			
4.230	...	...	...	...	306.7	306.4	305.9	306.2	306.2	306.2	307.2	306.2	307.2	307.2	307.2	306.2	306.2			
4.320	...	...	...	...	306.7	306.4	305.9	306.2	306.2	306.2	307.2	306.2	307.2	307.2	307.2	306.2	306.2			
4.410	...	...	...	...	306.7	306.4	305.9	306.2	306.2	306.2	307.2	306.2	307.2	307.2	307.2	306.2	306.2			
4.500	...	...	...	...	306.7	306.4	305.9	306.2	306.2	306.2	307.2	306.2	307.2	307.2	307.2	306.2	306.2			
4.590	...	...	...	...	306.7	306.4	305.9	306.2	306.2	306.2	307.2	306.2	307.2	307.2	307.2	306.2	306.2			
4.680	...	...	...	...	306.7	306.4	305.9	306.2	306.2	306.2	307.2	306.2	307.2	307.2	30					

### B-Tables

Tables 2B to 20B, called B-tables, present the pressurant mole fraction histories as inferred from the  $I$ -location temperature histories from the A-tables. The basis of this data reduction program (see Appendix B) is the transient thermodynamic analysis by Corlett et al. [2]. Reference 5 gives this analysis in more detail.

In addition to pressurant concentrations at each  $I$ -location corresponding to those in the matching A-tables, values of the mean pressurant concentration  $\bar{X}$  are given. These values represent theoretical perfect mixing; they are determined from the known amount of resident gas initially in the chamber and the estimated amount of pressurant gas injected during any given time interval. Further, in the first six columns of the table, variables are given, respectively, as follows:

- (1) time  $t$  in seconds,
- (2) mean temperature of chamber contents  $\bar{T}$  in °C,
- (3) mean temperature of resident air  $\bar{T}_a$  in °C,
- (4) mean temperature of pressurant gas  $\bar{T}_p$  in °C,
- (5) dimensionless parameter-characterizing molar heat-transfer coefficient  $\beta$ , and
- (6) the ratio  $\beta/\theta$ , where  $\theta$  is a characteristic time in seconds.

Table 2B -- Inferred Pressurant Distribution, Scaling Run 230; Three 3.279-cm Nozzles

Pressurant Fractions (X) at Locations /																			
$t$ (s)	$\bar{T}$ (°C)	$\bar{T}_c$ (°C)	$\bar{T}_p$ (°C)	$\beta$	$\beta/\theta$	$\bar{X}$	1	2	3	4	5	6	7	8	9	10	11	12	13
COMMENCE VALVE OPENING																			
0.0	16.1	16.1	13.9	1.6	0.0000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
1.0	21.9	24.5	-7.4	9.5	.9170	.092	.102	.095	.071	.077	.083	.117	.102	.117	.086	.086	.102	.086	.071
VALVE FULLY OPEN																			
2.0	25.5	31.4	-4.3	6.1	.5091	.165	.187	.179	.142	.159	.173	.195	.134	.176	.176	.162	.176	.148	.134
3.0	27.7	36.3	-2.1	5.7	.4124	.223	.251	.248	.204	.230	.248	.290	.175	.214	.214	.188	.227	.214	.201
4.0	29.1	40.0	-	5.7	.3489	.289	.319	.289	.264	.282	.304	.311	.232	.237	.257	.232	.257	.245	.233
5.0	30.5	43.7	.3	3.6	.1882	.387	.337	.338	.306	.329	.359	.382	.234	.292	.292	.269	.280	.269	.280
6.0	31.1	46.3	1.2	4.7	.2232	.339	.391	.352	.325	.354	.382	.409	.293	.338	.327	.305	.338	.305	.294
7.0	31.0	47.9	1.3	6.4	.2801	.367	.410	.389	.354	.384	.413	.434	.310	.343	.343	.343	.376	.343	.332
8.0	31.2	49.3	2.0	3.9	.0967	.383	.421	.404	.378	.400	.429	.450	.332	.385	.364	.342	.374	.342	.333
COMMENCE VALVE CLOSURE																			
9.0	31.3	51.1	2.0	4.3	.1525	.404	.444	.426	.408	.418	.444	.471	.347	.398	.387	.357	.398	.377	.377
10.0	31.0	52.3	2.0	1.7	.1673	.423	.465	.444	.416	.438	.471	.495	.372	.422	.422	.382	.412	.382	.377
VALVE FULLY CLOSED																			
11.0	30.1	52.9	.8	1.4	.1464	.437	.478	.461	.428	.451	.480	.499	.399	.428	.428	.409	.418	.409	.399
12.0	31.6	56.2	.1	-2.6	-.2610	.437	.480	.467	.439	.458	.483	.505	.392	.419	.419	.401	.428	.401	.392
13.0	31.5	55.9	.1	2.2	.0249	.437	.488	.475	.450	.465	.488	.510	.391	.427	.409	.391	.418	.391	.382
14.0	31.2	55.2	.3	3.5	.0506	.437	.488	.472	.446	.461	.492	.508	.397	.425	.425	.388	.416	.388	.379
15.0	30.9	54.5	.4	3.5	.0517	.437	.487	.471	.447	.463	.495	.513	.393	.421	.421	.402	.412	.384	.375
16.0	30.7	54.2	.5	3.3	.0282	.437	.493	.479	.449	.467	.493	.519	.387	.415	.415	.397	.406	.378	.387
17.0	30.6	53.9	.6	3.3	.0285	.437	.501	.477	.450	.469	.495	.516	.381	.409	.409	.390	.418	.390	.381
18.0	30.3	53.2	.7	5.5	.0539	.437	.494	.473	.443	.460	.490	.523	.389	.418	.418	.389	.409	.389	.389
19.0	30.1	52.9	.8	3.3	.0274	.437	.500	.475	.448	.467	.490	.523	.400	.410	.410	.391	.400	.391	.381
20.0	29.9	52.5	.9	3.3	.0277	.437	.502	.477	.458	.479	.497	.516	.375	.404	.404	.384	.413	.384	.394
21.0	29.8	52.2	1.0	3.3	.0280	.437	.505	.483	.458	.479	.497	.512	.374	.403	.403	.383	.413	.383	.393
22.0	29.6	51.8	1.1	3.3	.0283	.437	.504	.480	.453	.474	.492	.510	.378	.417	.407	.378	.407	.378	.388
23.0	29.5	51.5	1.2	3.3	.0286	.437	.504	.482	.456	.472	.490	.514	.387	.417	.397	.377	.407	.377	.387
24.0	29.3	51.2	1.2	3.3	.0290	.437	.508	.484	.454	.466	.486	.504	.382	.412	.402	.392	.412	.402	.382
25.0	29.2	50.8	1.3	3.3	.0293	.437	.505	.483	.451	.465	.477	.503	.380	.431	.410	.390	.400	.390	.400
26.0	29.0	50.5	1.4	3.3	.0296	.437	.500	.482	.443	.458	.472	.507	.401	.431	.431	.390	.401	.390	.380
27.0	28.9	50.1	1.5	3.3	.0300	.437	.503	.485	.450	.464	.476	.503	.396	.427	.407	.386	.417	.386	.386
28.0	28.7	49.8	1.6	3.3	.0304	.437	.503	.482	.441	.461	.482	.507	.391	.422	.401	.401	.412	.401	.391
29.0	28.7	49.8	1.6	0.0	0.0000	.437	.499	.472	.441	.464	.486	.515	.391	.422	.422	.401	.412	.391	.370
30.0	28.6	49.5	1.7	3.3	.0308	.437	.499	.473	.444	.465	.492	.515	.388	.419	.419	.398	.409	.377	.388
31.0	28.4	49.1	1.8	3.3	.0311	.437	.497	.472	.445	.466	.497	.514	.386	.417	.417	.386	.407	.396	.386
32.0	28.2	48.8	1.8	0.0	.0315	.437	.497	.478	.450	.471	.501	.522	.386	.418	.397	.375	.407	.397	.386
33.0	28.0	48.8	1.8	0.0	0.0000	.437	.499	.476	.448	.472	.506	.531	.384	.416	.395	.374	.406	.395	.384
34.0	28.1	48.4	1.9	3.3	.0319	.437	.504	.482	.452	.473	.506	.523	.383	.415	.394	.372	.405	.394	.383



Table 3B — Inferred Pressurant Distribution, Scaling Run 231, Three 3.279-cm Nozzles

Pressurant Fractions (X) at Locations /																		
COMMENCE VALVE OPENING																		
0.0	13.5	13.5	30.7	1.7	0.0000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
1.0	18.3	18.5	13.4	-6	-0.0235	0.03	-0.454	-0.299	-0.025	-0.201	-0.338	-0.299	0.000	0.000	0.000	0.000	0.000	0.000
VALVE FULLY OPEN																		
2.0	23.5	23.7	9.9	5.1	0.0931	0.131	-0.000	-0.000	-0.000	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006
3.0	27.5	32.5	7.5	2.0	0.1580	0.135	0.131	0.127	0.127	0.147	0.135	0.179	0.279	0.279	0.279	0.279	0.279	0.279
4.0	29.6	37.5	6.3	3.7	0.2509	0.253	0.218	0.202	0.205	0.221	0.212	0.220	0.280	0.280	0.280	0.280	0.280	0.280
5.0	31.1	41.9	5.4	3.5	0.2116	0.266	0.268	0.276	0.276	0.271	0.271	0.306	0.312	0.304	0.312	0.304	0.312	0.304
6.0	31.9	45.0	4.1	3.0	0.2003	0.307	0.324	0.317	0.317	0.331	0.331	0.353	0.343	0.343	0.343	0.343	0.343	0.343
7.0	32.0	48.9	2.6	5.0	0.2431	0.346	0.389	0.344	0.350	0.357	0.357	0.389	0.376	0.376	0.376	0.376	0.376	0.376
8.0	32.4	51.5	2.7	3.2	0.1323	0.390	0.389	0.369	0.369	0.375	0.387	0.422	0.389	0.389	0.389	0.389	0.389	0.389
9.0	32.2	53.1	2.7	4.6	0.1782	0.414	0.412	0.402	0.402	0.404	0.410	0.436	0.388	0.420	0.420	0.420	0.420	0.420
COMMENCE VALVE CLOSURE																		
10.0	32.1	54.6	2.7	0.1	0.1397	0.433	0.429	0.423	0.423	0.425	0.423	0.439	0.425	0.445	0.445	0.445	0.445	0.445
11.0	31.7	55.0	2.4	3.1	0.1366	0.450	0.443	0.441	0.432	0.447	0.450	0.481	0.436	0.454	0.454	0.454	0.454	0.454
VALVE FULLY CLOSED																		
12.0	31.0	56.9	9	1.1	0.0470	0.461	0.460	0.460	0.449	0.455	0.462	0.480	0.453	0.462	0.462	0.462	0.462	0.462
13.0	31.9	58.0	6	-2.9	-0.1205	0.461	0.475	0.468	0.463	0.462	0.468	0.491	0.462	0.462	0.462	0.462	0.462	0.462
14.0	31.6	58.1	7	0.9	0.0421	0.464	0.474	0.464	0.464	0.458	0.472	0.490	0.453	0.453	0.453	0.453	0.453	0.453
15.0	31.3	57.5	8	1.0	0.0420	0.466	0.473	0.461	0.461	0.463	0.479	0.500	0.463	0.463	0.463	0.463	0.463	0.463
16.0	31.2	57.2	8	5	0.0217	0.466	0.466	0.461	0.461	0.466	0.472	0.500	0.470	0.461	0.461	0.461	0.461	0.461
17.0	30.9	56.6	9	1.0	0.0440	0.467	0.463	0.456	0.456	0.465	0.468	0.492	0.459	0.459	0.459	0.459	0.459	0.459
18.0	30.7	56.2	9	5	0.0223	0.461	0.473	0.464	0.464	0.455	0.466	0.487	0.471	0.464	0.464	0.464	0.464	0.464
19.0	30.6	55.9	1.0	5	0.0225	0.461	0.472	0.463	0.463	0.452	0.461	0.479	0.464	0.464	0.464	0.464	0.464	0.464
20.0	30.3	55.3	1.1	1.0	0.0456	0.474	0.469	0.460	0.460	0.454	0.459	0.474	0.459	0.459	0.459	0.459	0.459	0.459
21.0	30.1	54.9	1.1	5	0.0231	0.477	0.469	0.460	0.460	0.460	0.463	0.478	0.456	0.456	0.456	0.456	0.456	0.456
22.0	29.9	54.6	1.1	5	0.0233	0.478	0.468	0.460	0.460	0.467	0.467	0.483	0.453	0.453	0.453	0.453	0.453	0.453
23.0	29.8	54.3	1.2	5	0.0235	0.461	0.473	0.468	0.468	0.460	0.466	0.483	0.453	0.453	0.453	0.453	0.453	0.453
24.0	29.6	54.0	1.2	5	0.0237	0.461	0.471	0.463	0.463	0.465	0.465	0.484	0.453	0.453	0.453	0.453	0.453	0.453
25.0	29.6	54.0	1.2	0.0	0.0000	0.461	0.469	0.463	0.463	0.465	0.465	0.488	0.456	0.456	0.456	0.456	0.456	0.456
26.0	29.5	53.7	1.3	5	0.0240	0.461	0.462	0.460	0.460	0.464	0.464	0.490	0.452	0.452	0.452	0.452	0.452	0.452
27.0	29.3	53.3	1.3	5	0.0242	0.461	0.470	0.466	0.466	0.471	0.476	0.490	0.453	0.453	0.453	0.453	0.453	0.453
28.0	29.2	53.0	1.4	5	0.0244	0.461	0.470	0.468	0.468	0.474	0.480	0.493	0.453	0.453	0.453	0.453	0.453	0.453
29.0	29.0	52.7	1.4	6	0.0247	0.461	0.479	0.476	0.476	0.486	0.482	0.493	0.456	0.456	0.456	0.456	0.456	0.456
30.0	29.0	52.6	1.5	0.0	0.0000	0.461	0.481	0.477	0.461	0.469	0.475	0.493	0.453	0.453	0.453	0.453	0.453	0.453
31.0	28.9	51.3	2.7	6	0.0249	0.461	0.483	0.474	0.462	0.468	0.474	0.491	0.454	0.454	0.454	0.454	0.454	0.454
32.0	28.7	50.1	3.0	6	0.0252	0.461	0.479	0.475	0.464	0.464	0.469	0.493	0.453	0.453	0.453	0.453	0.453	0.453
33.0	28.7	49.5	4.5	0.0	0.0000	0.461	0.478	0.472	0.461	0.465	0.472	0.492	0.450	0.450	0.450	0.450	0.450	0.450
34.0	28.6	48.5	5.3	6	0.0254	0.461	0.480	0.473	0.462	0.467	0.473	0.494	0.448	0.448	0.448	0.448	0.448	0.448

Table 4B — Inferred Pressurant Distribution, Scaling Run 232; Three 3.279-cm Nozzles

T (a)	T <sub>0</sub> (°C)	T <sub>0</sub> (°C)	T <sub>0</sub> (°C)	β	β/θ	X̄	Pressurant Fractions (X) at Locations /												
							1	2	3	4	5	6	7	8	9	10	11	12	13
COMMENCE VALVE OPENING																			
0.0	8.7	8.7	21.1	1.5	0.0000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
1.0	14.1	15.1	-1.2	10.1	.6784	.065	-.049	.007	.099	.062	-.036	-.030	.148	.086	.056	.117	.086	.179	
VALVE FULLY OPEN																			
2.0	19.7	24.1	-5.3	1.8	.1649	.148	.093	.104	.121	.114	.097	.124	.182	.182	.182	.216	.182	.182	
3.0	22.8	29.7	-6.0	-8	-.0398	.192	.148	.139	.142	.167	.153	.181	.223	.195	.195	.231	.223	.251	
4.0	24.4	34.3	-5.3	4.6	.3423	.249	.217	.212	.212	.222	.222	.243	.280	.268	.268	.293	.268	.280	
5.0	26.1	39.1	-4.7	2.7	.1787	.289	.282	.280	.259	.275	.273	.289	.305	.305	.305	.328	.305	.328	
6.0	26.0	42.1	-4.1	4.0	.2190	.323	.329	.316	.308	.319	.325	.338	.323	.344	.344	.344	.355	.355	
7.0	27.3	45.1	-3.7	3.2	.1548	.364	.375	.363	.349	.359	.359	.377	.357	.377	.357	.377	.377	.357	
8.0	27.1	46.8	-3.4	5.0	.2284	.392	.386	.386	.364	.376	.374	.406	.380	.396	.410	.410	.410	.420	
9.0	27.6	49.3	-3.3	2.3	.0865	.414	.409	.403	.394	.400	.401	.420	.392	.411	.411	.430	.430	.468	
COMMENCE VALVE CLOSURE																			
10.0	27.4	50.9	-3.2	3.9	.1344	.434	.435	.426	.404	.411	.424	.465	.437	.456	.437	.437	.437	.447	
11.0	26.8	51.9	-3.6	2.1	.1464	.452	.446	.441	.421	.441	.455	.473	.453	.472	.472	.453	.453	.453	
VALVE FULLY CLOSED																			
12.0	26.1	52.2	-4.7	-8	-.0547	.459	.462	.444	.427	.441	.457	.478	.448	.465	.483	.483	.465	.465	
13.0	26.8	53.8	-5.0	-1.5	-.1068	.459	.461	.461	.442	.459	.467	.481	.455	.455	.455	.464	.455	.455	
14.0	26.7	53.5	-4.9	3	.0210	.459	.467	.463	.433	.467	.479	.486	.448	.465	.465	.468	.448	.448	
15.0	26.4	52.9	-4.8	6	.0425	.459	.465	.462	.435	.457	.469	.478	.445	.453	.453	.471	.462	.453	
16.0	26.2	52.5	-4.8	3	.0215	.459	.468	.456	.431	.458	.472	.486	.449	.449	.449	.466	.449	.466	
17.0	25.9	51.9	-4.7	6	.0436	.459	.480	.473	.454	.468	.480	.487	.445	.445	.445	.445	.445	.445	
18.0	25.8	51.6	-4.6	3	.0221	.459	.473	.473	.462	.464	.471	.485	.441	.441	.441	.441	.441	.439	
19.0	25.5	51.0	-4.6	6	.0448	.459	.467	.471	.460	.464	.473	.485	.449	.449	.449	.449	.449	.440	
20.0	25.3	50.6	-4.5	3	.0227	.459	.463	.459	.435	.461	.468	.485	.454	.454	.454	.454	.454	.434	
21.0	25.2	50.3	-4.5	3	.0229	.459	.470	.463	.436	.461	.476	.490	.467	.468	.468	.468	.468	.448	
22.0	25.0	50.0	-4.4	3	.0231	.459	.476	.469	.436	.462	.476	.493	.445	.445	.445	.445	.445	.445	
23.0	24.9	49.7	-4.4	3	.0234	.459	.468	.462	.435	.462	.472	.488	.457	.457	.457	.457	.457	.438	
24.0	24.7	49.4	-4.3	3	.0236	.459	.470	.464	.461	.468	.479	.494	.461	.461	.461	.461	.461	.442	
25.0	24.6	49.0	-4.3	3	.0238	.459	.470	.464	.460	.464	.479	.498	.463	.463	.463	.463	.463	.445	
26.0	24.4	48.7	-4.2	3	.0240	.459	.468	.460	.449	.464	.479	.498	.463	.463	.463	.463	.463	.443	
27.0	24.3	48.4	-4.2	4	.0243	.459	.465	.461	.446	.457	.474	.498	.463	.463	.463	.463	.463	.440	
28.0	24.3	48.4	-4.2	0	0.0000	.459	.466	.459	.449	.457	.470	.485	.457	.457	.457	.457	.457	.438	
29.0	24.1	48.1	-4.1	4	.0245	.459	.470	.459	.449	.457	.468	.486	.457	.457	.457	.457	.457	.438	
30.0	24.0	47.7	-4.1	4	.0247	.459	.470	.459	.431	.462	.470	.491	.455	.455	.455	.455	.455	.435	
31.0	23.8	47.4	-4.0	4	.0250	.459	.471	.457	.437	.469	.477	.492	.452	.452	.452	.452	.452	.432	
32.0	23.8	47.4	-4.0	0	0.0000	.459	.476	.468	.456	.470	.476	.489	.450	.450	.450	.450	.450	.431	
33.0	23.7	47.1	-4.0	4	.0252	.459	.474	.476	.461	.469	.476	.490	.457	.457	.457	.457	.457	.427	
34.0	23.5	46.8	-3.9	4	.0255	.459	.475	.473	.459	.473	.479	.488	.443	.443	.443	.443	.443	.423	

Table SB — Inferred Pressurant Distribution, Scaling Run 233, Three 3.279-cm Nozzles

t (s)	T (°C)	T <sub>c</sub> (°C)	T <sub>p</sub> (°C)	β	β/θ	X	Pressurant Fractions (X) at Locations /												
							1	2	3	4	5	6	7	8	9	10	11	12	13
COMMENCE VALVE OPENING																			
0.0	12.6	12.6	40.5	1.9	0.0000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
1.0	16.3	16.5	12.9	36.1	1.6199	.044	-.554	-307	130	.040	-.253	-.171	513	240	-.034	240	240	240	
VALVE FULLY OPEN																			
2.0	22.1	24.3	7.6	3.2	.2931	.120	.020	.038	.074	.086	.068	.150	.248	.150	.150	.218	.128	.158	
3.0	25.3	30.0	6.4	4.0	.4002	.198	.122	.117	.134	.151	.139	.228	.270	.228	.228	.270	.228	.228	
4.0	28.0	35.7	4.7	2.6	.1764	.250	.215	.212	.206	.212	.209	.237	.272	.272	.261	.293	.277	.277	
5.0	29.6	40.5	3.2	3.1	.1841	.293	.270	.265	.270	.268	.278	.313	.292	.292	.319	.319	.319	.292	
6.0	30.7	44.9	1.7	2.9	.1485	.329	.332	.323	.307	.323	.328	.335	.318	.330	.330	.341	.330	.330	
7.0	31.0	47.7	1.2	4.2	.1993	.360	.333	.350	.340	.361	.363	.381	.346	.346	.346	.368	.368	.368	
8.0	31.4	50.3	1.4	3.1	.1273	.385	.392	.384	.375	.381	.390	.408	.381	.381	.381	.392	.381	.371	
9.0	31.1	51.5	1.6	5.3	.2037	.409	.404	.406	.388	.404	.412	.432	.398	.418	.418	.418	.398	.398	
COMMENCE VALVE CLOSURE																			
10.0	31.0	53.1	1.5	4.0	.1398	.420	.420	.422	.409	.422	.434	.449	.426	.436	.436	.436	.426	.416	
11.0	30.7	54.3	1.4	2.9	.1331	.446	.456	.454	.431	.442	.442	.473	.448	.448	.448	.448	.429	.429	
VALVE FULLY CLOSED																			
12.0	29.7	54.9	-0	2.4	.1082	.458	.470	.466	.449	.453	.458	.486	.451	.460	.460	.460	.451	.433	
13.0	30.8	57.1	-2	-3.3	.1324	.458	.470	.461	.447	.457	.468	.494	.454	.454	.454	.454	.434	.437	
14.0	30.7	56.8	-2	5	.0212	.458	.466	.457	.444	.459	.474	.501	.450	.450	.450	.450	.430	.430	
15.0	30.4	56.1	-1	5	.0430	.458	.467	.456	.447	.455	.469	.497	.462	.460	.460	.460	.460	.442	
16.0	30.0	55.5	-0	1.0	.0437	.458	.467	.460	.448	.458	.480	.507	.458	.458	.449	.449	.431	.440	
17.0	29.9	55.2	-0	5	.0222	.458	.474	.465	.462	.464	.480	.503	.462	.462	.444	.444	.425	.435	
18.0	29.6	54.5	1	1.0	.0449	.458	.476	.470	.461	.472	.489	.509	.456	.456	.437	.437	.417	.425	
19.0	29.4	54.2	1	5	.0228	.458	.484	.478	.463	.467	.476	.502	.454	.454	.436	.436	.416	.416	
20.0	29.3	53.9	2	5	.0230	.458	.482	.484	.486	.482	.473	.512	.451	.451	.431	.431	.412	.426	
21.0	29.1	53.6	2	5	.0232	.458	.470	.459	.450	.461	.478	.509	.450	.450	.430	.430	.410	.430	
22.0	29.0	53.3	3	5	.0234	.458	.473	.463	.446	.456	.473	.503	.446	.446	.426	.426	.406	.465	
23.0	28.8	52.9	3	5	.0236	.458	.479	.469	.446	.458	.467	.496	.444	.444	.424	.424	.404	.463	
24.0	28.7	52.6	3	5	.0238	.458	.483	.467	.454	.464	.477	.502	.444	.444	.424	.424	.404	.464	
25.0	28.5	52.3	4	5	.0241	.458	.480	.464	.453	.462	.472	.505	.449	.449	.429	.429	.409	.439	
26.0	28.4	52.0	4	5	.0243	.458	.482	.464	.450	.460	.470	.499	.462	.462	.442	.442	.422	.443	
27.0	28.4	52.0	4	0.0	.0000	.458	.472	.464	.456	.462	.468	.497	.458	.458	.438	.438	.418	.449	
28.0	28.2	51.7	5	5	.0245	.458	.470	.459	.449	.457	.468	.498	.451	.451	.431	.431	.411	.451	
29.0	28.0	51.3	5	5	.0248	.458	.473	.463	.452	.457	.467	.497	.450	.450	.430	.430	.410	.450	
30.0	27.9	51.0	6	5	.0250	.458	.477	.465	.453	.455	.465	.495	.447	.447	.427	.427	.407	.447	
31.0	27.9	49.5	2.4	0.0	.0000	.458	.480	.463	.448	.452	.462	.493	.454	.454	.434	.434	.414	.465	
32.0	27.7	48.3	3.5	6	.0253	.458	.484	.464	.450	.453	.470	.502	.441	.441	.421	.421	.401	.464	
33.0	27.6	47.1	4.5	6	.0256	.458	.487	.471	.452	.462	.473	.511	.443	.443	.423	.423	.403	.463	
34.0	27.6	46.6	5.1	0.0	.0000	.458	.484	.465	.453	.460	.474	.513	.441	.441	.421	.421	.401	.463	

Table 6B — Inferred Pressurant Distribution, Scaling Run 234; Three 3.279-cm Nozzles

i (a)	T (°C)	T <sub>c</sub> (°C)	T <sub>c</sub> (°C)	β	β/θ	X̄	Pressurant Fractions (X) at Locations /												
							1	2	3	4	5	6	7	8	9	10	11	12	13
COMMENCE VALVE OPENING																			
0.0	9.0	9.0	21.4	1.5	0.0000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
1.0	14.3	15.4	-2.2	8.9	.5088	.064	.016	.010	.044	.056	.022	-.041	.136	.050	.079	.136	.079	.136	
VALVE FULLY OPEN																			
2.0	19.6	23.9	-5.3	3.0	.2821	.148	.097	.111	.110	.110	.111	.113	.203	.203	.169	.203	.169	.169	
3.0	22.6	29.3	-5.6	2.0	.0114	.192	.147	.141	.164	.170	.170	.239	.239	.239	.239	.210	.210	.182	
4.0	24.7	34.4	-4.8	3.8	.2600	.248	.222	.220	.205	.220	.230	.240	.253	.266	.278	.266	.278	.266	
5.0	26.1	38.6	-4.1	3.5	.2227	.294	.286	.277	.261	.275	.284	.296	.296	.319	.296	.319	.296	.319	
6.0	27.0	42.2	-3.6	3.3	.1804	.331	.326	.324	.311	.313	.322	.330	.332	.354	.332	.354	.332	.354	
7.0	27.7	45.2	-3.2	3.1	.1434	.382	.380	.364	.339	.350	.362	.379	.356	.356	.376	.356	.376	.356	
8.0	27.9	47.6	-3.0	3.5	.1466	.389	.409	.403	.375	.391	.403	.403	.387	.387	.387	.387	.387	.379	
9.0	28.3	50.1	-3.0	2.5	.0940	.411	.430	.432	.417	.424	.426	.434	.398	.398	.398	.398	.417	.379	
COMMENCE VALVE CLOSURE																			
10.0	27.8	51.1	-2.9	5.1	.1794	.432	.454	.448	.428	.434	.434	.447	.419	.428	.428	.428	.437	.400	
11.0	27.5	52.6	-3.3	1.6	.1079	.449	.462	.462	.446	.453	.463	.474	.440	.440	.440	.440	.458	.422	
VALVE FULLY CLOSED																			
12.0	27.2	54.3	-4.8	-3	-.0212	.438	.480	.468	.437	.467	.480	.489	.443	.443	.443	.443	.462	.428	
13.0	28.4	56.8	-5.1	-2.4	-.1623	.438	.480	.466	.430	.466	.484	.492	.438	.446	.446	.446	.459	.438	
14.0	28.4	56.8	-5.1	0.0	0.0000	.438	.485	.474	.461	.474	.479	.482	.438	.438	.438	.438	.454	.438	
15.0	28.1	56.2	-5.1	6	.0396	.438	.482	.478	.469	.492	.491	.476	.445	.437	.437	.437	.454	.429	
16.0	28.0	55.8	-5.0	3	.0200	.438	.479	.467	.462	.469	.477	.476	.451	.434	.431	.431	.451	.434	
17.0	27.7	55.2	-4.9	6	.0406	.438	.484	.474	.461	.474	.474	.484	.444	.444	.444	.444	.454	.444	
18.0	27.5	54.9	-4.9	3	.0206	.438	.487	.480	.467	.479	.482	.482	.442	.442	.442	.442	.452	.435	
19.0	27.2	54.3	-4.8	6	.0416	.438	.481	.475	.468	.481	.490	.486	.430	.439	.439	.439	.447	.439	
20.0	27.1	53.9	-4.8	3	.0211	.438	.470	.463	.463	.469	.479	.482	.435	.435	.435	.435	.452	.432	
21.0	27.1	53.9	-4.8	0.0	0.0000	.438	.472	.464	.452	.466	.478	.483	.432	.439	.439	.439	.449	.432	
22.0	26.9	53.6	-4.7	3	.0212	.438	.474	.464	.460	.467	.479	.486	.446	.446	.446	.446	.456	.438	
23.0	26.7	53.3	-4.7	3	.0214	.438	.483	.476	.465	.473	.473	.482	.445	.445	.445	.445	.456	.438	
24.0	26.6	53.0	-4.6	3	.0216	.438	.487	.479	.465	.466	.473	.478	.445	.445	.445	.445	.456	.438	
25.0	26.4	52.7	-4.6	3	.0218	.438	.488	.476	.463	.464	.472	.483	.445	.445	.445	.445	.456	.438	
26.0	26.3	52.3	-4.5	3	.0220	.438	.490	.475	.463	.464	.471	.476	.443	.443	.443	.443	.456	.438	
27.0	26.1	52.0	-4.5	3	.0222	.438	.486	.473	.461	.464	.473	.477	.443	.443	.443	.443	.456	.438	
28.0	26.0	51.7	-4.4	3	.0224	.438	.483	.472	.461	.463	.474	.479	.443	.443	.443	.443	.456	.438	
29.0	26.0	51.7	-4.4	0.0	0.0000	.438	.480	.471	.467	.464	.476	.480	.444	.444	.444	.444	.456	.438	
30.0	25.8	51.4	-4.4	3	.0226	.438	.480	.475	.460	.466	.477	.480	.443	.443	.443	.443	.456	.438	
31.0	25.7	51.1	-4.3	3	.0228	.438	.485	.474	.462	.467	.478	.480	.440	.440	.440	.440	.456	.438	
32.0	25.7	51.1	-4.3	0.0	0.0000	.438	.482	.475	.460	.466	.478	.482	.439	.439	.439	.439	.457	.437	
33.0	25.5	50.7	-4.3	3	.0230	.438	.485	.474	.460	.469	.482	.482	.438	.438	.438	.438	.456	.436	
34.0	25.5	50.7	-4.3	0.0	0.0000	.438	.483	.477	.461	.470	.484	.483	.437	.437	.437	.437	.455	.435	

Table 7B — Inferred Pressurant Distribution, Sealing Run 235; Three 3.279-cm Nozzles

Pressurant Fractions (X) at Locations /															
	1	2	3	4	5	6	7	8	9	10	11	12	13		
CONDUCE VALVE OPENING	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000			
0.0 10.4 10.4 30.4															
1.0 15.6 15.0 10.5	0.049	- .359	- .152	.036	-.077	-.189	-.265	.450	.074	.262	-.020	.356	.262		
VALVE FULLY OPEN															
2.0 21.0 20.0 5.3	.135	.049	.063	.065	.071	.049	.076	.109	.243	.243	.199	.082	.199		
3.0 24.5 29.5 4.6	.203	.136	.128	.132	.144	.144	.180	.204	.264	.264	.244	.204	.224		
4.0 26.5 34.3 4.1	.267	.204	.211	.204	.204	.201	.234	.326	.293	.293	.293	.260	.293		
5.0 20.6 40.1 1.6	.299	.207	.207	.279	.207	.209	.302	.315	.302	.302	.302	.289	.320		
6.0 29.3 43.1 1.0	.335	.319	.312	.321	.339	.346	.370	.331	.331	.353	.331	.331	.331		
7.0 29.3 44.5 1.9	.356	.336	.351	.341	.349	.349	.370	.353	.353	.377	.353	.377	.353		
8.0 29.7 47.0 1.9	.383	.367	.381	.367	.369	.381	.401	.389	.401	.412	.389	.367	.389		
9.0 29.6 48.0 1.0	.407	.401	.403	.396	.392	.405	.415	.432	.432	.432	.411	.390	.390		
CONDUCE VALVE CLOSURE															
10.0 29.5 50.3 1.6	.427	.409	.411	.411	.405	.424	.442	.430	.430	.440	.420	.420	.420		
11.0 29.3 51.7 1.3	.445	.444	.444	.419	.428	.442	.460	.423	.462	.462	.442	.462	.442		
VALVE FULLY CLOSED															
12.0 20.3 52.5 -3	.450	.453	.457	.440	.450	.461	.476	.463	.463	.463	.446	.463	.463		
13.0 29.8 53.5 -6	.480	.463	.465	.446	.447	.450	.467	.463	.463	.463	.446	.463	.463		
14.0 29.7 55.2 -3	.480	.463	.469	.455	.456	.467	.481	.462	.462	.462	.444	.444	.453		
15.0 29.4 54.6 -5	.480	.458	.458	.469	.461	.470	.487	.452	.452	.470	.434	.452	.452		
16.0 29.2 50.3 -5	.450	.473	.466	.464	.466	.482	.489	.458	.458	.458	.440	.432	.440		
17.0 20.9 53.7 -4	.480	.483	.481	.473	.475	.481	.484	.451	.451	.451	.433	.433	.442		
18.0 20.0 53.4 -4	.480	.483	.478	.472	.463	.472	.478	.450	.450	.450	.431	.450	.450		
19.0 20.6 53.1 -4	.480	.486	.479	.467	.463	.463	.479	.450	.450	.450	.432	.432	.450		
20.0 20.3 52.5 -3	.480	.480	.482	.471	.463	.463	.476	.440	.440	.440	.429	.429	.440		
21.0 20.1 52.2 -3	.480	.480	.481	.460	.460	.462	.477	.444	.444	.444	.429	.444	.464		
22.0 20.0 51.9 -3	.480	.480	.487	.437	.439	.466	.480	.461	.461	.461	.441	.422	.441		
23.0 27.0 51.6 -2	.480	.480	.476	.436	.464	.470	.481	.458	.458	.458	.439	.439	.458		
24.0 27.0 51.6 -2	.480	.464	.460	.433	.450	.460	.478	.456	.456	.456	.437	.437	.456		
25.0 27.7 51.3 -2	.480	.459	.461	.449	.455	.463	.474	.451	.451	.470	.451	.432	.451		
26.0 27.5 51.0 -2	.480	.457	.453	.448	.457	.463	.475	.448	.448	.467	.448	.457	.467		
27.0 27.4 50.7 -2	.480	.456	.450	.450	.450	.466	.477	.462	.462	.462	.442	.462	.462		
28.0 27.2 50.4 -1	.480	.455	.457	.447	.455	.463	.473	.459	.459	.479	.459	.459	.459		
29.0 27.1 50.0 -1	.480	.455	.453	.443	.451	.461	.483	.475	.475	.475	.455	.455	.455		
30.0 27.1 50.0 -1	.480	.450	.458	.450	.450	.474	.490	.464	.464	.464	.434	.454	.454		
31.0 26.9 49.7 -1	.480	.454	.458	.450	.466	.480	.494	.456	.456	.456	.436	.456	.456		
32.0 26.8 49.4 -0	.480	.452	.452	.454	.462	.479	.489	.450	.450	.471	.450	.450	.450		
33.0 26.8 49.4 -0	.480	.453	.457	.459	.469	.477	.489	.471	.461	.451	.451	.451	.451		
34.0 26.6 49.0 -1	.480	.457	.461	.463	.469	.479	.496	.451	.451	.451	.430	.451	.451		

Table 8B — Inferred Pressurant Distribution, Scaling Run 236; Three 3.279-cm Nozzles

l (in)	T (°C)	T <sub>0</sub> (°C)	T <sub>1</sub> (°C)	β	β/θ	X̄	Pressurant Fractions (X) at Locations l												
							1	2	3	4	5	6	7	8	9	10	11	12	13
CORRECTION VALVE OPENING																			
0.0	17.4	17.4	23.7	1.6	0.0000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
1.0	23.1	24.2	6.9	5.1	.3268	.062	-.051	-.016	.030	.013	-.033	-.033	.157	.100	.129	.157	.100	.129	
VALVE FULLY OPEN																			
2.0	28.0	32.0	5.9	7.2	.7105	.151	.132	.128	.124	.139	.153	.170	.174	.174	.136	.174	.136	.174	
3.0	31.4	38.0	7.2	4.8	.3806	.215	.200	.213	.178	.210	.210	.226	.246	.262	.230	.230	.197	.197	
4.0	34.2	43.6	8.3	2.9	.1948	.267	.263	.277	.235	.260	.280	.305	.260	.260	.260	.280	.260	.260	
5.0	35.4	46.5	8.9	3.6	.1461	.296	.307	.302	.270	.294	.310	.334	.267	.320	.294	.294	.287	.294	
6.0	35.0	49.0	9.4	5.5	.3069	.334	.331	.333	.323	.336	.346	.360	.343	.331	.343	.331	.331	.331	
7.0	36.5	52.0	9.6	3.7	.1750	.364	.370	.376	.347	.371	.393	.402	.366	.366	.366	.366	.343	.343	
8.0	36.4	53.7	9.6	5.3	.2251	.392	.427	.396	.366	.382	.389	.414	.368	.391	.403	.403	.403	.380	
9.0	36.4	55.4	9.6	4.7	.1813	.415	.431	.429	.400	.420	.433	.470	.392	.413	.392	.413	.413	.392	
CORRECTION VALVE CLOSED																			
10.0	36.6	57.4	9.4	3.2	.1079	.434	.464	.456	.418	.441	.462	.477	.427	.427	.427	.416	.416	.406	
11.0	36.0	58.0	9.2	2.0	.1087	.451	.483	.468	.438	.460	.470	.479	.442	.442	.442	.442	.442	.421	
VALVE FULLY CLOSED																			
12.0	34.9	58.2	7.7	1.4	.0953	.461	.487	.477	.451	.471	.483	.504	.451	.451	.451	.451	.451	.431	
13.0	35.7	59.7	7.6	-1.7	.1056	.461	.499	.481	.451	.468	.479	.495	.447	.437	.447	.456	.447	.437	
14.0	35.6	59.4	7.7	.3	.0215	.461	.510	.494	.452	.465	.485	.504	.442	.442	.442	.442	.442	.423	
15.0	35.3	58.8	7.7	.7	.0436	.461	.513	.505	.458	.468	.483	.507	.436	.436	.436	.436	.436	.436	
16.0	34.9	58.2	7.7	.7	.0444	.461	.506	.496	.458	.474	.488	.504	.452	.452	.452	.452	.452	.432	
17.0	34.8	57.9	7.8	.3	.0225	.461	.500	.494	.460	.480	.498	.510	.446	.446	.446	.446	.446	.426	
18.0	34.5	57.3	7.8	.7	.0456	.461	.498	.496	.468	.484	.498	.508	.440	.440	.440	.440	.440	.419	
19.0	34.3	57.0	7.8	.3	.0231	.461	.502	.498	.473	.485	.498	.512	.435	.435	.435	.435	.435	.424	
20.0	34.0	56.3	7.9	.7	.0469	.461	.507	.499	.470	.485	.497	.507	.429	.429	.429	.429	.429	.429	
21.0	33.8	56.0	7.9	.4	.0230	.461	.504	.496	.479	.491	.498	.506	.446	.446	.446	.446	.446	.425	
22.0	33.7	55.7	7.9	.4	.0240	.461	.505	.494	.465	.480	.500	.513	.448	.448	.448	.448	.448	.427	
23.0	33.5	55.4	7.9	.4	.0243	.461	.494	.488	.465	.477	.494	.513	.446	.446	.446	.446	.446	.425	
24.0	33.4	55.1	8.0	.4	.0245	.461	.486	.482	.456	.473	.488	.512	.442	.442	.442	.442	.442	.442	
25.0	33.2	54.8	8.0	.4	.0247	.461	.488	.475	.456	.475	.490	.509	.436	.436	.436	.436	.436	.436	
26.0	33.1	54.5	8.0	.4	.0250	.461	.491	.476	.458	.476	.489	.512	.452	.452	.452	.452	.452	.430	
27.0	33.1	54.5	8.0	0.0	.0000	.461	.491	.493	.467	.482	.493	.506	.450	.450	.450	.450	.450	.429	
28.0	32.9	54.1	8.0	.4	.0232	.461	.492	.488	.468	.490	.496	.509	.451	.451	.451	.451	.451	.429	
29.0	32.7	53.8	8.1	.4	.0235	.461	.492	.492	.470	.490	.503	.516	.440	.440	.440	.440	.440	.429	
30.0	32.7	53.8	8.1	0.0	.0000	.461	.497	.488	.462	.488	.501	.521	.449	.449	.449	.449	.449	.427	
31.0	32.6	53.5	8.1	.4	.0238	.461	.500	.499	.469	.491	.504	.522	.449	.449	.449	.449	.449	.427	
32.0	32.4	53.2	8.1	.4	.0260	.461	.499	.492	.470	.492	.501	.519	.450	.450	.450	.450	.450	.428	
33.0	32.3	52.9	8.2	.4	.0262	.461	.501	.490	.477	.495	.501	.515	.430	.430	.430	.430	.430	.430	
34.0	32.3	52.9	8.2	0.0	.0000	.461	.502	.493	.473	.493	.502	.509	.431	.431	.431	.431	.431	.431	

Table 9B — Inferred Pressurant Distribution, Scaling Run 237; Three 3.279-cm Nozzles

t (s)	T (°C)	T <sub>0</sub> (°C)	T <sub>c</sub> (°C)	β	β/θ	X̄	Pressurant Fractions (X) at Locations /												
							1 = 1	2	3	4	5	6	7	8	9	10	11	12	13
COMMENCE VALVE OPENING																			
0.0	7.4	7.4	35.8	1.9	0.0000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
1.0	10.9	11.6	-1.0	36.4	1.9066	0.001	-0.232	-0.446	742	065	-143	-150	051	-061	-135	-061	068	311	
VALVE FULLY OPEN																			
2.0	15.5	18.6	-3.9	11.3	1.0980	0.139	-0.078	047	637	070	002	033	096	051	006	051	096	341	
3.0	18.3	23.0	-2.4	7.9	0.6800	0.207	0.023	176	684	126	084	077	126	107	088	107	241	603	
4.0	20.7	28.4	-1.4	5.3	0.3692	0.260	0.116	254	733	177	163	197	167	167	133	133	200	670	
5.0	21.0	31.7	-8	6.0	0.3612	0.303	0.143	251	769	245	245	269	208	208	161	177	254	716	
6.0	22.6	34.4	-4	5.6	0.3035	0.300	0.208	294	797	248	260	297	257	257	199	199	314	717	
7.0	22.7	36.2	-2	6.2	0.2939	0.370	0.232	310	836	296	274	280	296	269	241	241	337	62	
8.0	23.1	38.4	-2	4.5	0.1843	0.395	0.286	367	812	330	317	369	335	284	258	258	361	276	
9.0	22.8	38.0	-2	7.8	0.2061	0.411	0.209	360	852	342	342	378	291	342	266	291	394	603	
COMMENCE VALVE CLOSURE																			
10.0	22.3	39.5	-3	7.3	0.2636	0.432	0.318	411	850	340	366	398	353	353	315	315	391	605	
11.0	22.3	41.0	-3	2.5	0.1394	0.449	0.349	403	841	365	386	422	398	374	326	350	446	784	
VALVE FULLY CLOSED																			
12.0	21.5	42.0	-2.3	2.1	0.1105	0.463	0.380	491	899	385	412	414	396	385	339	339	441	791	
13.0	23.3	45.7	-2.7	-5.7	0.3069	0.463	0.434	483	568	391	413	428	434	413	393	393	455	640	
14.0	23.3	45.7	-2.7	0.0	0.0000	0.463	0.471	467	512	430	437	477	432	432	422	422	453	543	
15.0	23.0	48.1	-2.6	9	0.0487	0.483	0.489	466	512	445	479	500	447	447	426	426	457	668	
16.0	22.8	44.0	-2.6	15	0.0217	0.483	0.493	474	514	459	490	505	444	444	423	423	444	459	
17.0	22.5	44.2	-2.5	9	0.0501	0.483	0.492	468	509	462	498	511	440	440	419	419	440	462	
18.0	22.4	43.9	-2.5	5	0.0254	0.483	0.499	465	506	461	493	506	439	461	417	417	439	461	
19.0	22.2	43.6	-2.5	5	0.0287	0.483	0.501	468	505	459	488	501	451	451	429	429	451	451	
20.0	22.1	43.2	-2.4	5	0.0260	0.483	0.511	469	504	460	491	500	447	447	425	425	447	447	
21.0	21.9	42.9	-2.4	5	0.0262	0.483	0.505	470	499	457	485	499	446	446	424	424	446	446	
22.0	21.8	42.6	-2.4	5	0.0285	0.483	0.496	461	496	454	483	494	461	461	439	439	461	439	
23.0	21.6	42.3	-2.3	5	0.0288	0.483	0.492	459	497	459	483	497	454	454	432	432	454	454	
24.0	21.5	42.0	-2.3	5	0.0271	0.483	0.493	454	504	464	491	493	448	448	425	425	448	448	
25.0	21.3	41.7	-2.3	5	0.0274	0.483	0.492	461	513	470	488	495	447	447	424	424	447	447	
26.0	21.2	41.4	-2.2	5	0.0277	0.483	0.495	462	504	462	485	497	449	449	426	426	449	449	
27.0	21.2	41.4	-2.2	0.0	0.0000	0.483	0.490	460	501	460	488	499	446	446	423	423	446	446	
28.0	21.0	40.7	-2.2	5	0.0280	0.483	0.496	461	505	463	491	502	447	447	424	424	447	447	
29.0	20.9	40.7	-2.2	5	0.0283	0.483	0.496	471	505	471	489	501	445	445	422	422	445	445	
30.0	20.7	40.4	-2.1	5	0.0287	0.483	0.496	467	519	479	496	498	442	442	418	418	442	442	
31.0	20.7	40.4	-2.1	0.0	0.0000	0.483	0.490	462	513	473	499	499	437	437	437	437	437	437	
32.0	20.5	40.1	-2.1	5	0.0290	0.483	0.490	462	509	467	495	502	436	436	436	436	436	436	
33.0	20.4	39.0	-2.0	5	0.0293	0.483	0.492	457	502	461	492	502	435	435	435	435	435	435	
34.0	20.4	39.0	-2.0	0.0	0.0000	0.483	0.498	462	505	465	489	498	434	434	434	434	434	434	

Table 10B — Inferred Pressurant Distribution, Scaling Run 238; Three 3.279-cm Nozzles

i (°)	$\bar{T}$ (°C)	$\bar{T}_e$ (°C)	$\bar{T}_p$ (°C)	$\beta$	$\beta/\theta$	$\bar{X}$	Pressurant Fractions (X) at Locations i												
							1	2	3	4	5	6	7	8	9	10	11	12	13
COMMENCE VALVE OPENING																			
0.0	7.4	7.4	35.8	1.9	0.0000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
1.0	10.9	11.6	-1.6	36.4	1.9066	.031	-.232	-.046	.742	.065	-.143	-.150	.051	-.061	-.135	-.061	.088	.311	
VALVE FULLY OPEN																			
2.0	15.5	18.6	-3.9	11.3	1.0988	.139	-.078	.047	.637	.078	.002	.033	.096	.051	.006	.051	.096	.541	
3.0	18.3	23.8	-2.4	7.9	.6480	.207	.023	.176	.684	.126	.084	.077	.126	.107	.088	.107	.241	.603	
4.0	20.7	28.4	-1.4	5.3	.3692	.260	.116	.254	.733	.177	.163	.197	.167	.167	.133	.133	.200	.670	
5.0	21.8	31.7	-.8	5.0	.3612	.303	.143	.251	.769	.245	.245	.269	.208	.208	.161	.172	.254	.716	
6.0	22.6	34.4	-.4	5.6	.3035	.340	.208	.294	.797	.248	.260	.297	.257	.257	.199	.199	.314	.717	
7.0	22.7	36.2	-.2	6.2	.2939	.370	.232	.310	.836	.296	.274	.280	.296	.296	.241	.241	.337	.762	
8.0	23.1	38.4	-.2	4.5	.1843	.395	.286	.367	.812	.330	.317	.369	.335	.384	.258	.258	.361	.776	
9.0	22.8	38.8	-.2	7.8	.2061	.411	.289	.360	.852	.342	.342	.378	.291	.342	.266	.291	.394	.603	
COMMENCE VALVE CLOSURE																			
10.0	22.3	39.5	-.3	7.3	.2636	.432	.310	.411	.850	.348	.368	.398	.353	.353	.315	.315	.351	.605	
11.0	22.3	41.0	-.5	2.5	.1394	.449	.369	.403	.841	.363	.386	.422	.398	.374	.326	.350	.446	.784	
VALVE FULLY CLOSED																			
12.0	21.5	42.0	-2.3	2.1	.1195	.483	.380	.491	.809	.385	.412	.414	.396	.385	.339	.339	.441	.791	
13.0	23.3	45.7	-2.7	-5.7	-.3069	.483	.434	.483	.568	.391	.413	.428	.434	.413	.393	.393	.435	.640	
14.0	23.3	45.7	-2.7	0.0	0.0000	.483	.471	.467	.512	.430	.437	.477	.432	.432	.422	.422	.433	.543	
15.0	23.0	45.1	-2.6	3.0	.0487	.483	.489	.466	.512	.443	.479	.500	.447	.447	.426	.426	.447	.468	
16.0	22.8	44.8	-2.6	3.0	.0247	.483	.495	.474	.514	.459	.490	.505	.444	.444	.423	.423	.444	.452	
17.0	22.5	44.2	-2.5	3.0	.0501	.483	.492	.468	.509	.462	.498	.511	.440	.440	.419	.419	.440	.462	
18.0	22.4	43.9	-2.5	5.0	.0294	.483	.499	.465	.506	.461	.493	.506	.439	.461	.417	.417	.439	.461	
19.0	22.2	43.6	-2.5	5.0	.0237	.483	.501	.468	.505	.459	.488	.501	.451	.451	.429	.429	.451	.451	
20.0	22.1	43.2	-2.4	5.0	.0260	.483	.511	.469	.504	.460	.491	.500	.447	.447	.425	.425	.447	.447	
21.0	21.9	42.9	-2.4	5.0	.0262	.483	.505	.470	.499	.457	.485	.499	.446	.446	.424	.424	.446	.446	
22.0	21.8	42.6	-2.4	5.0	.0255	.483	.496	.461	.496	.454	.483	.494	.461	.461	.439	.439	.461	.461	
23.0	21.6	42.3	-2.3	5.0	.0288	.483	.492	.459	.497	.459	.483	.497	.454	.454	.432	.432	.454	.454	
24.0	21.5	42.0	-2.3	5.0	.0271	.483	.493	.464	.504	.464	.491	.493	.448	.448	.425	.425	.448	.448	
25.0	21.3	41.7	-2.3	5.0	.0274	.483	.492	.461	.513	.470	.488	.495	.447	.447	.424	.424	.447	.447	
26.0	21.2	41.4	-2.2	5.0	.0277	.483	.495	.462	.504	.462	.483	.497	.449	.449	.426	.426	.449	.449	
27.0	21.2	41.4	-2.2	0.0	0.0000	.483	.490	.460	.501	.460	.488	.499	.446	.446	.423	.423	.446	.446	
28.0	21.0	41.0	-2.2	5.0	.0280	.483	.496	.461	.505	.463	.491	.502	.447	.447	.424	.424	.447	.447	
29.0	20.9	40.7	-2.2	5.0	.0283	.483	.496	.471	.505	.471	.489	.501	.445	.445	.422	.422	.445	.445	
30.0	20.7	40.4	-2.1	5.0	.0287	.483	.496	.467	.519	.479	.496	.498	.442	.442	.418	.418	.442	.442	
31.0	20.7	40.4	-2.1	0.0	0.0000	.483	.492	.463	.513	.473	.495	.499	.437	.437	.417	.417	.437	.437	
32.0	20.5	40.1	-2.1	5.0	.0290	.483	.490	.462	.509	.467	.495	.502	.436	.436	.416	.416	.436	.436	
33.0	20.4	39.8	-2.0	5.0	.0293	.483	.492	.457	.502	.461	.492	.502	.435	.435	.415	.415	.435	.435	
34.0	20.4	39.8	-2.0	0.0	0.0000	.483	.498	.462	.505	.465	.489	.498	.434	.434	.414	.414	.434	.434	



Table 11B — Inferred Pressurant Distribution, Scaling Run 239; Three 3.279-cm Nozzles

Pressurant Fractions (X) at Locations /															
$\beta$	$\beta/\theta$	$\bar{X}$	1 = 1	2	3	4	5	6	7	8	9	10	11	12	13
1.9	0.0000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
20.8	4.0103	0.050	-.284	-.077	500	-.064	-.139	-.119	0.005	-.058	-.064	0.003	0.005	0.065	100
9.9	.9389	.136	-.064	.954	.425	.066	.017	.034	.095	.034	.034	.054	.095	.747	.176
8.8	.7338	.205	.003	.073	.493	.176	.114	.165	.121	.103	.084	.121	.158	.359	.213
7.2	.4989	.258	.091	.247	.567	.217	.183	.224	.142	.142	.142	.152	.159	.891	.222
6.9	.4508	.302	.156	.267	.657	.251	.242	.272	.194	.210	.163	.163	.194	.940	.210
5.9	.3134	.338	.199	.278	.694	.258	.275	.311	.228	.228	.199	.228	.258	.920	.317
6.2	.2899	.368	.235	.280	.704	.291	.263	.294	.299	.313	.271	.243	.335	.927	.313
4.6	.1897	.394	.281	.325	.734	.286	.310	.383	.312	.298	.286	.273	.325	.955	.351
5.0	.1874	.416	.325	.357	.747	.352	.365	.397	.340	.327	.315	.315	.340	.927	.302
4.9	.1152	.429	.335	.367	.748	.364	.359	.394	.354	.362	.330	.330	.379	.950	.342
5.3	.1654	.447	.349	.380	.744	.375	.408	.436	.347	.358	.347	.347	.394	.946	.382
1.3	.0656	.461	.396	.455	.723	.390	.425	.464	.357	.368	.357	.357	.401	.916	.390
-3	-.0165	.464	.461	.474	.542	.408	.442	.459	.380	.402	.391	.391	.423	.775	.487
0.0	0.0000	.464	.470	.459	.457	.433	.470	.495	.423	.433	.423	.423	.444	.647	.455
5	.0285	.464	.480	.450	.422	.437	.480	.497	.441	.452	.441	.441	.430	.635	.430
1.1	.0580	.464	.487	.457	.420	.441	.476	.498	.420	.432	.441	.441	.441	.627	.431
1.2	.0295	.464	.491	.460	.416	.445	.485	.505	.421	.434	.443	.443	.443	.608	.421
6	.0306	.464	.500	.460	.408	.444	.484	.505	.437	.448	.437	.437	.437	.628	.404
6	.0310	.464	.507	.471	.412	.455	.498	.514	.430	.441	.430	.430	.430	.622	.396
20.0	.14.0	.464	.505	.480	.418	.459	.505	.528	.432	.443	.432	.421	.409	.603	.398
21.0	.13.9	.464	.493	.467	.412	.463	.509	.527	.430	.442	.430	.430	.430	.603	.396
22.0	.13.7	.464	.492	.464	.401	.453	.497	.518	.450	.450	.439	.439	.439	.578	.414
23.0	.13.6	.464	.494	.458	.400	.451	.494	.512	.449	.461	.426	.449	.449	.578	.414
24.0	.13.4	.464	.500	.455	.393	.446	.488	.507	.443	.455	.443	.443	.443	.597	.419
25.0	.13.4	.464	.496	.460	.394	.443	.488	.512	.441	.453	.441	.441	.441	.595	.429
26.0	.13.3	.464	.499	.461	.398	.446	.489	.511	.439	.451	.439	.439	.439	.595	.427
27.0	.13.1	.464	.497	.461	.396	.452	.495	.517	.437	.449	.437	.437	.437	.594	.425
28.0	.13.0	.464	.504	.465	.397	.450	.497	.514	.436	.448	.436	.436	.436	.594	.423
29.0	.12.8	.464	.506	.469	.395	.452	.496	.514	.435	.447	.435	.435	.435	.595	.422
30.0	.12.8	.464	.506	.469	.397	.449	.496	.516	.434	.447	.434	.434	.434	.595	.422
31.0	.12.7	.464	.509	.469	.399	.457	.494	.514	.432	.444	.432	.432	.432	.594	.419
32.0	.12.7	.464	.505	.468	.416	.458	.490	.515	.428	.466	.428	.428	.428	.590	.416
33.0	.12.5	.464	.501	.471	.418	.460	.493	.513	.438	.465	.425	.425	.425	.589	.416
7	.0354	.464	.498	.465	.421	.462	.503	.513	.444	.457	.419	.419	.419	.610	.406

Table 12B — Inferred Pressurant Distribution, Scaling Run 240, Three 3.279-cm Nozzles

i (in)	T (°C)	T (°C)	T (°C)	β	β/θ	X̄	I = 1	Pressurant Fractions (X) at Locations /												
								2	3	4	5	6	7	8	9	10	11	12	13	
COMMENCE VALVE OPENING																				
0.0	2.6	2.6	43.4	1.9	0.0000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000		
1.0	5.0	3.4	-4.7	75.6	3.2002	.041	-0.436	-0.077	.829	-0.008	-0.336	-0.336	-0.018	-0.167	-0.167	-0.067	.032	1.127		
VALVE FULLY OPEN																				
2.0	9.6	12.3	-9.4	13.3	1.2869	.130	-0.141	-0.015	.689	.092	-0.141	-0.150	.034	.010	.010	.058	.058	.882		
3.0	12.7	17.6	-7.0	8.2	.6511	.199	-0.069	.098	.668	.139	.009	.049	.082	.102	.062	.062	.102	.956		
4.0	14.3	21.0	-5.4	8.7	.6146	.254	-0.002	.221	.735	.153	.066	.093	.131	.131	.112	.131	.206	.981		
5.0	15.9	24.6	-4.9	5.5	.3262	.296	.085	.218	.771	.201	.150	.167	.170	.187	.153	.187	.255	.935		
6.0	16.2	26.6	-4.6	7.5	.4187	.334	.124	.262	.799	.255	.185	.201	.210	.210	.210	.210	.258	.975		
7.0	16.5	28.6	-4.6	6.3	.2968	.364	.183	.318	.827	.261	.228	.267	.273	.228	.228	.258	.318	1.011		
8.0	16.9	30.6	-4.6	5.3	.2210	.390	.223	.365	.841	.303	.269	.280	.286	.286	.271	.271	.356	.980		
9.0	16.6	31.5	-4.7	7.5	.2882	.413	.239	.397	.847	.295	.275	.328	.303	.317	.317	.317	.372	1.007		
10.0	17.1	33.3	-4.6	1.4	.0257	.425	.260	.355	.833	.336	.315	.339	.334	.347	.347	.347	.373	1.004		
COMMENCE VALVE CLOSURE																				
11.0	16.9	34.2	-5.0	6.1	.1901	.443	.310	.379	.834	.356	.341	.338	.349	.361	.336	.336	.412	.974		
12.0	16.3	35.3	-6.1	3.5	.1500	.459	.331	.418	.820	.346	.336	.370	.380	.387	.367	.367	.416	.972		
VALVE FULLY CLOSED																				
13.0	17.1	38.3	-7.4	-4.8	-.2083	.464	.389	.434	.690	.393	.393	.399	.389	.410	.410	.410	.443	.793		
14.0	17.4	39.0	-7.3	-1.2	-.0506	.464	.416	.440	.513	.412	.427	.433	.446	.437	.435	.437	.437	.631		
15.0	17.3	38.7	-7.4	.6	.0252	.464	.434	.443	.491	.426	.441	.434	.434	.436	.436	.436	.436	.625		
16.0	17.0	38.0	-7.4	1.2	.0512	.464	.443	.449	.489	.438	.443	.438	.434	.434	.434	.434	.432	.630		
17.0	16.7	37.4	-7.3	1.2	.0522	.464	.440	.453	.491	.444	.451	.462	.438	.439	.449	.449	.449	.617		
18.0	16.5	37.1	-7.3	.6	.0255	.464	.446	.457	.484	.452	.452	.461	.434	.446	.446	.446	.446	.626		
19.0	16.4	36.8	-7.2	.6	.0268	.464	.445	.457	.482	.454	.464	.461	.429	.441	.441	.441	.441	.645		
20.0	16.2	36.5	-7.2	.6	.0271	.464	.452	.459	.482	.464	.466	.464	.429	.441	.441	.441	.441	.624		
21.0	16.1	36.2	-7.2	.6	.0274	.464	.452	.459	.479	.459	.461	.465	.447	.439	.435	.435	.435	.620		
22.0	15.9	35.9	-7.1	.6	.0277	.464	.452	.457	.482	.464	.461	.471	.440	.432	.432	.440	.429	.615		
23.0	15.8	35.6	-7.1	.6	.0280	.464	.454	.461	.485	.464	.461	.473	.440	.432	.432	.428	.428	.616		
24.0	15.6	35.3	-7.0	.7	.0283	.464	.455	.459	.485	.459	.462	.474	.440	.432	.432	.429	.429	.618		
25.0	15.5	34.9	-7.0	.7	.0287	.464	.457	.464	.483	.457	.459	.471	.437	.437	.437	.426	.426	.616		
26.0	15.3	34.6	-7.0	.7	.0290	.464	.462	.467	.488	.455	.457	.469	.431	.433	.433	.426	.426	.611		
27.0	15.3	34.6	-7.0	0.0	0.0000	.464	.470	.473	.494	.453	.465	.475	.424	.437	.437	.437	.437	.605		
28.0	15.2	34.3	-6.9	.7	.0293	.464	.465	.479	.499	.453	.455	.472	.424	.436	.436	.436	.436	.618		
29.0	15.0	34.0	-6.9	.7	.0297	.464	.462	.467	.486	.452	.454	.469	.447	.435	.435	.435	.435	.631		
30.0	15.0	34.0	-6.9	0.0	0.0000	.464	.460	.463	.485	.455	.455	.467	.448	.436	.436	.436	.436	.631		
31.0	14.9	33.7	-6.8	.7	.0300	.464	.465	.463	.483	.458	.456	.470	.423	.436	.436	.436	.436	.633		
32.0	14.7	33.4	-6.8	.7	.0304	.464	.468	.460	.485	.463	.455	.470	.420	.433	.433	.433	.433	.632		
33.0	14.7	33.4	-6.8	0.0	0.0000	.464	.463	.458	.481	.458	.458	.466	.428	.433	.428	.428	.428	.640		
34.0	14.6	33.1	-6.8	.7	.0308	.464	.458	.461	.479	.453	.453	.461	.436	.448	.423	.423	.423	.674		

**Table 13B — Inferred Pressurant Distribution, Scaling Run 241; South 3.279-cm Nozzle**

Pressurant Fractions (X) at Locations /																
$\alpha$	$\beta$	$\beta/\alpha$	$\bar{X}$	1	2	3	4	5	6	7	8	9	10	11	12	13
COMMENCE VALVE OPENING																
0.0	16.7	16.7	22.4	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
1.0	18.4	18.3	23.1	0.19	0.472	0.335	0.73	1.78	283	514	-348	-138	-138	-348	-348	-348
VALVE FULLY OPEN																
2.0	22.2	22.3	20.5	0.57	-1.380	-1.156	-989	-933	-1.268	-1.604	1.472	1.472	633	913	633	1.472
3.0	25.0	26.0	14.9	0.91	-1.136	-1.100	-082	-082	-1.127	-1.145	392	303	124	213	303	303
4.0	27.5	28.6	12.2	1.21	0.02	0.19	0.19	0.13	0.07	-0.04	225	254	197	197	254	225
5.0	29.3	32.5	10.6	1.48	0.632	0.692	0.85	0.76	0.94	0.90	1.76	176	222	176	222	176
6.0	31.2	35.6	9.7	1.72	1.16	1.13	1.50	1.54	1.74	1.11	212	193	212	173	135	212
7.0	32.4	38.0	9.4	1.95	1.51	1.54	1.94	1.76	1.69	222	187	187	187	187	222	222
8.0	33.3	39.9	9.3	2.17	2.23	2.37	2.56	2.10	2.14	2.20	2.04	2.20	188	188	220	233
9.0	34.4	42.1	9.3	2.36	2.36	2.42	2.30	2.36	2.33	2.33	1.96	2.27	227	227	257	286
10.0	34.4	42.7	9.4	2.49	2.66	2.69	2.30	2.60	2.72	2.82	2.12	2.42	242	242	272	272
11.0	35.0	44.2	9.5	2.62	2.87	2.73	2.70	2.61	2.67	2.70	2.04	2.18	261	261	304	304
12.0	35.7	46.0	9.6	2.81	2.84	2.81	2.62	2.70	2.84	2.94	2.29	2.29	284	284	338	338
13.0	35.2	46.0	9.7	2.98	3.32	3.18	2.93	3.15	3.40	3.54	2.02	2.30	285	285	312	326
14.0	35.7	47.3	9.9	3.11	3.33	3.39	3.65	3.44	3.33	3.30	2.58	2.32	312	285	312	312
15.0	36.6	49.2	10.0	3.23	4.00	3.84	3.49	3.41	3.18	3.00	2.82	3.21	308	308	322	333
16.0	36.7	50.0	10.1	3.36	3.96	3.96	3.73	3.73	3.40	3.18	2.85	3.10	310	310	325	335
17.0	36.8	50.9	10.2	3.47	3.75	3.72	3.70	3.65	3.60	3.58	2.76	2.89	326	350	326	363
18.0	36.8	51.6	10.3	3.59	4.00	3.93	3.66	3.81	3.83	3.76	2.65	2.89	337	313	317	410
19.0	36.3	51.3	10.4	3.66	4.11	4.04	4.18	4.18	4.01	3.87	2.59	2.59	337	333	333	382
20.0	36.6	52.3	10.4	3.76	4.38	4.26	4.26	4.24	4.17	4.34	2.78	2.90	350	314	326	374
21.0	36.3	52.4	10.5	3.86	4.26	4.38	4.36	4.48	4.43	4.07	2.81	3.28	328	328	342	400
22.0	35.8	52.2	10.6	3.96	4.20	4.20	4.32	4.41	4.46	4.37	3.02	3.02	374	374	422	398
23.0	36.5	53.9	10.7	4.02	4.27	4.29	4.36	4.27	4.23	4.11	3.07	3.76	399	376	422	422
24.0	36.4	54.3	10.8	4.10	4.35	4.32	4.30	4.16	4.23	4.12	3.13	3.47	405	416	428	439
25.0	36.5	55.0	10.8	4.18	4.11	4.11	4.22	4.02	4.06	4.06	3.25	3.47	438	438	481	483
26.0	36.2	54.8	10.8	4.23	4.20	4.30	4.28	4.28	4.28	4.51	3.21	3.44	412	435	455	481
27.0	35.5	54.2	10.9	4.31	4.44	4.56	4.56	4.51	4.60	4.63	3.13	3.47	428	458	474	483
COMMENCE VALVE CLOSURE																
28.0	35.1	54.0	10.9	4.38	4.60	4.63	4.67	4.63	4.67	4.72	3.56	3.56	425	435	449	472
29.0	35.0	54.3	10.9	4.45	4.56	4.71	4.94	4.64	4.73	4.67	3.61	3.61	441	441	441	441
VALVE FULLY CLOSED																
30.0	34.8	54.5	10.8	4.51	512	503	487	494	505	519	386	386	409	409	432	409
31.0	36.9	58.2	10.9	4.51	504	494	483	479	473	490	382	392	413	424	454	456
32.0	38.0	60.1	11.0	4.51	489	493	499	477	467	450	391	391	432	432	452	452
33.0	38.5	61.1	11.0	4.51	489	489	481	465	461	455	391	391	431	431	451	471
34.0	38.8	61.5	11.1	4.51	490	494	480	470	460	452	381	401	430	440	460	460
35.0	38.9	61.8	11.1	4.51	491	483	481	457	457	463	390	390	430	430	449	469
36.0	39.1	62.1	11.1	4.51	481	478	468	452	464	466	385	385	434	444	464	483
37.0	39.1	62.1	11.1	4.51	480	480	466	464	458	456	403	403	442	442	481	462
38.0	38.9	61.8	11.1	4.51	471	471	465	461	463	467	400	419	459	439	459	455
39.0	38.9	61.8	11.1	4.51	458	460	470	472	476	468	386	425	445	445	464	464
40.0	38.9	61.8	11.1	4.51	456	462	471	469	481	479	381	420	440	440	460	460
41.0	38.8	61.5	11.1	4.51	460	464	472	474	478	476	395	425	435	435	455	455
42.0	38.6	61.2	11.0	4.51	457	464	476	468	470	470	405	425	445	445	464	445
43.0	38.5	61.0	11.0	4.51	459	463	471	467	463	473	403	423	443	443	463	443
44.0	38.3	60.7	11.0	4.51	463	463	469	467	463	475	403	423	443	443	463	443
45.0	38.3	60.7	11.0	4.51	465	461	465	465	461	469	400	441	441	441	461	441
46.0	38.1	60.4	11.0	4.51	464	460	462	462	466	466	418	438	438	458	458	438
47.0	38.1	60.4	11.0	4.51	466	466	458	456	456	472	425	435	445	435	456	435
48.0	38.0	60.1	11.0	4.51	465	467	457	451	455	472	433	433	453	453	453	433
49.0	38.0	60.1	11.0	4.51	473	463	463	463	459	459	430	430	451	451	461	461
50.0	37.8	59.9	11.0	4.51	472	464	460	452	466	466	444	448	448	448	468	420

Table 14B — Inferred Pressurant Distribution, Scaling Run 242; South 3.279-cm Nozzle  
Pressurant Fractions (X) at Locations /

$t$ (s)	$\bar{T}$ (°C)	$\bar{T}_c$ (°C)	$T_c$ (°C)	$\beta$	$\beta/\theta$	$\bar{X}$	1	2	3	4	5	6	7	8	9	10	11	12	13
COMMENCE VALVE OPENING																			
0.0	19.7	19.7	65.1	1.9	0.0000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
1.0	22.3	21.9	35.6	92.5	2.6076	.029	.201	.165	.020	.049	.143	.230	-.052	-.032	-.080	-.008	-.016	-.008	-.032
VALVE FULLY OPEN																			
2.0	25.9	25.5	31.2	2.2	.0043	.065	.410	.418	.410	.401	.472	.490	-.329	-.240	-.151	-.329	-.151	-.329	-.240
3.0	28.8	28.9	28.0	1.1	.0379	.058	-2.431	-2.101	-2.087	-2.087	-2.316	-2.316	3.087	1.937	1.363	2.512	1.363	2.512	1.363
4.0	30.9	31.6	25.0	2.9	.0965	.127	-.140	-.105	-.122	-.122	-.122	-.122	-.227	.593	.331	.157	.244	.244	.593
5.0	32.9	34.2	25.9	6.6	.0195	.154	.035	-.014	-.026	.011	-.026	-.026	.240	.240	.240	.301	.301	.301	.422
6.0	34.1	36.0	25.2	2.2	.0032	.170	.129	.083	.129	.110	.101	.027	.166	.166	.166	.213	.213	.213	.298
7.0	35.4	37.8	25.2	3.4	.0945	.192	.230	.222	.175	.230	.238	.238	.127	.127	.127	.206	.206	.206	.206
8.0	36.8	40.0	24.0	1.1	.0270	.213	.311	.251	.251	.205	.172	.146	.185	.185	.185	.218	.218	.218	.284
9.0	37.5	41.6	23.9	4.6	.1173	.232	.277	.232	.186	.158	.181	.249	.192	.192	.192	.249	.249	.249	.333
10.0	37.5	42.3	23.3	7.7	.2013	.252	.249	.239	.249	.239	.265	.249	.217	.217	.217	.244	.244	.244	.351
11.0	38.3	43.9	23.0	2.0	.0636	.269	.270	.280	.261	.275	.280	.275	.179	.179	.179	.251	.251	.251	.347
12.0	38.4	44.6	22.0	7.0	.1589	.285	.317	.298	.294	.325	.349	.335	.110	.110	.110	.271	.271	.271	.362
13.0	38.9	45.9	22.3	3.0	.0760	.299	.330	.350	.330	.337	.337	.341	.158	.158	.158	.286	.286	.286	.350
14.0	39.3	47.2	21.9	3.9	.0721	.312	.356	.375	.344	.371	.375	.364	.158	.158	.158	.296	.296	.296	.375
15.0	39.1	47.4	21.0	7.9	.1093	.322	.351	.362	.339	.347	.355	.350	.202	.202	.202	.300	.300	.300	.375
16.0	39.3	48.3	21.4	4.9	.0887	.334	.351	.343	.328	.333	.343	.331	.228	.228	.228	.339	.339	.339	.432
17.0	39.8	49.8	20.6	2.0	.0432	.345	.370	.365	.354	.354	.361	.352	.261	.261	.261	.347	.347	.347	.416
18.0	39.9	50.4	20.6	5.4	.0939	.356	.371	.364	.371	.360	.361	.377	.277	.277	.277	.310	.310	.310	.427
19.0	39.9	51.2	20.2	9.1	.0891	.367	.390	.382	.366	.380	.401	.404	.291	.291	.291	.372	.372	.372	.404
20.0	39.4	51.2	20.0	9.1	.1533	.377	.409	.393	.397	.416	.429	.429	.272	.272	.272	.388	.388	.388	.400
21.0	39.2	51.7	19.3	6.9	.1059	.387	.430	.429	.410	.432	.447	.480	.265	.265	.265	.373	.373	.373	.404
22.0	39.6	52.5	19.4	7.7	.0939	.392	.472	.454	.427	.424	.409	.388	.312	.312	.312	.357	.357	.357	.388
23.0	38.9	52.2	19.0	10.7	.1727	.401	.480	.453	.429	.405	.372	.360	.302	.302	.302	.393	.393	.393	.423
24.0	38.0	52.7	18.7	6.5	.0886	.409	.469	.425	.419	.401	.398	.385	.310	.310	.310	.413	.413	.413	.501
25.0	39.3	54.2	18.5	-6.6	-.0068	.416	.439	.425	.419	.419	.419	.419	.321	.321	.321	.419	.419	.419	.489
26.0	39.2	54.7	18.1	6.2	.0787	.423	.451	.440	.427	.440	.418	.413	.315	.315	.315	.442	.442	.442	.478
27.0	39.6	56.1	17.5	8.0	.0089	.429	.439	.421	.410	.431	.428	.444	.335	.335	.335	.465	.465	.465	.517
COMMENCE VALVE CLOSURE																			
28.0	38.8	55.4	17.4	12.0	.1620	.437	.474	.445	.430	.459	.474	.487	.322	.322	.322	.440	.440	.440	.493
29.0	37.9	54.6	17.0	5.7	.1682	.443	.487	.479	.476	.476	.484	.487	.330	.330	.330	.423	.423	.423	.503
VALVE FULLY CLOSED																			
30.0	38.1	57.2	14.6	6.0	.0183	.448	.495	.481	.465	.479	.481	.484	.352	.352	.352	.434	.434	.434	.481
31.0	40.4	61.1	14.0	-9.7	-.2072	.448	.488	.484	.475	.468	.466	.473	.350	.350	.350	.447	.447	.447	.468
32.0	41.5	63.0	14.9	-4.5	-.1322	.448	.486	.483	.444	.454	.469	.484	.384	.384	.384	.457	.457	.457	.477
33.0	42.1	64.1	15.0	-2.5	-.0725	.448	.502	.471	.449	.457	.467	.489	.371	.371	.371	.463	.463	.463	.463
34.0	42.4	64.7	15.0	-1.2	-.0355	.448	.498	.482	.460	.458	.464	.478	.369	.369	.369	.456	.456	.456	.476
35.0	42.6	65.0	15.0	-6.6	-.0176	.448	.483	.475	.465	.463	.473	.481	.375	.375	.375	.465	.465	.465	.465
36.0	42.6	65.0	15.0	0.0	0.0000	.448	.479	.473	.467	.471	.473	.473	.367	.367	.367	.457	.457	.457	.477
37.0	42.6	65.0	15.0	0.0	0.0000	.448	.485	.483	.459	.459	.461	.485	.375	.375	.375	.445	.445	.445	.455
38.0	42.6	65.0	15.0	0.0	0.0000	.448	.465	.459	.453	.453	.463	.485	.371	.371	.371	.441	.441	.441	.471
39.0	42.4	64.7	15.0	6.0	.0176	.448	.453	.451	.457	.455	.465	.475	.393	.393	.393	.453	.453	.453	.453
40.0	42.3	64.4	15.0	6.0	.0177	.448	.457	.453	.457	.461	.477	.485	.398	.398	.398	.449	.449	.449	.459
41.0	42.1	64.1	15.0	6.0	.0178	.448	.456	.454	.456	.462	.476	.478	.401	.401	.401	.462	.462	.462	.462
42.0	42.0	64.1	15.0	0.0	0.0000	.448	.453	.451	.451	.461	.469	.473	.406	.406	.406	.457	.457	.457	.477
43.0	42.0	63.1	15.9	6.0	.0179	.448	.462	.457	.451	.464	.474	.477	.379	.379	.379	.453	.453	.453	.474
44.0	42.0	62.6	16.5	0.0	0.0000	.448	.456	.449	.447	.462	.469	.473	.388	.388	.388	.443	.443	.443	.486
45.0	41.8	61.6	17.3	6.0	.0181	.448	.466	.468	.463	.461	.466	.475	.382	.382	.382	.439	.439	.439	.450
46.0	41.6	60.7	18.2	6.0	.0182	.448	.474	.466	.453	.462	.471	.479	.398	.398	.398	.434	.434	.434	.493
47.0	41.6	60.0	19.0	0.0	0.0000	.448	.476	.467	.449	.471	.474	.483	.393	.393	.393	.430	.430	.430	.503
48.0	41.5	59.1	19.7	6.0	.0183	.448	.475	.469	.472	.480	.480	.493	.399	.399	.399	.424	.424	.424	.500
49.0	41.5	58.7	20.3	0.0	0.0000	.448	.470	.454	.451	.464	.477	.490	.430	.430	.430	.417	.417	.417	.496
50.0	41.5	58.2	20.9	0.0	0.0000	.448	.477	.464	.466	.469	.472	.498	.402	.402	.402	.415	.415	.415	.496

Table 15B — Inferred Pressurant Distribution, Scaling Run 243; South 3.279-cm Nozzle  
Pressurant Fractions (X) at Locations /

Pressurant Fractions (X) at Locations /																		

Table 16B — Inferred Pressurant Distribution, Sealing Run 244; South 3.279-cm Nozzle

Pressurant Fractions (X) at Locations I																					
	$\bar{t}$ (s)	$\bar{T}$ (°C)	$\bar{T}_c$ (°C)	$\bar{T}_p$ (°C)	$\beta$	$\beta/\theta$	$\bar{X}$	I = 1	2	3	4	5	6	7	8	9	10	11	12	13	
COMMENCE VALVE OPENING																					
	0.0	17.6	17.6	18.9	4	0.0000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
	1.0	19.6	19.5	24.6	92.0	2.0273	0.022	378	262	029	126	281	358	-164	-164	-164	-164	-164	-164	-164	
VALVE FULLY OPEN																					
	2.0	23.5	23.5	23.0	6.9	2637	0.059	-4	174	-3	039	-4	363	-5	308	3	578	2	633	4	523
	3.0	26.5	27.5	17.3	8	0279	0.093	-093	-093	-084	-143	-162	282	282	183	378	3	578	2	633	4
	4.0	28.7	30.8	14.1	2.5	0843	0.123	-008	-002	034	034	004	-008	251	281	191	221	161	251	191	
	5.0	30.6	33.8	12.6	3.1	0632	0.150	093	084	103	093	084	070	197	244	197	197	150	244	197	
	6.0	32.0	36.3	11.8	3.6	1067	0.175	163	138	138	146	126	130	171	252	191	171	191	232	232	
	7.0	33.7	39.2	11.2	-1	-0025	0.197	161	161	175	172	175	143	200	236	200	200	200	272	272	
	8.0	35.1	41.8	11.0	7	0172	0.218	204	204	204	214	220	201	201	217	217	217	217	249	266	
	9.0	35.6	43.4	10.9	5.1	1342	0.238	244	251	241	238	235	214	177	238	208	238	300	266	266	
	10.0	36.2	44.7	10.9	2.3	0357	0.249	244	250	247	238	220	232	208	267	238	238	327	297	297	
	11.0	36.4	45.8	10.9	6.1	1490	0.268	285	285	251	268	280	320	191	234	263	263	306	306	306	
	12.0	37.2	47.5	11.0	2.3	0495	0.283	301	299	307	301	301	326	217	244	271	271	244	299	299	
	13.0	37.5	48.8	11.0	4.4	0931	0.290	319	297	290	298	301	325	229	295	282	295	335	327	327	
	14.0	38.1	50.2	11.2	2.7	0510	0.311	323	312	310	325	328	320	271	323	297	297	323	323	323	
	15.0	37.8	50.7	11.3	7.2	1480	0.325	349	349	334	329	331	323	255	280	318	306	331	369	336	
	16.0	37.5	50.0	11.4	8.4	1681	0.339	340	350	350	347	360	365	259	284	335	335	385	360	360	
	17.0	37.5	51.6	11.5	5.3	0894	0.350	378	376	376	373	388	396	261	273	323	336	361	373	361	
	18.0	38.0	52.9	11.6	2.0	0323	0.360	402	394	397	399	387	358	249	297	346	346	394	370	370	
	19.0	38.2	53.6	11.7	2.9	0296	0.367	426	412	391	393	376	364	262	286	357	333	397	405	405	
	20.0	38.1	54.0	11.8	6.1	0996	0.377	400	395	412	398	372	360	270	341	365	365	437	412	412	
	21.0	37.7	54.1	11.8	8.0	1363	0.387	394	404	387	397	399	397	295	342	366	390	437	437	437	
	22.0	38.0	55.1	11.9	2.8	0398	0.396	402	402	402	411	420	397	311	358	381	392	450	427	427	
	23.0	38.3	56.1	11.9	1.6	0202	0.403	410	412	410	426	419	414	306	374	396	396	441	441	441	
	24.0	38.5	57.0	12.0	2.9	0376	0.411	408	413	419	433	417	404	319	386	442	419	408	442	430	
	25.0	39.0	58.3	12.1	-9	-0103	0.417	413	400	415	415	408	415	339	404	447	426	466	447	447	
	26.0	38.4	57.7	12.1	11.4	1229	0.423	436	436	431	444	453	488	352	374	418	418	396	440	418	
	27.0	37.7	57.2	12.1	10.3	1435	0.431	456	458	458	458	476	491	356	389	411	411	411	422	411	
	28.0	36.9	56.4	12.1	11.8	1619	0.439	469	460	469	469	478	489	379	401	424	401	424	424	424	
COMMENCE VALVE CLOSURE																					
	29.0	37.0	56.9	12.1	4.4	0484	0.445	468	466	489	491	497	486	386	397	431	408	431	431	431	
	30.0	37.1	57.7	12.1	9	0192	0.451	473	471	469	495	482	475	396	418	440	440	440	440	440	
VALVE FULLY CLOSED																					
	31.0	37.2	58.1	12.0	4	0100	0.454	475	473	466	479	481	477	401	423	466	445	423	445	445	
	32.0	38.8	60.9	12.1	-8.8	-1961	0.454	466	454	470	472	472	476	399	440	460	450	440	450	450	
	33.0	39.7	62.6	12.2	-5.0	-1167	0.454	457	451	451	461	467	470	395	455	455	455	474	455	455	
	34.0	40.1	63.2	12.2	-1.6	-0359	0.454	470	464	458	458	464	473	407	446	446	446	466	466	466	
	35.0	40.2	63.5	12.3	-8	-0177	0.454	489	462	450	456	462	469	391	430	450	450	469	469	469	
	36.0	40.4	63.7	12.3	-8	-0176	0.454	483	456	448	450	458	462	402	431	460	460	479	460	460	
	37.0	40.4	63.7	12.3	0.0	0.0000	0.454	477	467	460	456	464	467	399	419	458	458	477	458	458	
	38.0	40.4	63.7	12.3	0.0	0.0000	0.454	485	461	444	448	459	457	409	428	457	448	487	457	457	
	39.0	40.2	63.5	12.3	8	0176	0.454	473	459	457	457	457	461	403	422	461	461	442	481	461	
	40.0	40.1	63.2	12.2	8	0177	0.454	468	460	458	460	462	466	399	419	458	458	477	458	458	
	41.0	39.9	62.9	12.2	8	0179	0.454	464	457	455	461	463	466	415	425	455	455	474	455	455	
	42.0	39.9	62.9	12.2	0.0	0.0000	0.454	462	454	456	462	464	470	413	413	452	472	452	472	452	
	43.0	39.7	62.6	12.2	8	0180	0.454	459	451	455	467	469	472	407	417	467	467	457	467	457	
	44.0	39.6	62.3	12.2	8	0181	0.454	454	446	458	464	468	480	418	418	458	458	458	458	458	
	45.0	39.6	62.3	12.2	0.0	0.0000	0.454	452	450	458	464	464	480	414	424	454	454	474	454	454	
	46.0	39.4	62.1	12.2	8	0182	0.454	453	449	461	465	463	475	405	425	465	465	465	465	465	
	47.0	39.4	62.1	12.2	0.0	0.0000	0.454	466	458	462	470	464	472	418	418	458	458	458	458	458	
	48.0	39.3	61.8	12.2	8	0184	0.454	469	463	461	465	461	483	409	419	469	449	469	449	449	
	49.0	39.3	61.8	12.2	0.0	0.0000	0.454	473	467	467	471	459	463	402	423	463	463	463	463	463	
	50.0	39.1	61.5	12.2	8	0185	0.454	471	471	471	477	465	467	400	420	441	441	441	441	441	

Table 17B — Inferred Pressurant Distribution, Sealing Run 245; South 3.279-cm Nozzle

$\theta$	$\beta$	$\beta/\theta$	$\bar{X}$	Pressurant Fractions ( $X$ ) at Locations /												
				1	2	3	4	5	6	7	8	9	10	11	12	13
CONFORMANCE VALVE OPENING																
0.0	26.1	26.1	54.6	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
1.0	28.5	28.1	44.2	.022	.178	.153	.091	.109	.153	.184	-.127	-.065	-.065	-.065	-.127	-.065
VALVE FULLY OPEN																
2.0	32.5	32.2	39.2	.060	.546	.496	.496	.546	.629	.596	-.516	-.433	-.267	-.267	-.433	-.350
3.0	35.3	35.3	35.8	.095	5.730	5.321	4.298	3.684	4.911	4.707	-6.547	-4.501	-2.455	-2.455	-4.501	-5.014
4.0	37.8	38.4	33.5	.125	-.265	-.306	-.223	-.182	-.265	-.389	.791	.584	.273	.170	.273	.584
5.0	39.6	40.7	32.9	.147	-.134	-.032	-.198	-.070	-.070	-.019	.493	.429	.211	.173	.211	.493
6.0	41.4	43.4	32.6	.178	.048	.048	.031	.109	.065	.074	.293	.337	.162	.162	.162	.337
7.0	42.9	45.7	31.5	.201	.137	.137	.109	.137	.109	.109	.328	.328	.186	.186	.186	.328
8.0	43.3	46.0	30.7	.215	.188	.175	.132	.175	.212	.237	.293	.293	.231	.169	.169	.293
9.0	43.9	48.1	30.5	.236	.263	.241	.201	.212	.212	.224	.258	.258	.201	.229	.229	.258
10.0	44.5	49.4	30.2	.255	.266	.261	.234	.255	.261	.266	.266	.224	.224	.224	.224	.266
11.0	45.6	51.4	30.0	.272	.283	.272	.266	.286	.272	.291	.296	.296	.223	.223	.223	.296
12.0	46.3	53.4	29.8	.287	.301	.301	.301	.326	.314	.306	.175	.297	.257	.257	.257	.326
13.0	47.1	55.0	29.5	.301	.344	.341	.318	.306	.318	.321	.149	.264	.245	.245	.245	.341
14.0	46.9	55.5	29.5	.316	.326	.319	.304	.311	.330	.374	.200	.274	.274	.311	.311	.374
15.0	47.0	56.1	29.0	.325	.386	.372	.329	.336	.354	.368	.179	.286	.286	.286	.286	.368
16.0	46.9	56.9	27.5	.342	.437	.400	.369	.369	.349	.342	.267	.267	.301	.301	.301	.369
17.0	47.4	58.2	27.4	.349	.438	.431	.389	.376	.363	.341	.263	.263	.320	.293	.293	.363
18.0	47.8	59.7	26.6	.360	.427	.415	.400	.391	.369	.381	.215	.261	.381	.336	.306	.381
19.0	48.5	61.5	26.3	.369	.410	.404	.393	.415	.401	.413	.240	.296	.381	.353	.325	.381
20.0	48.0	61.3	26.3	.380	.429	.386	.401	.418	.449	.481	.235	.249	.321	.349	.378	.449
21.0	48.3	62.6	25.7	.388	.462	.457	.454	.459	.470	.476	.259	.232	.286	.313	.367	.421
22.0	48.0	62.8	25.3	.395	.464	.459	.467	.467	.472	.483	.232	.232	.312	.339	.392	.419
23.0	48.1	63.4	25.4	.403	.495	.475	.485	.466	.477	.479	.232	.245	.351	.391	.390	.429
24.0	48.0	64.2	24.8	.411	.485	.463	.465	.460	.460	.472	.283	.283	.359	.384	.435	.460
25.0	47.9	65.0	24.2	.419	.479	.455	.455	.460	.462	.469	.318	.318	.342	.367	.367	.428
26.0	47.8	65.5	24.0	.426	.468	.479	.474	.474	.463	.462	.325	.349	.373	.397	.373	.445
CONFORMANCE VALVE CLOSURE																
27.0	48.1	66.7	23.5	.432	.507	.470	.465	.460	.451	.420	.351	.363	.375	.409	.432	.467
28.0	46.8	65.6	23.0	.441	.534	.520	.494	.487	.450	.437	.365	.341	.341	.388	.412	.459
VALVE FULLY CLOSED																
29.0	46.9	67.3	21.5	.445	.525	.505	.481	.481	.488	.492	.335	.333	.355	.376	.420	.485
30.0	49.4	71.6	21.7	.445	.495	.487	.489	.459	.463	.467	.377	.357	.387	.397	.437	.477
31.0	50.9	74.1	21.9	.445	.496	.482	.489	.461	.469	.463	.333	.332	.428	.428	.448	.486
32.0	51.6	75.2	22.0	.445	.483	.481	.475	.462	.458	.471	.372	.372	.428	.428	.438	.475
33.0	51.9	75.7	22.1	.445	.471	.473	.469	.462	.463	.469	.397	.387	.424	.424	.443	.462
34.0	52.1	76.0	22.1	.445	.469	.465	.467	.462	.463	.465	.410	.391	.428	.437	.428	.456
35.0	52.1	76.0	22.1	.445	.473	.469	.466	.466	.466	.471	.473	.397	.434	.415	.415	.453
36.0	52.1	76.0	22.1	.445	.471	.469	.468	.462	.465	.465	.406	.406	.425	.425	.425	.452
37.0	52.1	76.0	22.1	.445	.468	.468	.471	.462	.464	.468	.405	.405	.423	.423	.423	.460
38.0	51.9	75.7	22.1	.445	.467	.465	.476	.467	.468	.481	.401	.401	.420	.420	.420	.457
39.0	51.7	75.5	22.1	.445	.465	.467	.477	.467	.467	.470	.396	.396	.415	.415	.415	.452
40.0	51.6	75.2	22.0	.445	.467	.464	.467	.466	.467	.471	.396	.405	.424	.424	.424	.462
41.0	51.4	74.9	22.0	.445	.468	.464	.468	.465	.469	.476	.399	.418	.418	.418	.418	.456
42.0	51.4	74.8	22.1	.445	.473	.473	.465	.463	.469	.476	.395	.414	.414	.414	.414	.456
43.0	51.2	73.8	23.0	.445	.472	.472	.468	.466	.466	.472	.393	.403	.422	.422	.422	.462
44.0	51.1	72.9	23.8	.445	.468	.468	.466	.466	.468	.474	.395	.395	.415	.415	.415	.457
45.0	51.1	72.3	24.5	.445	.468	.468	.468	.473	.473	.479	.389	.410	.410	.410	.410	.453
46.0	50.9	71.6	25.1	.445	.464	.464	.467	.469	.471	.482	.424	.424	.402	.402	.402	.488
47.0	50.7	70.7	25.8	.445	.459	.461	.461	.465	.467	.483	.396	.418	.396	.407	.418	.456
48.0	50.7	70.4	26.2	.445	.453	.465	.458	.469	.465	.479	.390	.424	.390	.406	.424	.456
49.0	50.7	69.9	26.8	.445	.453	.458	.455	.471	.460	.476	.393	.430	.393	.407	.430	.476
50.0	50.6	69.1	27.4	.445	.449	.456	.456	.473	.459	.475	.396	.420	.396	.420	.420	.452

Table 18B — Inferred Pressurant Distribution, Scaling Run 246; South 3.279-cm Nozzle

Pressurant Fractions (X) at Locations /																			
r (°)	T (°C)	T <sub>0</sub> (°C)	T <sub>1</sub> (°C)	β	R/θ	X̄	1 - 1	2	3	4	5	6	7	8	9	10	11	12	13
COMMENCE VALVE OPENING																			
0.0	16.2	16.2	25.3	5	0.0000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
1.0	18.0	17.9	22.0	93.4	1.0204	0.019	0.519	0.324	0.079	0.177	0.275	0.397	0.409	0.165	0.165	0.165	0.165	0.165	0.165
VALVE FULLY OPEN																			
2.0	21.6	21.8	19.2	10.7	0.4130	0.056	0.937	0.605	0.259	0.453	0.724	0.918	0.980	0.787	0.399	0.593	0.787	0.593	0.399
3.0	25.0	28.0	14.4	-4.0	-0.1662	0.089	-0.078	-0.027	-0.018	-0.044	-0.112	-0.112	0.324	0.239	0.153	0.153	0.239	0.153	0.239
4.0	27.3	29.4	11.9	1.2	-0.0462	0.118	0.062	0.030	0.030	0.030	0.019	0.025	0.324	0.260	0.176	0.148	0.232	0.176	0.232
5.0	28.9	32.2	9.9	3.2	0.0230	0.146	0.080	0.077	0.061	0.110	0.083	0.056	0.222	0.222	0.177	0.133	0.222	0.177	0.133
6.0	30.6	35.0	9.1	6.8	0.0234	0.169	0.115	0.127	0.127	0.135	0.135	0.131	0.204	0.224	0.166	0.166	0.224	0.166	0.224
7.0	32.6	37.5	8.0	2.6	0.0740	0.192	0.183	0.180	0.172	0.165	0.155	0.162	0.218	0.218	0.183	0.183	0.218	0.183	0.218
8.0	33.6	39.0	8.7	6	0.1638	0.214	0.225	0.228	0.221	0.215	0.198	0.208	0.225	0.208	0.175	0.208	0.225	0.175	0.208
9.0	33.4	40.8	8.6		0.1002	0.234	0.259	0.244	0.221	0.231	0.222	0.219	0.206	0.206	0.206	0.222	0.206	0.222	0.206
10.0	34.2	42.8	8.8		0.0544	0.251	0.307	0.289	0.275	0.245	0.245	0.230	0.177	0.222	0.222	0.222	0.236	0.222	0.236
11.0	35.0	44.5	8.9		-0.0532	0.267	0.297	0.297	0.281	0.275	0.264	0.244	0.205	0.205	0.261	0.261	0.275	0.261	0.275
12.0	36.1	46.4	9.0		-0.0582	0.275	0.303	0.314	0.319	0.303	0.282	0.255	0.191	0.164	0.241	0.271	0.264	0.319	0.289
13.0	36.8	48.0	9.1	0	0.0402	0.290	0.295	0.300	0.303	0.303	0.287	0.272	0.236	0.213	0.290	0.303	0.316	0.316	0.316
14.0	36.9	49.1	9.2	4.8	0.0972	0.304	0.334	0.344	0.339	0.326	0.326	0.319	0.196	0.221	0.286	0.296	0.309	0.321	0.321
15.0	36.7	49.5	9.3	7.2	0.1489	0.318	0.344	0.354	0.364	0.352	0.354	0.359	0.217	0.205	0.294	0.306	0.317	0.342	0.342
16.0	36.7	49.5	9.4	8.7	0.1784	0.332	0.366	0.378	0.366	0.364	0.378	0.381	0.231	0.231	0.306	0.319	0.336	0.331	0.331
17.0	36.0	49.9	9.5	7.0	0.1254	0.344	0.381	0.378	0.381	0.363	0.378	0.388	0.227	0.240	0.314	0.326	0.351	0.376	0.363
18.0	36.3	50.9	9.7	4.0	0.0644	0.354	0.387	0.389	0.396	0.382	0.374	0.374	0.258	0.282	0.331	0.331	0.367	0.379	0.355
19.0	36.4	51.5	9.8	3.8	0.0390	0.361	0.391	0.384	0.375	0.382	0.375	0.384	0.233	0.293	0.341	0.353	0.389	0.389	0.389
20.0	37.2	53.2	9.9	-2.0	-0.0267	0.369	0.387	0.399	0.399	0.392	0.387	0.382	0.233	0.322	0.346	0.346	0.357	0.403	0.392
21.0	37.3	54.0	9.9	3.8	0.0557	0.379	0.419	0.399	0.388	0.406	0.394	0.397	0.230	0.313	0.358	0.358	0.392	0.403	0.403
22.0	37.0	54.2	10.0	7.3	0.1111	0.388	0.435	0.403	0.383	0.392	0.424	0.437	0.281	0.338	0.360	0.372	0.394	0.417	0.406
23.0	36.6	54.1	10.0	8.5	0.1270	0.397	0.445	0.445	0.434	0.439	0.449	0.448	0.291	0.268	0.359	0.359	0.416	0.427	0.387
24.0	36.4	54.4	10.1	6.0	0.0792	0.405	0.466	0.459	0.457	0.450	0.457	0.459	0.293	0.297	0.364	0.364	0.410	0.432	0.387
25.0	36.8	55.4	10.1	1.2	0.0138	0.412	0.470	0.463	0.450	0.450	0.448	0.452	0.247	0.291	0.379	0.401	0.434	0.445	0.423
26.0	36.0	54.7	10.1	13.2	0.1391	0.422	0.472	0.474	0.467	0.472	0.463	0.429	0.234	0.301	0.391	0.413	0.425	0.456	0.426
27.0	36.5	55.9	10.2	-1.1	-0.0122	0.424	0.457	0.465	0.464	0.426	0.420	0.429	0.239	0.321	0.398	0.399	0.469	0.474	0.441
28.0	37.0	57.2	10.2	-1.8	-0.0177	0.430	0.459	0.465	0.463	0.426	0.467	0.463	0.237	0.340	0.425	0.425	0.414	0.446	0.446
COMMENCE VALVE CLOSURE																			
29.0	36.1	56.2	10.2	12.4	0.1739	0.438	0.512	0.497	0.476	0.465	0.473	0.510	0.315	0.358	0.391	0.402	0.413	0.434	0.445
30.0	36.0	56.7	10.2	2.5	0.0489	0.444	0.497	0.495	0.491	0.485	0.485	0.487	0.332	0.353	0.418	0.418	0.407	0.439	0.461
VALVE FULLY CLOSED																			
31.0	35.8	56.7	10.1	3.2	0.0638	0.449	0.512	0.489	0.489	0.491	0.489	0.512	0.332	0.364	0.407	0.418	0.439	0.450	0.450
32.0	37.4	59.6	10.1	-9.9	-0.1931	0.459	0.510	0.494	0.494	0.490	0.492	0.492	0.334	0.385	0.426	0.426	0.416	0.426	0.446
33.0	38.0	60.7	10.2	-3.8	-0.0740	0.469	0.497	0.487	0.487	0.483	0.471	0.477	0.337	0.396	0.436	0.436	0.426	0.436	0.456
34.0	38.5	61.5	10.2	-2.7	-0.0541	0.479	0.497	0.489	0.489	0.487	0.487	0.483	0.339	0.378	0.417	0.426	0.436	0.456	0.434
35.0	38.8	62.1	10.2	-1.6	-0.0354	0.489	0.500	0.494	0.485	0.479	0.481	0.467	0.339	0.379	0.417	0.437	0.446	0.456	0.437
36.0	39.0	62.4	10.2	9	0.0175	0.489	0.489	0.489	0.483	0.479	0.481	0.464	0.370	0.370	0.427	0.427	0.446	0.466	0.446
37.0	39.0	62.4	10.2	0.0	0.0000	0.485	0.483	0.482	0.478	0.474	0.474	0.472	0.339	0.378	0.416	0.436	0.445	0.474	0.455
38.0	39.0	62.4	10.2	9	0.0175	0.485	0.472	0.475	0.475	0.477	0.475	0.472	0.339	0.370	0.427	0.427	0.447	0.475	0.459
39.0	38.8	62.1	10.2	0.0	0.0000	0.485	0.465	0.469	0.470	0.476	0.474	0.472	0.332	0.363	0.420	0.440	0.449	0.497	0.459
40.0	38.8	62.1	10.2	0.0	0.0000	0.485	0.467	0.458	0.458	0.467	0.463	0.456	0.330	0.381	0.438	0.438	0.450	0.496	0.456
41.0	38.6	61.8	10.2	9	0.0176	0.489	0.464	0.458	0.444	0.452	0.452	0.456	0.410	0.390	0.448	0.448	0.458	0.487	0.468
42.0	38.5	61.5	10.2	9	0.0178	0.489	0.468	0.462	0.453	0.451	0.459	0.459	0.406	0.406	0.445	0.445	0.455	0.484	0.445
43.0	38.5	61.5	10.2	0.0	0.0000	0.491	0.467	0.461	0.443	0.443	0.455	0.465	0.404	0.395	0.443	0.443	0.457	0.482	0.443
44.0	38.3	61.2	10.2	9	0.0179	0.491	0.467	0.471	0.467	0.447	0.453	0.465	0.402	0.402	0.441	0.441	0.451	0.480	0.441
45.0	38.3	61.2	10.2	0.0	0.0000	0.491	0.467	0.459	0.465	0.449	0.447	0.453	0.412	0.402	0.451	0.451	0.461	0.490	0.451
46.0	38.2	61.0	10.2	9	0.0180	0.491	0.475	0.471	0.463	0.457	0.453	0.453	0.409	0.408	0.447	0.428	0.438	0.487	0.447
47.0	38.0	60.7	10.2	9	0.0182	0.491	0.475	0.473	0.469	0.465	0.459	0.449	0.408	0.400	0.439	0.420	0.439	0.475	0.439
48.0	38.0	60.7	10.2	0.0	0.0000	0.491	0.475	0.471	0.469	0.467	0.467	0.467	0.411	0.404	0.437	0.437	0.443	0.473	0.437
49.0	38.0	60.7	10.2	0.0	0.0000	0.491	0.472	0.468	0.466	0.468	0.464	0.466	0.411	0.406	0.436	0.436	0.443	0.473	0.436
50.0	37.8	60.4	10.2	9	0.0183	0.491	0.476	0.472	0.470	0.476	0.462	0.470	0.412	0.402	0.432	0.432	0.442	0.472	0.432



Table 19B — Inferred Pressurant Distribution, Sealing Run 247; South 3.279-cm Nozzle

i (°C)	T (°C)	T <sub>0</sub> (°C)	T <sub>1</sub> (°C)	B	B/θ	X	Pressurant Fractions (X) at Locations /												
							1	2	3	4	5	6	7	8	9	10	11	12	13
COMMERCE VALVE OPENING																			
0.0	18.5	19.9	20.3	106.2	0.0000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
1.0	20.1	20.6	20.4	106.2	1.2449	0.012	0.213	0.139	0.070	0.166	0.165	0.225	0.225	0.134	0.014	0.134	0.074	0.134	
VALVE FULLY OPEN																			
2.0	23.3	23.2	25.2	33.7	1.4809	0.034	1.308	0.962	0.764	0.271	0.715	1.011	0.965	0.618	0.618	0.865	0.124	0.618	
3.0	27.0	27.7	20.3	4.4	1.564	0.087	1.220	1.066	0.139	0.099	0.180	0.933	0.841	0.372	0.372	0.237	0.036	0.372	
4.0	29.6	31.1	18.5	1.4	0.473	0.118	0.622	0.31	0.07	0.15	0.055	0.055	0.070	0.292	0.292	0.253	0.174	0.253	
5.0	31.4	33.9	16.6	4.3	0.395	0.146	0.539	0.53	0.30	0.42	0.030	0.030	0.030	0.332	0.332	0.290	0.232	0.332	
6.0	33.2	36.7	16.3	2.0	0.613	0.172	0.51	0.56	0.121	0.102	0.058	0.058	0.082	0.258	0.258	0.234	0.185	0.258	
7.0	34.5	39.1	15.2	3.7	0.445	0.195	0.484	0.56	0.192	0.151	0.096	0.096	0.171	0.217	0.217	0.217	0.196	0.217	
8.0	35.4	40.7	15.3	1.9	0.334	0.209	0.451	0.51	0.167	0.167	0.151	0.167	0.167	0.226	0.226	0.226	0.206	0.226	
9.0	36.8	43.2	14.9	6.1	0.156	0.221	0.400	0.294	0.190	0.194	0.181	0.181	0.222	0.240	0.240	0.240	0.222	0.240	
10.0	37.2	44.8	14.0	6.1	0.1587	0.240	0.352	0.255	0.265	0.268	0.265	0.272	0.272	0.272	0.272	0.272	0.272	0.272	
11.0	37.5	46.2	13.7	5.7	0.1395	0.260	0.304	0.287	0.288	0.276	0.257	0.253	0.268	0.223	0.223	0.223	0.223	0.223	
12.0	37.9	47.2	13.7	6.2	0.1386	0.282	0.319	0.316	0.274	0.274	0.269	0.269	0.269	0.248	0.248	0.248	0.248	0.248	
13.0	38.9	49.4	13.0	1.7	0.142	0.296	0.363	0.374	0.332	0.325	0.325	0.325	0.325	0.304	0.304	0.304	0.304	0.304	
14.0	39.7	51.2	14.0	1.0	0.184	0.309	0.355	0.355	0.347	0.347	0.347	0.347	0.347	0.325	0.325	0.325	0.325	0.325	
15.0	40.3	52.7	14.1	2.3	0.421	0.322	0.309	0.327	0.324	0.363	0.371	0.371	0.371	0.351	0.351	0.351	0.351	0.351	
16.0	39.7	52.7	14.1	9.2	0.1555	0.336	0.393	0.406	0.390	0.372	0.380	0.357	0.357	0.336	0.336	0.336	0.336	0.336	
17.0	40.0	53.5	14.2	2.3	0.251	0.343	0.414	0.407	0.397	0.381	0.341	0.315	0.315	0.244	0.244	0.244	0.244	0.244	
18.0	40.7	55.1	14.3	4.4	0.065	0.353	0.409	0.406	0.424	0.375	0.343	0.348	0.348	0.225	0.225	0.225	0.225	0.225	
19.0	41.1	56.3	14.4	2.4	0.377	0.363	0.445	0.426	0.412	0.414	0.424	0.426	0.426	0.399	0.399	0.399	0.399	0.399	
20.0	40.5	56.2	14.4	8.5	0.1555	0.375	0.415	0.410	0.386	0.408	0.422	0.422	0.422	0.408	0.408	0.408	0.408	0.408	
21.0	39.5	55.3	14.4	11.7	0.137	0.386	0.393	0.408	0.410	0.415	0.425	0.425	0.425	0.403	0.403	0.403	0.403	0.403	
22.0	39.6	55.9	14.4	5.0	0.732	0.395	0.422	0.430	0.420	0.422	0.417	0.422	0.422	0.405	0.405	0.405	0.405	0.405	
23.0	39.0	55.7	14.4	9.7	0.1529	0.404	0.464	0.485	0.450	0.466	0.466	0.466	0.466	0.444	0.444	0.444	0.444	0.444	
24.0	39.4	56.6	14.5	1.6	0.126	0.409	0.449	0.439	0.446	0.442	0.449	0.449	0.449	0.427	0.427	0.427	0.427	0.427	
25.0	39.3	57.0	14.5	6.1	0.0832	0.417	0.487	0.477	0.470	0.465	0.482	0.482	0.482	0.460	0.460	0.460	0.460	0.460	
26.0	39.8	58.3	14.6	1.4	0.146	0.423	0.499	0.506	0.508	0.480	0.480	0.501	0.501	0.481	0.481	0.481	0.481	0.481	
27.0	39.8	58.7	14.7	5.4	0.676	0.430	0.492	0.497	0.488	0.497	0.492	0.492	0.492	0.479	0.479	0.479	0.479	0.479	
COMMERCE VALVE CLOSED																			
28.0	39.9	59.5	14.7	2.5	0.280	0.436	0.470	0.472	0.468	0.484	0.481	0.497	0.497	0.480	0.480	0.480	0.480	0.480	
29.0	40.1	60.0	14.7	1.6	0.189	0.441	0.474	0.463	0.466	0.479	0.465	0.465	0.465	0.463	0.463	0.463	0.463	0.463	
VALVE FULLY CLOSED																			
30.0	39.2	59.2	14.6	13.5	0.1587	0.448	0.478	0.478	0.472	0.468	0.467	0.476	0.476	0.462	0.462	0.462	0.462	0.462	
31.0	41.6	63.3	14.8	3.9	0.1818	0.448	0.472	0.467	0.457	0.474	0.474	0.474	0.474	0.462	0.462	0.462	0.462	0.462	
32.0	42.9	65.5	15.0	1.7	0.1382	0.448	0.461	0.457	0.462	0.479	0.479	0.479	0.479	0.467	0.467	0.467	0.467	0.467	
33.0	43.5	66.6	15.1	5.6	0.0664	0.448	0.464	0.462	0.458	0.478	0.478	0.478	0.478	0.466	0.466	0.466	0.466	0.466	
34.0	43.9	67.1	15.2	2.8	0.326	0.448	0.471	0.467	0.459	0.469	0.469	0.469	0.469	0.466	0.466	0.466	0.466	0.466	
35.0	44.0	67.4	15.2	1.4	0.161	0.448	0.474	0.470	0.464	0.470	0.474	0.474	0.474	0.470	0.470	0.470	0.470	0.470	
36.0	44.2	67.7	15.2	1.4	0.160	0.448	0.475	0.469	0.463	0.469	0.469	0.469	0.469	0.467	0.467	0.467	0.467	0.467	
37.0	44.2	67.7	15.2	0.0	0.0000	0.448	0.476	0.474	0.462	0.462	0.468	0.468	0.468	0.466	0.466	0.466	0.466	0.466	
38.0	44.0	67.4	15.2	1.4	0.160	0.448	0.465	0.461	0.456	0.459	0.469	0.469	0.469	0.467	0.467	0.467	0.467	0.467	
39.0	43.9	67.1	15.2	1.4	0.161	0.448	0.472	0.462	0.454	0.458	0.468	0.468	0.468	0.466	0.466	0.466	0.466	0.466	
40.0	43.9	67.1	15.2	0.0	0.0000	0.448	0.464	0.462	0.456	0.458	0.462	0.462	0.462	0.460	0.460	0.460	0.460	0.460	
41.0	43.7	66.9	15.1	1.4	0.162	0.448	0.466	0.459	0.453	0.455	0.460	0.460	0.460	0.458	0.458	0.458	0.458	0.458	
42.0	43.5	66.6	15.1	1.4	0.163	0.448	0.453	0.453	0.443	0.445	0.453	0.453	0.453	0.450	0.450	0.450	0.450	0.450	
43.0	43.5	66.6	15.1	0.0	0.0000	0.448	0.448	0.446	0.436	0.438	0.443	0.443	0.443	0.440	0.440	0.440	0.440	0.440	
44.0	43.4	66.3	15.1	1.4	0.164	0.448	0.450	0.441	0.433	0.435	0.442	0.442	0.442	0.440	0.440	0.440	0.440	0.440	
45.0	43.2	66.0	15.1	1.4	0.165	0.448	0.445	0.437	0.430	0.431	0.439	0.439	0.439	0.437	0.437	0.437	0.437	0.437	
46.0	43.2	66.0	15.1	0.0	0.0000	0.448	0.446	0.436	0.432	0.440	0.442	0.442	0.442	0.440	0.440	0.440	0.440	0.440	
47.0	43.0	65.8	15.1	1.4	0.167	0.448	0.447	0.439	0.435	0.445	0.445	0.445	0.445	0.443	0.443	0.443	0.443	0.443	
48.0	43.0	65.8	15.1	0.0	0.0000	0.448	0.445	0.443	0.443	0.449	0.449	0.449	0.449	0.447	0.447	0.447	0.447	0.447	
49.0	42.9	65.3	15.0	1.4	0.168	0.448	0.449	0.443	0.449	0.443	0.449	0.449	0.449	0.447	0.447	0.447	0.447	0.447	
50.0	42.9	65.3	15.0	0.0	0.0000	0.448	0.454	0.450	0.450	0.454	0.454	0.454	0.454	0.451	0.451	0.451	0.451	0.451	

Table 20B -- Inferred Pressurant Distribution, Scaling Run 248; South 3.279-cm Nozzle

[illegible]

**C-Tables**

Each of the four sets of experiments has a C-table. These tables give mean values for replicate runs in each set. Otherwise, they are similar to the B-tables, with two exceptions: Dimensionless time  $\tau$  is added in the last column of the table, and all values in the table have been extrapolated to correspond to equal  $\tau$ -increments of 0.05 (see Appendix C for program).

MEAN VALUES OF ALL QUANTITIES

I	T <sub>1</sub> (°C)	T <sub>2</sub> (°C)	T <sub>3</sub> (°C)	B/θ	B	MEAN PRESSURANT FRACTIONS AT LOCATIONS I										TAU					
						1	2	3	4	5	6	7	8	9	10		11	12	13		
0.0	12.5	12.5	27.4	0.0000	1.6	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
0.4	14.6	14.5	19.1	0.2499	5.5	-1.04	-0.53	-0.22	-0.08	-0.57	-0.55	1.14	0.54	0.46	0.89	0.45	1.04	0.85	0.05	0.05	
0.8	16.2	19.4	9.0	0.4992	9.2	-1.96	-0.98	-0.42	0.11	-1.06	-1.02	2.39	1.23	0.91	1.72	0.93	2.01	1.64	1.10	1.10	
1.1	18.2	19.4	5.0	0.5921	9.0	-1.46	-0.61	-0.34	0.01	-0.70	-	2.93	1.22	1.15	1.88	1.08	2.08	1.73	1.15	1.15	
1.4	19.7	21.5	3.3	0.5315	7.6	-	-	-	0.12	-0.63	-0.38	-0.17	2.27	1.42	1.34	1.90	1.21	1.94	1.68	2.0	
1.6	21.1	23.7	2.4	0.4725	5.9	0.10	0.38	0.73	0.65	0.36	0.67	2.09	1.61	1.53	1.93	1.34	1.80	1.64	2.5	2.5	
1.9	22.4	25.8	1.7	0.4163	4.6	0.74	0.81	0.87	0.93	0.84	1.23	1.98	1.82	1.71	1.99	1.50	1.72	1.64	3.0	3.0	
2.2	23.7	28.0	1.3	0.3621	4.0	1.06	1.09	1.09	1.20	1.16	1.59	2.12	2.03	1.92	2.14	1.73	1.85	1.79	3.5	3.5	
2.5	25.0	30.3	1.3	0.2945	3.4	1.37	1.35	1.30	1.40	1.45	1.82	2.29	2.23	2.14	2.30	1.97	2.03	1.97	4.0	4.0	
2.8	26.0	32.4	1.5	0.2706	3.5	1.67	1.64	1.55	1.75	1.74	2.09	2.45	2.42	2.35	2.44	2.20	2.22	2.16	4.5	4.5	
3.1	27.0	34.5	1.6	0.2482	3.8	1.98	1.96	1.83	2.00	2.02	2.33	2.56	2.56	2.53	2.59	2.41	2.46	2.41	5.0	5.0	
3.3	27.9	36.7	1.6	0.2048	4.0	2.30	2.26	2.12	2.26	2.30	2.57	2.68	2.70	2.70	2.75	2.61	2.70	2.65	5.5	5.5	
3.6	28.7	39.0	1.6	0.1740	3.7	2.60	2.57	2.43	2.54	2.61	2.86	2.91	2.84	2.85	2.93	2.83	2.90	2.79	6.0	6.0	
3.9	29.6	41.4	1.5	0.1594	3.4	2.93	2.87	2.74	2.85	2.93	3.16	3.21	3.02	3.02	3.08	3.03	3.07	2.93	6.5	6.5	
4.2	30.1	43.5	1.4	0.1592	3.7	3.19	3.14	3.02	3.15	3.24	3.44	3.49	3.23	3.24	3.23	3.19	3.21	3.12	7.0	7.0	
4.5	30.5	45.6	1.4	0.1294	4.1	3.43	3.39	3.26	3.40	3.49	3.70	3.72	3.43	3.43	3.43	3.42	3.43	3.31	7.5	7.5	
4.8	30.7	47.6	1.4	0.1059	4.1	3.72	3.66	3.47	3.62	3.72	3.93	3.94	3.62	3.64	3.67	3.65	3.66	3.51	8.0	8.0	
5.1	30.8	49.4	1.6	0.0843	4.3	4.00	3.92	3.70	3.82	3.93	4.14	4.15	3.87	3.92	3.91	3.92	3.84	3.66	8.5	8.5	
5.4	30.9	51.3	1.6	0.0642	4.0	4.18	4.14	4.00	4.09	4.19	4.40	4.39	4.13	4.17	4.09	4.08	4.11	4.08	3.91	9.0	9.0
5.7	30.7	53.0	1.5	0.0478	3.6	4.43	4.38	4.19	4.29	4.42	4.63	4.21	4.37	4.36	4.27	4.32	4.29	4.13	9.5	9.5	
6.0	29.6	54.6	-1.1	0.0377	4.56	4.74	4.62	4.43	4.55	4.69	4.87	4.45	4.54	4.56	4.51	4.46	4.49	4.37	1.00	1.00	
6.3	30.7	56.7	-4.1	-1.0980	4.56	4.76	4.68	4.50	4.61	4.74	4.93	4.44	4.48	4.48	4.44	4.43	4.43	4.36	1.05	1.05	
6.6	30.4	56.2	-3.1	0.0331	4.56	4.77	4.72	4.56	4.64	4.79	4.93	4.41	4.48	4.47	4.40	4.42	4.38	4.32	1.10	1.10	
6.9	30.1	55.5	-2.2	0.0341	4.56	4.78	4.70	4.57	4.65	4.81	4.96	4.45	4.46	4.46	4.41	4.38	4.35	4.32	1.15	1.15	
7.2	29.8	55.0	-1.1	0.0342	4.56	4.83	4.75	4.59	4.70	4.82	4.95	4.42	4.46	4.41	4.35	4.37	4.31	4.33	1.20	1.20	
7.5	29.6	54.4	-1.1	0.0321	4.56	4.84	4.77	4.61	4.69	4.81	4.96	4.41	4.43	4.42	4.34	4.36	4.33	4.33	1.25	1.25	
7.8	29.3	53.9	0.0	0.0296	4.56	4.84	4.75	4.61	4.69	4.78	4.94	4.38	4.42	4.42	4.38	4.36	4.37	4.37	1.30	1.30	
8.1	29.1	53.4	1.1	0.0266	4.56	4.84	4.74	4.58	4.68	4.78	4.93	4.37	4.43	4.42	4.36	4.39	4.37	4.42	1.35	1.35	
8.4	28.9	53.0	2.2	0.0236	4.56	4.84	4.75	4.57	4.67	4.79	4.95	4.41	4.45	4.45	4.38	4.33	4.38	4.40	1.40	1.40	
8.7	28.7	52.6	2.2	0.0235	4.56	4.83	4.74	4.57	4.67	4.76	4.93	4.41	4.45	4.45	4.36	4.36	4.35	4.37	1.45	1.45	
9.0	28.5	52.3	3.3	0.0199	4.56	4.83	4.71	4.55	4.65	4.74	4.94	4.43	4.47	4.47	4.45	4.36	4.41	4.40	1.50	1.50	
9.3	28.3	51.9	3.3	0.0234	4.56	4.79	4.69	4.55	4.64	4.74	4.92	4.41	4.49	4.49	4.46	4.37	4.41	4.42	1.55	1.55	
9.6	28.2	51.6	3.3	0.0183	4.56	4.78	4.68	4.53	4.63	4.73	4.93	4.44	4.47	4.47	4.40	4.39	4.42	4.37	1.60	1.60	
9.9	28.1	51.3	4.1	0.0189	4.56	4.78	4.69	4.53	4.66	4.76	4.93	4.44	4.49	4.49	4.47	4.37	4.38	4.41	1.65	1.65	
10.2	27.9	50.9	5.1	0.0221	4.56	4.79	4.70	4.55	4.65	4.79	4.93	4.44	4.48	4.48	4.46	4.37	4.36	4.42	1.70	1.70	
10.5	27.8	50.4	6.8	0.0116	4.56	4.81	4.70	4.55	4.67	4.82	5.00	4.43	4.46	4.40	4.33	4.38	4.40	4.35	1.75	1.75	
10.8	27.6	47.9	1.0	0.0159	3.94	4.10	4.03	3.94	4.02	4.12	4.26	3.84	3.82	3.82	3.78	3.82	3.82	3.80	1.80	1.80	
11.1	23.6	42.9	1.3	0.0132	3.94	4.11	4.05	3.95	4.03	4.12	4.26	3.84	3.82	3.81	3.77	3.79	3.84	3.81	1.85	1.85	
11.4	21.3	42.3	1.6	1.0081	1.97	2.05	2.04	1.99	2.05	2.09	2.14	1.90	1.89	1.89	1.86	1.89	1.92	1.89	1.90	1.90	
11.7	0.0	0.0	0.0	0.0000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.95	1.95	
12.0	0.0	0.0	0.0	0.0000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.00	2.00	
12.3	0.0	0.0	0.0	0.0000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.05	2.05	
12.6	0.0	0.0	0.0	0.0000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.10	2.10	
12.9	0.0	0.0	0.0	0.0000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.15	2.15	
13.2	0.0	0.0	0.0	0.0000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.20	2.20	
13.5	0.0	0.0	0.0	0.0000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.25	2.25	
13.8	0.0	0.0	0.0	0.0000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.30	2.30	
14.1	0.0	0.0	0.0	0.0000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.35	2.35	
14.4	0.0	0.0	0.0	0.0000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.40	2.40	
14.7	0.0	0.0	0.0	0.0000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.45	2.45	

Set 2, Table C – Mean Values of All Quantities, Scaling Runs 237-240

MEAN VALUES OF ALL QUANTITIES																							
$\omega$	$\bar{T}$ (°C)	$\bar{T}$ (°C)	$\bar{T}$ (°C)	$\beta$	$\frac{\Delta \rho}{\rho}$	$\bar{X}$	1	2	3	4	5	6	7	MEAN PRESSURANT FRACTIONS AT LOCATIONS 1						11	12	13	TAU
0.0	17.7	17.7	30.6	0.0	0.0000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
1.0	17.7	19.6	27.8	65.7	1.9414	0.23	334	242	-006	119	252	380	-139	-090	-202	-196	-109	-182	-140	05			
1.6	22.1	22.0	24.2	40.1	1.0014	0.05	-727	-766	-738	-863	-1	007	814	640	927	725	536	969	796	10			
2.3	24.2	24.5	22.2	3.9	1.0489	0.08	-1	039	-907	-838	-765	1	027	1	052	926	700	1	250	1			
2.9	26.2	26.5	18.9	3.9	1.0480	0.00	-580	-318	-474	-474	-374	-604	844	814	442	391	427	785	613	20			
3.7	27.9	29.4	16.7	1.6	0.5229	1.13	-334	-324	-201	-289	-339	-359	666	481	344	513	336	597	456	25			
4.5	29.5	31.8	15.1	2.1	0.671	1.35	017	025	029	021	011	014	285	244	201	213	192	317	219	30			
5.3	31.1	34.2	14.3	1.5	0.495	1.58	108	089	022	091	074	063	201	209	224	317	199	221	206	35			
6.3	34.6	36.6	13.6	1.2	0.2594	1.80	178	153	132	156	143	126	191	192	201	196	180	263	225	40			
7.4	32.0	39.3	13.3	1.0	0.492	2.03	211	201	156	195	192	180	192	198	198	203	184	231	231	45			
8.5	35.0	41.4	13.0	3.5	0.935	2.26	236	233	223	211	212	213	196	219	224	223	214	223	244	55			
9.9	35.6	43.1	12.9	5.5	1.137	2.80	238	257	247	245	250	251	204	228	243	41	235	300	268	55			
11.2	36.4	45.2	12.8	3.1	0.730	2.71	232	280	275	278	279	287	208	237	270	259	257	319	290	60			
12.7	36.0	46.8	12.9	5.0	0.137	2.53	314	303	239	308	318	328	203	257	284	284	274	334	310	65			
14.3	37.4	48.6	12.8	4.0	0.767	3.16	335	345	339	344	342	321	236	262	304	305	301	341	323	70			
16.2	37.6	50.2	12.9	4.4	0.814	3.38	335	363	358	346	345	343	256	274	333	344	325	383	352	75			
18.3	37.7	51.7	12.8	5.4	0.084	3.61	335	350	381	371	381	370	265	292	337	349	346	410	381	80			
20.6	37.4	52.7	12.8	6.9	1.112	3.83	405	411	407	414	418	413	280	319	365	369	363	418	401	85			
23.4	37.5	54.5	12.7	5.6	0.846	4.06	435	431	421	419	409	403	306	358	408	405	409	443	427	90			
26.6	37.2	55.6	12.6	7.5	0.966	4.28	451	447	440	442	443	449	336	360	430	424	424	473	453	95			
30.3	36.3	56.5	11.7	2.2	0.462	4.51	454	486	474	482	486	486	374	376	443	432	427	458	444	1			
34.3	39.5	62.8	12.0	-1.4	-0.306	4.51	453	475	466	461	465	470	382	402	450	445	443	471	450	1.05			
38.4	39.5	62.9	12.0	3	0.081	4.51	462	458	458	463	465	473	393	404	457	452	449	458	460	1.10			
42.5	39.5	61.0	12.2	5	0.114	4.51	463	460	455	461	463	472	411	411	449	453	453	473	450	1.15			
46.5	39.1	60.5	13.1	5	0.126	4.51	463	460	455	461	463	472	411	411	449	453	453	473	450	1.20			
50.6	38.6	59.5	13.7	40.3	0.067	4.51	466	464	460	465	461	466	410	422	439	433	445	478	444	1.25			
54.7	38.5	58.6	14.1	5	0.106	4.51	467	464	461	469	462	464	410	423	436	439	441	467	436	1.30			
58.7	38.3	57.9	14.4	2	0.049	4.51	469	464	461	461	457	463	414	439	438	442	438	463	437	1.35			
62.7	38.1	57.3	14.6	5	0.060	4.51	466	463	464	464	464	467	417	425	434	440	444	464	436	1.40			
66.8	37.8	56.7	14.9	5	0.103	4.51	467	464	462	468	467	473	413	418	434	436	444	477	439	1.45			
70.9	37.7	56.3	15.0	3	0.065	4.51	467	464	460	466	464	472	420	436	425	436	446	465	439	1.50			
75.0	37.5	56.0	15.1	0	0.007	4.51	458	453	450	459	461	463	437	441	429	432	452	464	442	1.55			
79.0	37.3	55.5	15.1	6	0.112	4.51	453	458	452	461	453	459	433	439	428	445	450	453	439	1.60			
83.1	37.1	55.2	15.1	3	0.065	4.51	456	456	450	458	452	458	437	445	439	439	439	435	438	1.65			
87.2	37.0	54.9	15.1	2	0.045	4.51	453	453	453	458	455	457	445	450	439	440	444	447	431	1.70			
91.2	36.8	54.6	15.1	5	0.094	4.51	454	454	448	459	453	459	441	447	447	447	447	447	429	1.75			
95.3	36.6	54.6	15.1	3	0.061	4.51	454	454	454	459	459	459	441	447	447	447	447	447	429	1.80			
99.4	36.4	54.4	15.1	3	0.061	4.51	454	454	454	459	459	459	441	447	447	447	447	447	429	1.85			
103.5	36.2	54.2	15.1	3	0.061	4.51	454	454	454	459	459	459	441	447	447	447	447	447	429	1.90			
107.6	36.0	54.0	15.1	3	0.061	4.51	454	454	454	459	459	459	441	447	447	447	447	447	429	1.95			
111.7	35.8	53.8	15.1	3	0.061	4.51	454	454	454	459	459	459	441	447	447	447	447	447	429	2.00			
115.8	35.6	53.6	15.1	3	0.061	4.51	454	454	454	459	459	459	441	447	447	447	447	447	429	2.05			
119.9	35.4	53.4	15.1	3	0.061	4.51	454	454	454	459	459	459	441	447	447	447	447	447	429	2.10			
124.0	35.2	53.2	15.1	3	0.061	4.51	454	454	454	459	459	459	441	447	447	447	447	447	429	2.15			
128.1	35.0	53.0	15.1	3	0.061	4.51	454	454	454	459	459	459	441	447	447	447	447	447	429	2.20			
132.2	34.8	52.8	15.1	3	0.061	4.51	454	454	454	459	459	459	441	447	447	447	447	447	429	2.25			
136.3	34.6	52.6	15.1	3	0.061	4.51	454	454	454	459	459	459	441	447	447	447	447	447	429	2.30			
140.4	34.4	52.4	15.1	3	0.061	4.51	454	454	454	459	459	459	441	447	447	447	447	447	429	2.35			
144.5	34.2	52.2	15.1	3	0.061	4.51	454	454	454	459	459	459	441	447	447	447	447	447	429	2.40			
148.6	34.0	52.0	15.1	3	0.061	4.51	454	454	454	459	459	459	441	447	447	447	447	447	429	2.45			
152.7	33.8	51.8	15.1	3	0.061	4.51	454	454	454	459	459	459	441	447	447	447	447	447	429	2.50			
156.8	33.6	51.6	15.1	3	0.061	4.51	454	454	454	459	459	459	441	447	447	447	447	447	429	2.55			
160.9	33.4	51.4	15.1	3	0.061	4.51	454	454	454	459	459	459	441	447	447	447	447	447	429	2.60			
165.0	33.2	51.2	15.1	3	0.061	4.51	454	454	454	459	459	459	441	447	447	447	447	447	429	2.65			
169.1	33.0	51.0	15.1	3	0.061	4.51	454	454	454	459	459	459	441	447	447	447	447	447	429	2.70			
173.2	32.8	50.8	15.1	3	0.061	4.51	454	454	454	459	459	459	441	447	447	447	447	447	429	2.75			
177.3	32.6	50.6	15.1	3	0.061	4.51	454	454	454	459	459	459	441	447	447	447	447	447	429	2.80			
181.4	32.4	50.4	15.1	3	0.061	4.51	454	454	454	459	459	459	441	447	447	447	447	447	429	2.85			
185.5	32.2	50.2	15.1	3	0.061	4.51	454	454	454	459	459	459	441	447	447	447	447	447	429	2.90			
189.6	32.0	50.0	15.1	3	0.061	4.51	454	454	454	459	459	459	441	447	447	447	447	447	429	2.95			
193.7	31.8	49.8	15.1	3	0.061	4.51	454	454	454	459	459	459	441	447	447	447	447	447	429	3.00			
197.8	31.6	49.6	15.1	3	0.061	4.51	454	454	454	459	459	459	441	447	447	447	447	447	429	3.05			
201.9	31.4	49.4	15.1	3	0.061	4.51	454	454	454	459	459	459	441	447	447	447	447	447	429	3.10			
206.0	31.2	49.2	15.1	3	0.061	4.51	454	454	454	459	459	459	441	447	447	447	447	447	429	3.15			
210.1	31.0	49.0	15.1	3	0.061	4.51	454	454	454	459	459	459	441	447	447	447	447	447	429	3.20			
214.2	30.8																						

Set 3, Table C — Mean Values of All Quantities, Scaling Runs 241-244

MEAN VALUES OF ALL QUANTITIES										MEAN PRESSURANT FRACTIONS AT LOCATIONS I													TAU		
$\bar{t}$ (a)	$\bar{t}$ (°C)	$\bar{t}$ (°C)	$\bar{t}$ (°C)	$\bar{t}$ (°C)	$\bar{t}$ (°C)	$\bar{t}$ (°C)	$\bar{t}$ (°C)	$\bar{t}$ (°C)	$\bar{t}$ (°C)	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16
0.0	5.9	5.9	35.8	2.1	0.0000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
5.9	7.2	7.2	17.1	27.2	1.3294	0.23	-1.18	-0.21	272	0.01	-0.75	-0.75	-0.75	-0.75	-0.75	-0.75	-0.75	-0.75	-0.75	-0.75	-0.75	-0.75	-0.75	-0.75	-0.75
17.1	8.4	8.4	17.1	48.9	2.5243	0.46	-2.17	-0.38	514	0.04	-1.36	-1.36	-1.36	-1.36	-1.36	-1.36	-1.36	-1.36	-1.36	-1.36	-1.36	-1.36	-1.36	-1.36	-1.36
48.9	9.6	9.6	11.0	43.6	2.4937	0.65	-1.84	-0.26	335	0.21	-1.08	-1.08	-1.08	-1.08	-1.08	-1.08	-1.08	-1.08	-1.08	-1.08	-1.08	-1.08	-1.08	-1.08	-1.08
11.0	10.7	10.7	12.8	35.0	2.3039	0.92	-1.36	-0.63	327	0.40	-0.70	-0.70	-0.70	-0.70	-0.70	-0.70	-0.70	-0.70	-0.70	-0.70	-0.70	-0.70	-0.70	-0.70	-0.70
12.8	11.9	11.9	14.6	23.7	1.8117	1.15	-0.89	-0.26	516	0.63	-0.31	-0.31	-0.31	-0.31	-0.31	-0.31	-0.31	-0.31	-0.31	-0.31	-0.31	-0.31	-0.31	-0.31	-0.31
14.6	13.0	13.0	16.4	13.7	1.3012	1.38	-0.49	-0.50	510	0.86	-0.07	-0.07	-0.07	-0.07	-0.07	-0.07	-0.07	-0.07	-0.07	-0.07	-0.07	-0.07	-0.07	-0.07	-0.07
16.4	13.9	13.9	18.1	11.1	1.0137	1.61	-0.26	-0.76	526	1.12	0.41	0.41	0.41	0.41	0.41	0.41	0.41	0.41	0.41	0.41	0.41	0.41	0.41	0.41	0.41
18.1	14.8	14.8	19.8	9.4	0.8071	1.84	0.00	-0.71	541	1.34	0.75	1.01	1.02	0.96	0.72	0.89	1.25	0.73	0.89	1.25	0.73	0.89	1.25	0.73	0.89
19.8	15.7	15.7	21.5	8.5	0.6850	2.07	0.30	-1.40	560	1.52	1.05	1.34	1.15	1.18	0.89	1.07	1.62	0.89	1.07	1.62	0.89	1.07	1.62	0.89	1.07
21.5	16.6	16.6	23.2	7.0	0.5899	2.30	0.66	-1.90	589	1.66	1.33	1.66	1.29	1.38	1.05	1.17	1.73	1.05	1.17	1.73	1.05	1.17	1.73	1.05	1.17
23.2	17.3	17.3	25.0	7.1	0.4947	2.53	0.99	-2.34	618	1.85	1.62	1.85	1.45	1.57	1.28	1.37	1.87	1.28	1.37	1.87	1.28	1.37	1.87	1.28	1.37
25.0	18.1	18.1	26.8	6.3	0.4047	2.76	1.31	-2.44	649	2.12	2.00	2.28	1.65	1.93	1.32	1.59	2.04	1.32	1.59	2.04	1.32	1.59	2.04	1.32	1.59
26.8	18.7	18.7	28.6	6.1	0.3588	2.99	1.61	-2.49	678	2.37	2.33	2.60	1.91	2.10	1.73	1.79	2.27	1.73	1.79	2.27	1.73	1.79	2.27	1.73	1.79
28.6	19.1	19.1	30.2	6.2	0.3438	3.22	1.91	-2.66	698	2.51	2.53	2.80	2.19	2.30	1.99	2.01	2.53	1.99	2.01	2.53	1.99	2.01	2.53	1.99	2.01
30.2	19.4	19.4	31.7	6.3	0.3225	3.45	2.22	-2.89	714	2.64	2.70	2.94	2.35	2.56	2.26	2.26	2.87	2.26	2.26	2.87	2.26	2.26	2.87	2.26	2.26
31.7	19.5	19.5	33.2	6.3	0.2894	3.68	2.53	-3.08	732	2.84	2.83	3.08	2.80	2.89	2.60	2.53	3.26	2.60	2.53	3.26	2.60	2.53	3.26	2.60	2.53
33.2	19.8	19.8	34.9	5.4	0.2226	3.91	2.87	-3.48	742	3.05	3.19	3.62	3.08	3.07	2.84	2.74	3.40	2.84	2.74	3.40	2.84	2.74	3.40	2.84	2.74
34.9	19.7	19.7	36.2	5.7	0.2039	4.14	3.14	-3.67	761	3.35	3.56	3.91	3.22	3.41	3.12	3.14	3.63	3.12	3.14	3.63	3.12	3.14	3.63	3.12	3.14
36.2	19.6	19.6	37.7	5.7	0.1886	4.37	3.51	-3.81	767	3.61	3.86	4.08	3.34	3.66	3.38	3.36	3.97	3.38	3.36	3.97	3.38	3.36	3.97	3.38	3.36
37.7	19.4	19.4	41.0	5.7	0.0881	4.60	3.81	-4.48	781	4.14	4.32	4.42	4.22	4.22	4.07	4.07	4.32	4.07	4.07	4.32	4.07	4.07	4.32	4.07	4.07
41.0	19.5	19.5	42.1	5.7	0.0364	4.80	4.28	-4.50	785	4.56	4.66	4.66	4.46	4.46	4.29	4.29	4.56	4.29	4.29	4.56	4.29	4.29	4.56	4.29	4.29
42.1	19.5	19.5	43.3	5.7	0.0303	4.90	4.48	-4.55	785	4.80	4.80	4.80	4.60	4.60	4.46	4.46	4.80	4.46	4.46	4.80	4.46	4.46	4.80	4.46	4.46
43.3	19.2	19.2	44.6	5.7	0.0286	4.90	4.55	-4.59	785	4.90	4.90	4.90	4.70	4.70	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55
44.6	18.9	18.9	46.0	5.5	0.0330	4.90	4.90	-4.60	785	4.90	4.90	4.90	4.70	4.70	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55
46.0	18.7	18.7	49.4	5.5	0.0317	4.90	4.90	-4.60	785	4.90	4.90	4.90	4.70	4.70	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55
49.4	18.5	18.5	48.9	5.7	0.0203	4.90	5.00	-4.59	785	4.90	4.90	4.90	4.70	4.70	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55
48.9	18.2	18.2	48.9	5.6	0.0246	4.90	4.98	-4.56	785	4.90	4.90	4.90	4.70	4.70	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55
48.9	18.1	18.1	48.9	5.6	0.0200	4.90	5.01	-4.60	785	4.90	4.90	4.90	4.70	4.70	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55
48.9	17.9	17.9	48.9	5.4	0.0319	4.90	5.02	-4.61	785	4.90	4.90	4.90	4.70	4.70	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55
48.9	17.7	17.7	48.9	5.3	0.0125	4.90	5.02	-4.60	785	4.90	4.90	4.90	4.70	4.70	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55
48.9	17.6	17.6	48.9	5.3	0.0200	4.90	5.03	-4.59	785	4.90	4.90	4.90	4.70	4.70	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55
48.9	17.4	17.4	48.9	5.2	0.0280	4.90	5.03	-4.60	785	4.90	4.90	4.90	4.70	4.70	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55
48.9	17.3	17.3	48.9	5.2	0.0062	4.90	5.03	-4.60	785	4.90	4.90	4.90	4.70	4.70	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55
48.9	16.5	16.5	48.9	5.2	0.0167	4.90	5.03	-4.60	785	4.90	4.90	4.90	4.70	4.70	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55
48.9	16.4	16.4	48.9	5.2	0.0067	4.90	5.03	-4.60	785	4.90	4.90	4.90	4.70	4.70	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55
48.9	16.3	16.3	48.9	5.2	0.0067	4.90	5.03	-4.60	785	4.90	4.90	4.90	4.70	4.70	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55
48.9	16.2	16.2	48.9	5.2	0.0067	4.90	5.03	-4.60	785	4.90	4.90	4.90	4.70	4.70	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55
48.9	16.1	16.1	48.9	5.2	0.0067	4.90	5.03	-4.60	785	4.90	4.90	4.90	4.70	4.70	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55
48.9	16.0	16.0	48.9	5.2	0.0067	4.90	5.03	-4.60	785	4.90	4.90	4.90	4.70	4.70	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55
48.9	15.9	15.9	48.9	5.2	0.0067	4.90	5.03	-4.60	785	4.90	4.90	4.90	4.70	4.70	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55
48.9	15.8	15.8	48.9	5.2	0.0067	4.90	5.03	-4.60	785	4.90	4.90	4.90	4.70	4.70	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55
48.9	15.7	15.7	48.9	5.2	0.0067	4.90	5.03	-4.60	785	4.90	4.90	4.90	4.70	4.70	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55
48.9	15.6	15.6	48.9	5.2	0.0067	4.90	5.03	-4.60	785	4.90	4.90	4.90	4.70	4.70	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55
48.9	15.5	15.5	48.9	5.2	0.0067	4.90	5.03	-4.60	785	4.90	4.90	4.90	4.70	4.70	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55
48.9	15.4	15.4	48.9	5.2	0.0067	4.90	5.03	-4.60	785	4.90	4.90	4.90	4.70	4.70	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55
48.9	15.3	15.3	48.9	5.2	0.0067	4.90	5.03	-4.60	785	4.90	4.90	4.90	4.70	4.70	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55
48.9	15.2	15.2	48.9	5.2	0.0067	4.90	5.03	-4.60	785	4.90	4.90	4.90	4.70	4.70	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55	4.90	4.55	4.55
48.9	15.1	15.1	48.9	5.2	0.0067	4.90	5.03	-4.60	785	4.90	4.90	4.90	4.70	4.70	4.55	4.55	4.90	4.55							

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**D-Tables**

The D-tables give the standard-deviation history of each local mean pressurant mole fraction, according to experimental set, for values of dimensionless time  $\tau$  from 0.00 to 2.45 (see Appendix C for program). Each experimental set is treated in a separate D-table.



STONE, ALEXANDER, STREET, ST. AUBIN, AND WILLIAMS

Set 1, Table D — Standard Deviation of Mean Local Pressurant Fractions, Scaling Runs 230-236

LOCATIONS 1														TAU
1	2	3	4	5	6	7	8	9	10	11	12	13	14	
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.00
.271	.160	.051	.099	.157	.142	.203	.085	.100	.133	.096	.172	.138	.05	.05
.505	.297	.096	.104	.290	.264	.384	.158	.193	.245	.181	.318	.253	.10	.10
.380	.228	.088	.155	.219	.195	.294	.118	.169	.197	.147	.246	.197	.15	.15
.270	.172	.078	.125	.164	.142	.213	.078	.132	.158	.116	.186	.154	.20	.20
.162	.120	.076	.096	.114	.097	.143	.056	.100	.121	.094	.129	.115	.25	.25
.092	.084	.075	.072	.081	.069	.107	.064	.078	.095	.084	.084	.091	.30	.30
.084	.077	.057	.058	.075	.061	.100	.060	.072	.084	.067	.069	.081	.35	.35
.072	.071	.040	.047	.065	.053	.094	.061	.064	.075	.051	.059	.072	.40	.40
.063	.069	.032	.042	.057	.049	.089	.058	.059	.072	.040	.053	.064	.45	.45
.054	.061	.024	.039	.055	.056	.085	.049	.053	.071	.035	.048	.063	.50	.50
.052	.051	.020	.037	.055	.058	.079	.041	.050	.065	.032	.050	.067	.55	.55
.050	.039	.013	.027	.046	.050	.063	.032	.038	.064	.039	.056	.056	.60	.60
.043	.028	.014	.021	.038	.044	.060	.036	.032	.062	.047	.063	.042	.65	.65
.038	.025	.013	.019	.035	.042	.069	.033	.031	.052	.040	.059	.032	.70	.70
.035	.016	.012	.014	.030	.035	.062	.024	.032	.047	.028	.054	.040	.75	.75
.032	.014	.011	.013	.031	.028	.057	.025	.039	.044	.025	.049	.041	.80	.80
.036	.014	.013	.013	.029	.025	.056	.033	.044	.045	.028	.046	.033	.85	.85
.026	.026	.018	.021	.027	.038	.057	.031	.044	.037	.033	.066	.030	.90	.90
.032	.025	.017	.021	.029	.027	.054	.030	.031	.052	.029	.051	.040	.95	.95
.023	.021	.024	.021	.024	.022	.043	.028	.035	.046	.031	.044	.043	1.00	1.00
.028	.016	.014	.013	.019	.017	.049	.029	.034	.044	.021	.043	.048	1.05	1.05
.036	.028	.016	.018	.017	.024	.043	.028	.030	.050	.028	.045	.050	1.10	1.10
.033	.029	.015	.013	.016	.028	.051	.031	.030	.043	.032	.052	.048	1.15	1.15
.026	.020	.014	.011	.021	.031	.055	.035	.032	.040	.031	.043	.052	1.20	1.20
.021	.020	.020	.021	.024	.034	.049	.027	.032	.042	.033	.050	.050	1.25	1.25
.028	.023	.017	.022	.030	.035	.054	.037	.036	.051	.029	.055	.049	1.30	1.30
.033	.029	.017	.022	.028	.032	.059	.035	.038	.053	.032	.055	.049	1.35	1.35
.028	.025	.015	.020	.025	.027	.051	.026	.038	.053	.038	.043	.052	1.40	1.40
.031	.021	.012	.013	.021	.025	.054	.031	.039	.045	.029	.042	.053	1.45	1.45
.027	.019	.010	.010	.015	.027	.048	.021	.024	.042	.037	.049	.051	1.50	1.50
.033	.020	.008	.012	.018	.026	.043	.026	.041	.047	.026	.034	.052	1.55	1.55
.032	.016	.016	.015	.017	.028	.049	.028	.036	.039	.030	.047	.052	1.60	1.60
.031	.022	.020	.022	.024	.031	.051	.031	.036	.039	.031	.059	.048	1.65	1.65
.026	.026	.019	.026	.032	.030	.057	.036	.042	.054	.032	.046	.046	1.70	1.70
.030	.023	.013	.022	.030	.036	.054	.030	.046	.057	.035	.045	.052	1.75	1.75
.368	.362	.353	.361	.369	.382	.344	.343	.343	.339	.343	.342	.342	1.80	1.80
.369	.363	.353	.362	.369	.382	.345	.342	.342	.338	.339	.344	.342	1.85	1.85
.519	.516	.505	.520	.528	.541	.481	.480	.479	.472	.479	.487	.479	1.90	1.90
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.95	1.95
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.00	2.00
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.05	2.05
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.10	2.10
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.15	2.15
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.20	2.20
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.25	2.25
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.30	2.30
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.35	2.35
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.40	2.40
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.45	2.45

Set 2, Table D — Standard Deviation of Mean Local Pressurant  
Fractions, Scaling Runs 237-240

LOCATIONS 1														TAU
1	2	3	4	5	6	7	8	9	10	11	12	13	14	
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.00
.202	.051	.334	.047	.162	.175	.027	.081	.083	.043	.034	.474	.078	.05	.05
.348	.093	.591	.033	.280	.303	.050	.137	.145	.076	.068	.822	.149	.10	.10
.304	.091	.545	.079	.255	.270	.049	.109	.122	.061	.069	.695	.152	.15	.15
.254	.086	.475	.059	.231	.234	.048	.080	.093	.039	.067	.554	.146	.20	.20
.203	.087	.421	.039	.211	.234	.048	.060	.071	.026	.059	.446	.142	.25	.25
.166	.076	.372	.026	.191	.209	.050	.047	.055	.017	.053	.375	.134	.30	.30
.152	.062	.339	.020	.172	.180	.043	.043	.050	.024	.074	.377	.122	.35	.35
.151	.072	.347	.033	.152	.156	.038	.039	.041	.036	.093	.374	.120	.40	.40
.157	.086	.283	.043	.139	.152	.031	.040	.029	.039	.102	.364	.120	.45	.45
.160	.051	.273	.044	.137	.150	.026	.046	.018	.023	.055	.342	.137	.50	.50
.156	.020	.263	.052	.139	.147	.025	.050	.028	.011	.043	.330	.133	.55	.55
.137	.032	.244	.046	.125	.130	.025	.037	.039	.017	.054	.298	.145	.60	.60
.131	.034	.232	.036	.110	.119	.023	.034	.044	.024	.058	.281	.154	.65	.65
.133	.021	.226	.014	.109	.118	.020	.045	.043	.014	.048	.279	.141	.70	.70
.120	.015	.239	.010	.105	.090	.023	.035	.036	.021	.052	.281	.087	.75	.75
.107	.035	.249	.021	.088	.087	.021	.074	.044	.021	.052	.269	.087	.80	.80
.099	.042	.221	.032	.086	.099	.036	.058	.041	.024	.043	.246	.062	.85	.85
.105	.024	.217	.034	.101	.096	.020	.031	.042	.023	.047	.233	.081	.90	.90
.084	.035	.200	.014	.080	.099	.025	.030	.025	.008	.035	.214	.062	.95	.95
.095	.080	.315	.073	.072	.084	.018	.036	.060	.057	.021	.134	.081	1.00	1.00
.077	.036	.157	.033	.071	.073	.023	.030	.034	.041	.030	.104	.121	1.05	1.05
.070	.018	.144	.014	.060	.071	.025	.006	.021	.031	.043	.173	.065	1.10	1.10
.071	.023	.156	.013	.060	.067	.015	.016	.021	.020	.029	.193	.063	1.15	1.15
.069	.031	.137	.015	.048	.060	.009	.025	.025	.019	.033	.179	.065	1.20	1.20
.071	.020	.155	.010	.058	.070	.029	.017	.016	.011	.036	.179	.041	1.25	1.25
.070	.019	.157	.012	.058	.063	.028	.019	.027	.021	.047	.153	.049	1.30	1.30
.067	.018	.159	.012	.062	.060	.028	.022	.015	.012	.043	.170	.053	1.35	1.35
.064	.021	.168	.012	.067	.071	.024	.027	.020	.012	.049	.173	.056	1.40	1.40
.064	.020	.174	.014	.073	.072	.027	.025	.016	.012	.036	.177	.051	1.45	1.45
.071	.025	.168	.010	.067	.075	.023	.027	.008	.015	.039	.182	.040	1.50	1.50
.064	.021	.167	.015	.064	.069	.020	.040	.014	.013	.040	.182	.052	1.55	1.55
.071	.022	.175	.025	.064	.073	.013	.034	.018	.007	.037	.196	.051	1.60	1.60
.372	.494	.471	.501	.567	.578	.470	.502	.476	.464	.455	.483	.450	1.65	1.65
.579	.493	.465	.496	.564	.580	.468	.500	.474	.462	.464	.481	.459	1.70	1.70
.543	.429	.282	.426	.509	.531	.397	.452	.409	.386	.364	.404	.354	1.75	1.75
.542	.430	.279	.420	.511	.531	.393	.448	.412	.382	.360	.423	.349	1.80	1.80
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.85	1.85
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.90	1.90
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.95	1.95
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.00	2.00
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.05	2.05
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.10	2.10
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.15	2.15
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.20	2.20
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.25	2.25
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.30	2.30
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.35	2.35
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.40	2.40
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.45	2.45

Set 3, Table D — Standard Deviation of Mean Local Pressurant Fractions, Scaling Runs 241-244

LOCATIONS 1														YAU
1	2	3	4	5	6	7	8	9	10	11	12	13	14	
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.00
.461	.297	.055	.232	.409	.519	.171	.210	.487	.496	.194	.305	.176	.05	.05
2.345	2.254	1.930	1.717	2.446	3.016	1.969	1.949	1.975	1.990	1.418	2.497	1.980	.10	.10
2.737	2.647	2.292	2.031	2.895	3.524	2.310	2.305	2.298	2.330	1.696	2.940	2.339	.15	.15
1.457	1.321	1.268	1.266	1.346	1.313	1.769	1.004	.718	1.425	.719	1.347	1.066	.20	.20
1.243	1.133	1.098	1.097	1.175	1.215	1.558	.874	.561	1.158	.624	1.267	.965	.25	.25
.141	.138	.163	.138	.137	.202	.271	.058	.015	.063	.089	.294	.112	.30	.30
.086	.114	.118	.082	.100	.103	.035	.065	.082	.095	.114	.177	.052	.35	.35
.049	.036	.017	.014	.022	.020	.063	.078	.041	.038	.036	.097	.036	.40	.40
.082	.051	.039	.031	.022	.032	.051	.061	.051	.035	.061	.039	.058	.45	.45
.059	.016	.028	.042	.045	.018	.016	.039	.039	.025	.018	.059	.045	.50	.50
.017	.031	.043	.042	.043	.027	.027	.050	.014	.007	.026	.082	.048	.55	.55
.017	.014	.036	.025	.011	.045	.052	.024	.039	.018	.028	.044	.044	.60	.60
.040	.028	.031	.037	.039	.023	.095	.062	.012	.021	.040	.031	.033	.65	.65
.029	.040	.030	.032	.040	.007	.092	.079	.011	.028	.025	.049	.025	.70	.70
.056	.037	.044	.043	.031	.047	.040	.026	.027	.041	.043	.069	.025	.75	.75
.031	.029	.019	.054	.017	.024	.020	.020	.026	.047	.037	.021	.049	.80	.80
.036	.032	.035	.043	.041	.040	.018	.040	.046	.058	.049	.045	.048	.85	.85
.054	.026	.020	.022	.039	.045	.018	.038	.026	.014	.018	.030	.010	.90	.90
.021	.021	.031	.024	.049	.063	.038	.039	.031	.018	.022	.076	.057	.95	.95
.029	.024	.020	.016	.025	.045	.045	.070	.052	.031	.027	.044	.047	1.00	1.00
.019	.022	.021	.007	.008	.018	.025	.047	.029	.016	.024	.013	.030	1.05	1.05
.027	.009	.019	.017	.013	.014	.019	.050	.018	.035	.029	.020	.069	1.10	1.10
.005	.008	.017	.006	.010	.006	.027	.042	.011	.024	.014	.018	.012	1.15	1.15
.018	.016	.008	.018	.022	.022	.028	.041	.032	.028	.035	.037	.017	1.20	1.20
.010	.006	.017	.034	.032	.028	.044	.027	.056	.047	.029	.018	.024	1.25	1.25
.022	.011	.020	.038	.043	.039	.038	.024	.068	.045	.044	.030	.017	1.30	1.30
.027	.026	.017	.032	.033	.038	.025	.030	.051	.060	.062	.019	.033	1.35	1.35
.039	.034	.020	.019	.019	.028	.027	.026	.037	.034	.034	.038	.043	1.40	1.40
.030	.017	.020	.029	.036	.020	.021	.028	.021	.025	.036	.034	.054	1.45	1.45
.048	.026	.024	.025	.018	.018	.042	.021	.026	.032	.050	.037	.053	1.50	1.50
.023	.012	.009	.018	.023	.018	.024	.033	.044	.046	.028	.066	.038	1.55	1.55
.015	.015	.012	.038	.024	.023	.029	.040	.052	.025	.031	.051	.042	1.60	1.60
.015	.007	.007	.031	.022	.027	.030	.013	.029	.029	.029	.032	.057	1.65	1.65
.020	.014	.012	.021	.027	.019	.008	.019	.042	.016	.041	.035	.052	1.70	1.70
.010	.013	.030	.013	.006	.021	.016	.028	.035	.009	.009	.054	.063	1.75	1.75
.500	.505	.506	.506	.501	.503	.502	.502	.502	.494	.489	.508	.501	1.80	1.80
.499	.503	.502	.507	.495	.499	.495	.495	.495	.507	.501	.532	.495	1.85	1.85
.497	.505	.503	.509	.497	.499	.493	.493	.493	.505	.505	.536	.493	1.90	1.90
.430	.430	.435	.439	.437	.442	.432	.432	.432	.432	.432	.453	.432	1.95	1.95
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.00	2.00
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.05	2.05
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.10	2.10
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.15	2.15
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.20	2.20
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.25	2.25
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.30	2.30
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.35	2.35
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.40	2.40
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.45	2.45

Set 4, Table D — Standard Deviation of Mean Local Pressurant  
Fractions, Scaling Runs 245-248

LOCATIONS I														TAU
1	2	3	4	5	6	7	8	9	10	11	12	13	14	
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.00
.251	.150	.202	.132	.158	.185	.156	.151	.158	.215	.122	.163	.164	.164	.05
1.257	.955	.655	.621	.926	1.127	1.103	.938	.592	.845	.449	.894	.716	.716	.10
3.208	3.014	3.441	2.905	4.132	3.890	5.483	3.670	2.161	1.515	1.534	3.841	2.452	1.5	.15
11.231	11.012	12.643	10.747	15.074	13.898	20.263	13.954	7.671	5.018	5.062	14.006	8.702	2.0	.20
5.498	5.357	6.103	5.189	7.248	6.629	9.751	6.699	3.702	2.535	2.503	6.714	4.174	2.5	.25
.242	.240	.266	.205	.233	.250	.447	.282	.095	.108	.101	.323	.267	.30	.30
.166	.100	.193	.112	.111	.067	.202	.183	.078	.075	.061	.232	.219	.35	.35
.109	.102	.061	.036	.072	.064	.096	.126	.076	.060	.082	.185	.190	.40	.40
.097	.075	.083	.049	.060	.069	.096	.104	.041	.059	.041	.106	.121	.45	.45
.080	.046	.062	.033	.039	.044	.057	.068	.055	.063	.027	.040	.063	.50	.50
.045	.026	.044	.024	.029	.030	.070	.021	.011	.009	.042	.032	.031	.55	.55
.040	.034	.019	.005	.046	.077	.089	.069	.031	.032	.040	.085	.050	.60	.60
.049	.047	.015	.013	.029	.035	.054	.064	.030	.042	.060	.014	.023	.65	.65
.020	.022	.046	.044	.026	.016	.022	.055	.057	.043	.011	.076	.051	.70	.70
.032	.041	.042	.017	.027	.026	.103	.093	.012	.035	.047	.023	.056	.75	.75
.036	.032	.030	.028	.060	.044	.079	.065	.067	.030	.052	.020	.020	.80	.80
.045	.060	.062	.057	.057	.057	.073	.051	.041	.035	.031	.051	.058	.85	.85
.021	.025	.040	.025	.023	.031	.109	.078	.038	.048	.025	.029	.038	.90	.90
.033	.032	.033	.019	.022	.024	.073	.057	.041	.022	.037	.054	.025	.95	.95
.043	.035	.030	.047	.024	.020	.046	.051	.061	.053	.038	.043	.060	1.00	1.00
.033	.025	.024	.032	.027	.028	.030	.012	.004	.008	.007	.003	.013	1.05	1.05
.029	.024	.026	.011	.021	.020	.008	.018	.022	.023	.030	.035	.019	1.10	1.10
.032	.029	.037	.031	.032	.039	.011	.027	.040	.042	.035	.033	.024	1.15	1.15
.038	.037	.027	.040	.038	.048	.025	.020	.045	.057	.038	.040	.025	1.20	1.20
.035	.031	.015	.035	.045	.043	.020	.029	.053	.039	.018	.040	.034	1.25	1.25
.042	.027	.011	.018	.018	.042	.023	.020	.015	.032	.019	.022	.029	1.30	1.30
.036	.021	.010	.019	.020	.027	.025	.022	.015	.015	.021	.051	.030	1.35	1.35
.024	.022	.006	.018	.008	.025	.027	.068	.016	.017	.039	.072	.028	1.40	1.40
.015	.031	.017	.018	.020	.025	.018	.029	.021	.027	.045	.058	.038	1.45	1.45
.016	.011	.019	.021	.010	.028	.031	.031	.041	.047	.049	.032	.014	1.50	1.50
.029	.018	.011	.019	.027	.026	.020	.035	.048	.052	.040	.029	.038	1.55	1.55
.025	.010	.012	.015	.017	.031	.012	.024	.037	.023	.015	.051	.021	1.60	1.60
.019	.010	.016	.007	.017	.021	.017	.021	.024	.024	.019	.056	.015	1.65	1.65
.012	.011	.019	.012	.006	.023	.021	.021	.027	.012	.025	.052	.035	1.70	1.70
.489	.486	.481	.494	.497	.511	.487	.495	.487	.508	.479	.521	.521	1.75	1.75
.419	.415	.407	.427	.427	.446	.411	.450	.412	.449	.411	.450	.450	1.80	1.80
.414	.422	.418	.440	.426	.433	.414	.454	.454	.416	.414	.454	.416	1.85	1.85
.419	.421	.425	.449	.421	.432	.445	.445	.445	.405	.405	.445	.414	1.90	1.90
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.95	1.95
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.00	2.00
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.05	2.05
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.10	2.10
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.15	2.15
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.20	2.20
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.25	2.25
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.30	2.30
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.35	2.35
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.40	2.40
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.45	2.45

**E-Tables**

These tables give the local mean pressurant fraction deviations for dimensionless-time values 0.00 to 2.45. By pressurant-fraction deviation, we mean the ratio of the difference between the local pressurant and the mean pressurant fraction at time  $t$  to the mean pressurant fraction at the time of valve closure,  $t = t_c$ . As in the D-tables, these values are given at equal intervals of dimensionless time  $\tau$  (see Appendix C for program).

Set 1, Table E — Deviations of Mean Local Pressurant Fractions,  
Scaling Runs 230-236

LOCATIONS 1														TAU
1	2	3	4	5	6	7	8	9	10	11	12	13	14	
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.00
-278	-163	-003	-067	-175	-170	.221	.067	.051	.144	.055	.175	.137	.05	.05
-329	-315	-008	-127	-313	-325	.425	.127	.100	.277	.103	.340	.260	.10	.10
-458	-284	-033	-126	-304	-295	.382	.118	.102	.261	.087	.306	.229	.15	.15
-343	-227	-062	-117	-238	-193	.297	.112	.093	.217	.066	.226	.169	.20	.20
-227	-168	-090	-107	-170	-102	.208	.102	.085	.173	.044	.146	.109	.25	.25
-138	-122	-108	-096	-115	-029	.135	.101	.076	.137	.029	.078	.061	.30	.30
-117	-111	-111	-087	-096	-011	.115	.096	.072	.121	.030	.056	.044	.35	.35
-100	-103	-114	-075	-081	-001	.102	.088	.070	.105	.033	.045	.033	.40	.40
-083	-090	-110	-066	-068	.008	.086	.080	.066	.086	.032	.037	.024	.45	.45
-066	-070	-098	-060	-057	.012	.061	.061	.055	.068	.028	.040	.028	.50	.50
-047	-054	-085	-055	-045	.013	.039	.041	.043	.053	.023	.041	.031	.55	.55
-027	-038	-067	-043	-027	.028	.016	.022	.026	.042	.019	.035	.011	.60	.60
-007	-021	-050	-026	-007	.042	-.017	.011	.012	.026	.013	.024	-.007	.65	.65
-002	-013	-038	-010	.009	.055	-.023	.008	.010	.008	-.000	.004	-.016	.70	.70
.006	-.007	-.035	-.004	.017	.061	-.022	.003	.007	.002	.001	.002	-.024	.75	.75
.016	.003	-.039	-.006	.017	.061	-.023	-.005	.001	.005	.002	.004	-.030	.80	.80
.026	.010	-.038	-.012	.013	.059	-.020	-.001	.009	.007	.010	-.007	-.047	.85	.85
.017	.008	-.023	-.003	.019	.064	-.039	.008	-.003	-.005	.002	-.004	-.042	.90	.90
.026	.011	-.031	-.008	.019	.066	-.026	.009	.006	-.014	-.003	-.009	-.044	.95	.95
.040	.013	-.029	-.001	.028	.069	-.025	-.005	.001	-.011	-.017	-.015	-.042	1.00	1.00
.044	.027	-.013	.010	.039	.080	-.027	-.017	-.017	-.027	-.025	-.028	-.043	1.05	1.05
.047	.034	-.001	.018	.051	.081	-.032	-.018	-.019	-.034	-.031	-.039	-.053	1.10	1.10
.048	.031	.002	.020	.054	.088	-.025	-.021	-.022	-.034	-.039	-.045	-.053	1.15	1.15
.060	.042	.007	.031	.057	.086	-.032	-.023	-.032	-.046	-.042	-.055	-.050	1.20	1.20
.060	.045	.011	.028	.054	.087	-.033	-.029	-.030	-.048	-.040	-.051	-.049	1.25	1.25
.061	.042	.010	.028	.048	.084	-.040	-.030	-.031	-.040	-.044	-.042	-.041	1.30	1.30
.060	.039	.005	.026	.048	.081	-.042	-.028	-.032	-.043	-.036	-.041	-.031	1.35	1.35
.062	.041	.003	.024	.050	.086	-.034	-.025	-.039	-.051	-.039	-.041	-.024	1.40	1.40
.059	.039	.003	.025	.044	.081	-.033	-.023	-.025	-.043	-.043	-.038	-.041	1.45	1.45
.053	.032	-.002	.020	.040	.084	-.029	-.019	-.025	-.044	-.039	-.032	-.034	1.50	1.50
.051	.029	-.003	.018	.040	.079	-.032	-.015	-.023	-.042	-.032	-.030	-.037	1.55	1.55
.047	.026	-.006	.019	.044	.080	-.025	-.019	-.020	-.035	-.037	-.030	-.041	1.60	1.60
.047	.029	-.002	.021	.048	.081	-.027	-.015	-.016	-.042	-.040	-.034	-.046	1.65	1.65
.050	.031	-.003	.021	.050	.086	-.026	-.017	-.023	-.043	-.043	-.031	-.049	1.70	1.70
.055	.031	-.002	.025	.057	.097	-.029	-.022	-.035	-.050	-.040	-.036	-.047	1.75	1.75
.037	.021	-.000	.018	.040	.071	-.021	-.026	-.026	-.034	-.025	-.026	-.029	1.80	1.80
.038	.025	.002	.021	.039	.071	-.020	-.026	-.028	-.037	-.032	-.021	-.028	1.85	1.85
.017	.015	.006	.018	.026	.037	-.013	-.016	-.017	-.023	-.017	-.010	-.017	1.90	1.90
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.95	1.95
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.00	2.00
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.05	2.05
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.10	2.10
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.15	2.15
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.20	2.20
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.25	2.25
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.30	2.30
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.35	2.35
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.40	2.40
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.45	2.45

7 CASES

Set 2, Table E — Deviations of Mean Local Pressurant Fractions,  
Scaling Runs 237-240

LOCATIONS 1														TAU
1	2	3	4	5	6	7	8	9	10	11	12	13	14	
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.00
-305	-095	.542	-.047	-.213	-.213	-.034	-.135	-.145	-.079	-.016	.644	.104	.03	
-570	-183	1.019	-.090	-.395	-.395	-.065	-.233	-.273	-.148	-.034	1.200	.197	.10	
-549	-194	1.013	-.103	-.384	-.376	-.082	-.252	-.275	-.162	-.063	1.227	.200	.15	
-496	-194	.946	-.114	-.333	-.336	-.098	-.237	-.260	-.166	-.095	1.210	.187	.20	
-444	-194	.873	-.113	-.319	-.293	-.114	-.216	-.241	-.165	-.119	1.164	.177	.25	
-405	-191	.810	-.112	-.284	-.247	-.130	-.196	-.228	-.170	-.138	1.134	.163	.30	
-406	-185	.793	-.107	-.260	-.214	-.154	-.194	-.235	-.187	-.132	1.141	.140	.35	
-399	-172	.775	-.109	-.237	-.181	-.178	-.191	-.245	-.200	-.119	1.151	.108	.40	
-385	-145	.767	-.120	-.221	-.158	-.201	-.194	-.257	-.226	-.097	1.160	.066	.45	
-357	-.086	.782	-.138	-.210	-.140	-.219	-.201	-.271	-.245	-.110	1.166	.025	.50	
-335	-.040	.796	-.147	-.197	-.125	-.235	-.209	-.271	-.253	-.142	1.162	-.006	.55	
-315	-.070	.812	-.138	-.166	-.103	-.240	-.202	-.270	-.254	-.157	1.138	-.033	.60	
-300	-.109	.823	-.135	-.143	-.086	-.234	-.194	-.274	-.261	-.157	1.117	-.049	.65	
-285	-.121	.818	-.156	-.151	-.092	-.224	-.200	-.266	-.263	-.150	1.085	.001	.70	
-266	-.121	.803	-.176	-.163	-.110	-.196	-.194	-.259	-.259	-.125	1.060	.002	.75	
-245	-.131	.794	-.181	-.184	-.131	-.169	-.171	-.233	-.249	-.090	1.044	-.039	.80	
-227	-.092	.765	-.186	-.156	-.063	-.179	-.183	-.233	-.253	-.110	1.017	-.093	.85	
-218	-.102	.754	-.172	-.126	-.049	-.200	-.158	-.222	-.218	-.112	.987	-.167	.90	
-188	-.122	.717	-.167	-.110	-.064	-.180	-.156	-.216	-.219	-.088	.934	-.147	.95	
-070	-.024	.342	-.100	-.061	-.038	-.148	-.115	-.162	-.172	-.060	.633	-.023	1.00	
.023	-.021	-.009	-.066	.013	.052	-.066	-.033	-.067	-.067	-.045	.300	-.006	1.05	
.061	-.011	-.041	-.030	.053	.094	-.059	-.017	-.046	-.057	-.061	.181	-.063	1.10	
.076	-.003	-.058	-.019	.067	.100	-.056	-.022	-.051	-.056	-.055	.172	-.088	1.15	
.084	.001	-.063	-.007	.082	.110	-.061	-.016	-.056	-.071	-.075	.167	-.091	1.20	
.084	-.001	-.067	-.006	.082	.114	-.051	-.013	-.049	-.064	-.066	.139	-.097	1.25	
.088	-.003	-.074	-.010	.074	.108	-.048	-.007	-.048	-.061	-.067	.152	-.097	1.30	
.083	-.008	-.082	-.018	.070	.101	-.044	-.002	-.032	-.057	-.072	.148	-.086	1.35	
.090	-.001	-.073	-.013	.082	.109	-.057	-.014	-.045	-.057	-.070	.139	-.088	1.40	
.091	.003	-.067	-.009	.080	.110	-.061	-.021	-.052	-.064	-.063	.149	-.088	1.45	
.091	-.004	-.080	-.014	.077	.111	-.049	-.022	-.046	-.069	-.067	.156	-.084	1.50	
.098	-.001	-.071	-.004	.074	.111	-.061	-.011	-.060	-.072	-.072	.154	-.080	1.55	
.093	.001	-.064	.001	.079	.106	-.053	.001	-.070	-.083	-.082	.163	-.087	1.60	
.074	-.001	-.052	.005	.071	.081	-.025	.005	-.019	-.032	-.041	-.013	-.048	1.65	
.080	-.003	-.057	.001	.067	.083	-.028	.003	-.021	-.034	-.034	-.015	-.040	1.70	
.070	.004	-.081	.002	.050	.063	-.014	.017	-.008	-.021	-.033	-.010	-.039	1.75	
.069	.005	-.083	.003	.052	.063	-.017	.015	-.006	-.023	-.036	.001	-.042	1.80	
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.85	
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.90	
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.95	
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.00	
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.05	
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.10	
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.15	
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.20	
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.25	
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.30	
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.35	
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.40	
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.45	

4 CASES

NRL REPORT 8523

Set 3, Table E — Deviations of Mean Local Pressurant Fractions,  
Scaling Runs 241-244

LOCATIONS 1														TAU	
1	2	3	4	5	6	7	8	9	10	11	12	13	14	TAU	TAU
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.00	0.00
.757	.485	-.065	.214	.508	.793	-.356	-.251	-.499	-.404	-.293	-.455	-.360	.05		
-1.867	-1.799	-1.735	-1.486	-2.009	-2.329	1.703	1.763	1.445	1.508	1.088	2.049	1.669	.10		
-2.344	-2.339	-2.008	-1.046	-2.591	-3.092	2.193	2.183	1.502	1.989	1.401	2.622	2.124	.15		
-1.487	-1.349	-1.251	-1.252	-1.472	-1.540	1.671	1.161	.780	1.332	.747	1.495	1.159	.20		
-1.635	-.925	-.873	-.891	-1.002	-1.045	1.227	.816	.513	.887	.494	1.074	.760	.25		
-.263	-.243	-.234	-.252	-.275	-.331	.332	.241	.147	.174	.125	.402	.187	.30		
-.110	-.153	-.147	-.147	-.186	-.211	.094	.113	.146	.130	.090	.273	.107	.35		
-.024	-.060	-.060	-.055	-.084	-.121	.024	.027	.045	.035	-.002	.184	.100	.40		
.018	-.004	-.016	-.018	-.025	-.032	-.024	-.011	-.011	.013	-.042	.107	.062	.45		
.045	.016	-.006	-.033	-.029	-.027	-.065	-.016	-.004	-.006	-.027	.104	.040	.50		
.022	.019	-.003	-.008	.004	.006	-.098	-.045	-.012	-.017	-.029	.115	.044	.55		
.025	.021	.008	.017	.019	.036	-.138	-.074	-.001	-.027	-.032	.098	.042	.60		
.045	.022	.013	.032	.055	.078	-.201	-.081	-.021	-.021	-.042	.090	.037	.65		
.063	.065	.051	.062	.057	.011	-.177	-.120	-.027	-.025	-.034	.055	.016	.70		
.081	.055	.043	.018	.015	.011	-.182	-.141	-.012	.013	-.028	.099	.032	.75		
.076	.064	.045	.023	.044	.021	-.212	-.193	-.008	-.027	-.029	.110	.045	.80		
.056	.060	.033	.068	.076	.065	-.230	-.144	-.039	-.031	-.045	.076	.038	.85		
.073	.053	.034	.028	.007	-.006	-.223	-.107	.004	-.003	.007	.083	.047	.90		
.051	.042	.026	.030	.032	.046	-.203	-.151	.003	-.009	-.011	.099	.055	.95		
.095	.077	.051	.069	.077	.078	-.171	-.166	-.018	-.042	-.054	.015	-.016	1.00		
.071	.054	.033	.023	.030	.041	-.154	-.109	-.002	-.014	-.017	.044	-.003	1.05		
.028	.017	.014	.017	.030	.032	-.129	-.104	.013	.001	-.006	.059	.019	1.10		
.024	.015	.014	.027	.030	.048	-.118	-.101	-.001	.004	.003	.053	-.003	1.15		
.030	.019	.008	.021	.027	.057	-.088	-.089	-.004	-.010	-.014	.054	-.016	1.20		
.033	.028	.019	.032	.022	.033	-.090	-.065	-.027	-.039	-.013	.060	.001	1.25		
.036	.029	.023	.039	.025	.029	-.092	-.063	-.033	-.027	-.023	.079	-.029	1.30		
.040	.028	.020	.023	.013	.025	-.083	-.026	-.029	-.021	-.029	.071	-.032	1.35		
.034	.026	.011	.028	.028	.034	-.076	-.057	-.038	-.024	-.016	.074	-.030	1.40		
.034	.029	.024	.038	.035	.048	-.084	-.073	-.038	-.034	-.015	.057	-.028	1.45		
.035	.029	.021	.033	.028	.047	-.069	-.033	-.057	-.034	-.011	.032	-.027	1.50		
.014	.004	-.003	.018	.021	.027	-.032	-.022	-.048	-.043	.003	.074	-.020	1.55		
.004	.015	.002	.022	.004	.018	-.041	-.027	-.052	-.014	-.002	.093	-.028	1.60		
.010	.011	-.003	.016	.003	.016	-.030	-.014	-.028	-.028	-.028	.098	-.028	1.65		
.004	.003	.003	.016	.008	.012	-.014	-.003	-.028	-.024	-.016	.080	-.044	1.70		
.007	.006	-.007	.017	.005	.017	-.022	-.010	-.008	-.008	-.008	.058	-.049	1.75		
-.002	.003	.004	.006	-.001	.001	.000	.000	.000	-.008	-.012	.006	-.001	1.80		
-.003	.002	0.000	.005	-.007	-.003	-.007	-.007	-.007	.005	-.001	.030	-.007	1.85		
-.004	-.002	.002	.007	-.004	-.003	-.009	-.009	-.009	.003	.003	.034	-.009	1.90		
-.003	-.003	-.001	.002	.001	.003	-.002	-.002	-.002	-.002	-.002	.010	-.002	1.95		
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.00		
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.05		
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.10		
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.15		
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.20		
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.25		
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.30		
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.35		
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.40		
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.45		

4 CASES



Set 4, Table E — Deviations of Mean Local Pressurant Fractions,  
Scaling Runs 245-248

LOCATIONS 1														TAU	
1	2	3	4	5	6	7	8	9	10	11	12	13	14	TAU	TAU
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.00	0.00
.690	.512	.305	.304	.483	.608	-.598	-.349	-.389	-.413	-.331	-.436	-.379	-.05		
.687	.596	.615	.343	.544	.592	-.697	-.562	-.498	-.530	-.134	-.509	-.450	.10		
-.526	-.567	-.950	-.968	-1.398	-1.249	1.934	1.178	.528	.043	.349	1.245	.389	.15		
-2.755	-2.987	-4.638	-3.938	-5.712	-5.172	7.674	5.191	2.813	1.185	1.122	5.136	1.981	.20		
-1.370	-1.442	-2.275	-1.959	-2.781	-2.558	3.704	2.591	1.382	.573	.570	2.546	1.020	.25		
-.464	-.430	-.459	-.392	-.470	-.496	.665	.528	.250	.145	.176	.539	.407	.30		
-.256	-.209	-.292	-.221	-.253	-.235	.350	.325	.123	.041	.034	.385	.205	.35		
-.108	-.116	-.096	-.116	-.102	-.137	.195	.207	.048	.007	-.056	.231	.118	.40		
-.017	-.028	-.069	-.077	-.137	-.092	.123	.128	-.005	-.017	-.048	.120	.113	.45		
-.020	-.009	-.060	-.061	-.060	-.037	.039	.057	.007	-.019	-.044	.125	.053	.50		
.061	.032	0.000	-.004	-.019	-.007	-.087	-.048	-.063	-.055	-.023	.138	.070	.55		
.055	.036	.025	.023	.017	.007	-.197	-.098	-.055	-.053	-.031	.155	.115	.60		
.075	.078	.043	.051	.019	.023	-.201	-.098	-.032	-.047	-.051	.097	.039	.65		
.061	.062	.059	.061	.065	.086	-.257	-.171	-.060	-.061	-.018	.112	.066	.70		
.121	.098	.058	.053	.068	.061	-.299	-.181	-.078	-.043	-.029	.095	.067	.75		
.123	.104	.087	.078	.071	.066	-.291	-.224	-.062	-.041	-.044	.074	.055	.80		
.102	.071	.065	.095	.118	.132	-.326	-.215	-.071	-.043	-.004	.046	.026	.85		
.145	.123	.081	.100	.122	.138	-.336	-.242	-.086	-.070	-.022	.061	-.003	.90		
.123	.125	.116	.113	.127	.131	-.272	-.230	-.084	-.065	-.098	-.009	.017	.95		
.136	.120	.085	.092	.090	.130	-.269	-.226	-.115	-.085	-.053	.044	.051	1.00		
.080	.072	.058	.062	.067	.065	-.166	-.152	-.054	-.050	-.016	.034	-.002	1.05		
.058	.046	.029	.032	.040	.044	-.107	-.123	-.026	-.020	-.022	.037	.009	1.10		
.046	.033	.027	.017	.028	.049	-.096	-.096	-.014	-.027	-.021	.055	-.003	1.15		
.052	.041	.038	.050	.045	.065	-.100	-.093	-.035	-.061	-.037	.065	-.026	1.20		
.042	.050	.038	.065	.057	.071	-.107	-.099	-.050	-.066	-.043	.056	-.016	1.25		
.039	.033	.031	.057	.043	.076	-.112	-.104	-.044	-.047	-.017	.055	-.013	1.30		
.017	.018	.019	.039	.043	.048	-.095	-.071	-.038	-.038	-.023	.098	-.019	1.35		
.030	.020	.002	.020	.019	.023	-.055	-.056	-.046	-.034	-.012	.087	.001	1.40		
.028	.028	.012	.021	.007	.031	-.063	-.033	-.041	-.051	-.018	.096	-.017	1.45		
.028	.014	.009	.026	.017	.031	-.033	-.033	-.052	-.048	-.015	.069	-.016	1.50		
.023	.015	.002	.022	.028	.037	-.027	-.041	-.056	-.033	-.025	.083	-.027	1.55		
.006	-.003	-.012	.013	.023	.052	-.039	-.027	-.035	-.025	-.026	.082	-.011	1.60		
-.004	-.013	-.023	.002	.022	.052	-.039	-.027	-.026	-.026	-.026	.095	.012	1.65		
-.013	-.014	-.037	-.008	.009	.042	-.029	-.029	-.028	-.010	-.017	.088	.043	1.70		
-.007	-.011	-.016	-.002	0.000	.014	-.011	-.003	-.011	.011	-.018	.024	.024	1.75		
-.006	-.008	-.012	-.001	-.001	.010	-.010	.012	-.009	.012	-.010	.012	.012	1.80		
-.008	-.004	-.006	.007	-.002	.003	-.008	.014	.014	-.007	-.008	.014	-.007	1.85		
-.006	-.004	-.002	.012	-.004	.002	.009	.009	.009	-.014	-.014	.009	-.008	1.90		
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.95		
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.00		
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.05		
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.10		
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.15		
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.20		
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.25		
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.30		
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.35		
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.40		
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	2.45		

4 CASES

## DISCUSSION

For convenience of discussion, we have plotted in Figs. 6 through 9 typical data from the four sets of experiments described in Table 1. Mean local pressurant fractions for selected  $I$  locations,  $\bar{X}_I$ , are plotted vs dimensionless times  $\tau$ . From scale-modeling considerations [2], values of  $\tau$  are defined for the pressurization period as follows:

$$\tau = \bar{X}/\bar{X}_c \quad (t < t_c)$$

and

$$\tau - 1 = (t - t_c)/\theta_c \quad (t > t_c),$$

where  $t_c$  is the time of valve closure,  $\bar{X} = \bar{X}_c$  when  $t = t_c$ , and

$$\theta_c = -[\ln(1 - \bar{X})/dt]_{t=t_c}^{-1}.$$

Typical error bars are given in Figs. 6 to 9 for  $I$  location number 8; they show  $\pm 1$  standard deviation. In general, these data are statistically meaningless for low values of  $\tau$ , below 0.5 or 0.6. We attribute this condition at the beginning of each experimental run to the time required for control valves to open (about 2 s) and for flows to become quasi-steady. The analysis that infers local pressurant history from measured local temperature history, called the thermal method [2], assumes quasi-steady flow conditions. Response times for the bare-wire thermocouples, 0.1 mm in diameter, are conservatively 0.2 s or less; bead diameters are 2 to 2.5 times the wire diameter. Thus, these results represent engineering approximations, average values that show no turbulent structure. Even so, the data imply that the gases mix rapidly and that no pockets with large excesses of oxygen or nitrogen gas exist for any appreciable time period.

In Fig. 6, we show typical local mean pressurant mole fractions at three  $I$ -locations for experimental set 1, which had seven replicate runs. The solid line represents perfect mixing; at  $\tau = 1.0$ ,  $t = t_c$ . With pressurant delivered from three 32.79-mm nozzles at Mach-1 velocities, mixing is almost instantaneous when there are no flow obstacles. These  $I$ -locations are off center, 0.6 of the distance to the

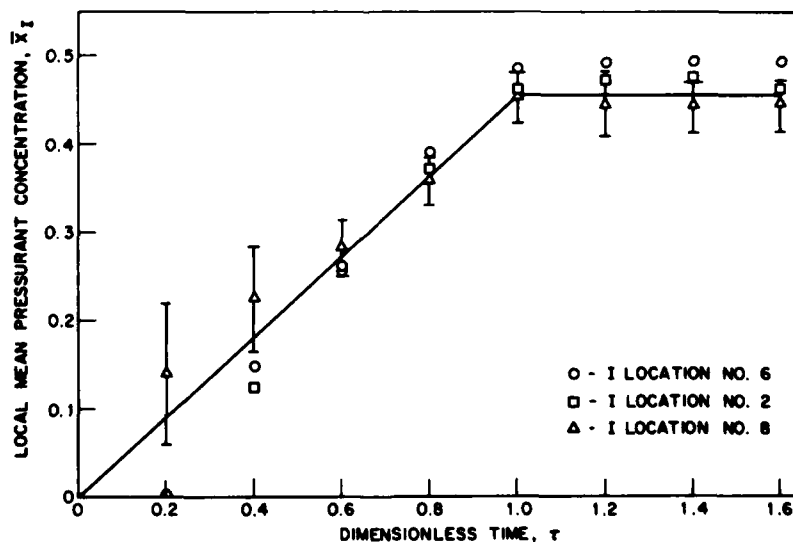


Fig. 6 — Local mean pressurant concentration (mole fraction) vs dimensionless time for three  $I$  locations of experimental set 1, off-center thermocouple-array position 1 with three nozzles and no flow obstacle

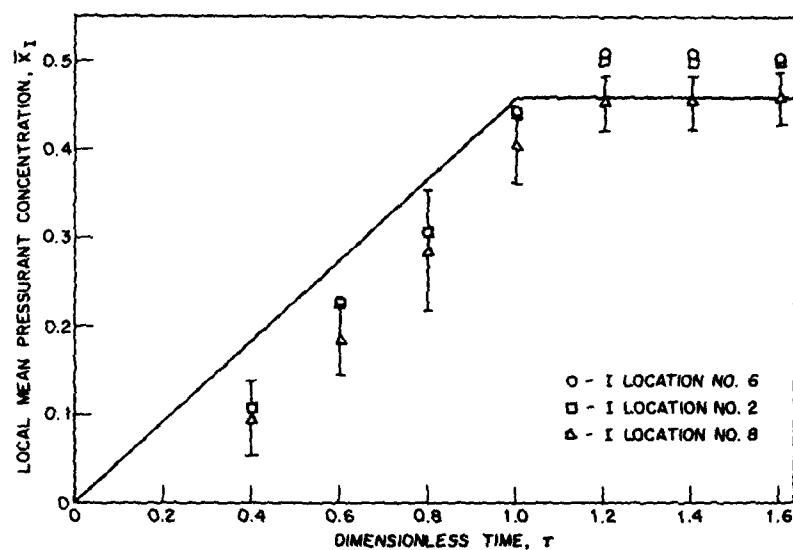


Fig. 7 — Local mean pressurant concentration (mole fraction) vs dimensionless time for three / locations of experimental set 2, chamber-centerline thermocouple-array position 2, with three nozzles and no flow obstacle

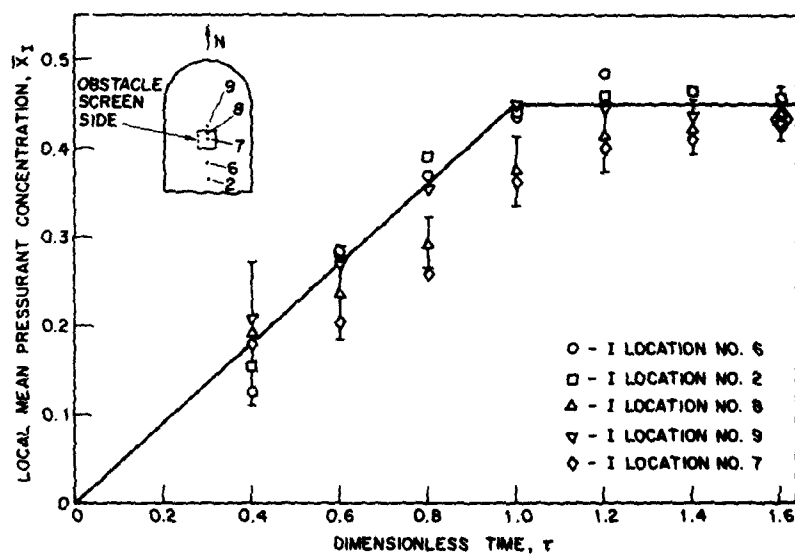


Fig. 8 — Local mean pressurant concentration (mole fraction) vs dimensionless time for five / locations of experimental set 3, centerline thermocouple-array position 2, with the south nozzle and flow obstacle, screen side facing west.

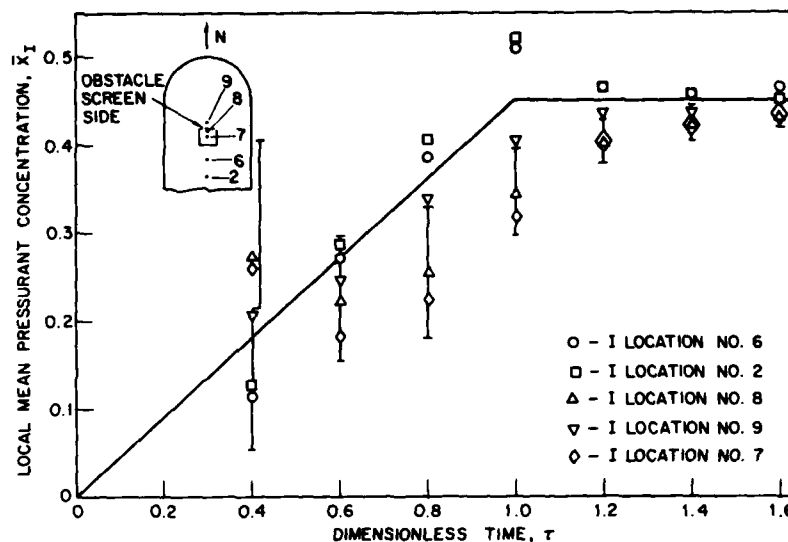


Fig. 9 — Local mean pressurant concentration (mole fraction) vs dimensionless time for five  $I$  locations of experimental set 4, centerline thermocouple-array position 2, with the south nozzle and flow obstacle, screen side facing north.

chamber wall. Figure 7 shows the same experimental conditions, but the  $I$ -locations are along the chamber centerline. Notice that mixing is less rapid here, and 1.2 injection times pass before complete mixing is indicated. These data represent set 2, which had four replicate runs. Although pressurant deficiencies were small, they were statistically significant. These centerline  $I$ -locations were not beneath any of the three nozzles, where pressurant concentrations are high.

Experimental sets 3 and 4 were performed with a flow obstacle; Figs. 8 and 9, respectively, show typical data for them. The obstacle was a cabinetlike enclosure with top, bottom, and three sides closed; the fourth side was covered with a screen wire. As the sketches in Figs. 8 and 9 show,  $I$ -locations 7 and 8 are inside the obstacle and  $I$ -location 9 is directly behind the obstacle (see Fig. 5), relative to the south-nozzle location. Pressurant was injected only from the south nozzle in sets 3 and 4, thus giving the most severe conditions for mixing; injection times were about 30 s. With the obstacle screen side facing west, Fig. 8 shows that pressurant is mixed inside and behind the obstacle within about 1.4 injection times. With the screen side facing north, Fig. 9 shows that these conditions are met in about 1.6 injection times.

## REFERENCES

1. H.W. Carhart and G.H. Fielding, "Applications of Gaseous Fire Extinguishants in Submarines," in *Proceedings of a Symposium on Appraisal of Halogenated Fire Extinguishing Agents*, National Academy of Sciences, National Research Council, Washington, D.C., Apr. 1972, pp. 239-256.
2. R.C. Corlett, J.P. Stone, and F.W. Williams, "Scale Modeling of Inert Pressurant Distribution," *Fire Technology* 16, 259-272 (Nov. 1980).
3. H.S. Bean, ed., *Fluid Meters: Their Theory and Application*, 6th ed., American Society of Mechanical Engineers, New York, 1971.
4. A.S. Shapiro, *The Dynamics and Thermodynamics of Compressible Fluid Flow*, Ronald Press, New York, 1953, Vol. 1, pp. 83-93.

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5. J.P. Stone, R.C. Corlett, J.I. Alexander, and F.W. Williams, "NRL 5-m<sup>3</sup> Chamber Pressurization Experiment: Pressurant Concentration Histories," NRL Report 8503, Sept. 8, 1981.
6. R.C. Corlett, University of Washington, original computer programs written under Contract N00014-75-C-1085 (1979).

## **APPENDIX A**

**Programs BIGST and PRODF accept raw data tapes and produce the A-tables [6].**

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BIGST T=00004 IS ON CR00069 USING 00075 BLKS R=0000

```

0001 FTH4
0002 C-----C
0003      PROGRAM BIGST
0004 C
0005 C      VERSION 800721--4    BY STEVE LUSTIG
0006 C
0007 C-----FUNCTIONS:-----C
0008 C 1) TO MAKE ASCII DISC FILES FROM EBCDIC DATA
0009 C     LOGGER TAPES
0010 C 2) TO MAKE ASCII DISC FILES FROM ASCII OR
0011 C     EBCDIC MASTER TAPE
0012 C 3) TO BUILD ASCII MASTER TAPE FROM EBCDIC
0013 C     DATA LOGGER TAPES
0014 C 4) TO BUILD A 'PRODA INPUT TAPE' FROM DISC FILES
0015 C 5) TO PRINT DISC FILES ON LINEPRINTER/TERMINAL
0016 C
0017 C-----MISCELLANEOUS:-----C
0018 C 1) THIS PROGRAM & ITS SUBROUTINES CALL:
0019 C
0020 C 2) DATA LOGGERS WHICH THIS PROGRAM ACCOMMODATES:
0021 C     DORIC #220 (FIXED,EBCDIC)
0022 C     DORIC #220 (MOBILE,EBCDIC)
0023 C     DORIC #240 (MOBILE,EBCDIC)
0024 C 3) THIS PROGRAM ASSUMES:
0025 C     -MAXIMUM 20 CHANNELS/SCAN
0026 C     ( 0< CHANNEL #'S < 100 )
0027 C     -TAPE DRIVES LU9 & LU18 ARE AVAILABLE
0028 C     ON REQUEST
0029 C     -MASTER TAPE CHARACTER SET IS ASCII
0030 C 4) NO FUNCTION IN THIS PROGRAM IS DEPENDENT
0031 C     ON THE USER'S RUNNING ANY PREVIOUS FUNCTION
0032 C     DURING THE SAME SCHEDULING OF THIS PROGRAM
0033 C-----C
0034      COMMON LU(5),NAME(3,20),NAMCNT,(CR(20),IPAST(3),IBUFR(272),
0035      +IDCB(272),ISCR(214)
0036      INTEGER BMD,IBLANK(384),ANS
0037      DATA IBLANK/384*2H /
0038 C
0039 C      -----DETERMINE LUN OF THE DEVICE-----
0040      CALL RMPAR(LU)
0041 C      -----ARRAY PAST ACCOUNTS VISITED TASKS-----
0042      DO 1 I=1,3
0043      1  IPAST(I)=0
0044      NAMCNT = 0
0045 C      -----DETERMINE TASK-----
0046      2  WRITE(LU,5)
0047      3  FORMAT(1X 'ENTER:      0      TO CREATE ASCII DISC FILE'
0048      +/17X,'FROM ONE DATA LOGGER TAPE'
0049      +/17X,'OR MASTER TAPE'
0050      +/11X,'1      TO CREATE ASCII DISC FILES FROM'
0051      +/17X,'FROM 2 DATA LOGGER TAPES'
0052      +/11X,'2      TO CREATE A MASTER TAPE FROM DISC FILES'
0053      +/11X,'3      TO LIST DATA ON A PRODA INPUT TAPE'
0054      +/17X,'OR ON A TERMINAL/LINEPRINTER'
0055      +/11X,'4      TO END PROGRAM')
0056      READ(LU,*)NODE
0057      GO TO (100,100,200,300,400),NODE+1
0058 C

```

```

0059 C
0060 C      100 IPAST(1)=1
0061 C
0062 C      FUNCTION: TO TRANSFER A FILE (EG. DATA) OF ANY RECORD C
0063 C                  LENGTH FROM MT TO ONE OF THE PLATTERS C
0064 C      FORMAT: USER IS REQUIRED TO INPUT RECORD LENGTH C
0065 C                  THIS FUNCTION USES ONLY AS MUCH SPACE AS FILE C
0066 C                  REQUIRES, RETURNING THE REST BACK TO FNGR. C
0067 C      !!MAXIMUM OF 20 CHANNELS/SCAN!!(SOUNDS REASONABLE) C
0068 C-----C
0069 C      7 ITAPE=MODE+1
0070 C
0071 C
0072 C      IF(ITAPE.EQ.1)WRITE(LU,15)
0073 C      IF(ITAPE.EQ.2)WRITE(LU,16)
0074 C      15 FORMAT('MOUNT TAPE ON LU 8 ..... ENTER "1" WHEN READY')
0075 C      16 FORMAT('MOUNT TAPE WITH 1ST CHANNELS ON LU 8',
0076 C      1/'MOUNT TAPE WITH 2ND CHANNELS ON LU 10',
0077 C      2/'ENTER "1" WHEN READY')
0078 C      READ(LU,*)IANS
0079 C
0080 C-----CHARACTERS/RECORD FOR BUFFER
0081 C
0082 C      WRITE(LU,35)
0083 C      35 FORMAT('ENTER # OF CHANNELS PER SCAN')
0084 C      READ(LU,*)NCHAN
0085 C      NCHAR=(NCHAN+1)*23)
0086 C      NWORDS=(NCHAR+1)/2
0087 C      IOCBS=256
0088 C      NINTEG=NCHAN*8+6
0089 C
0090 C-----SKIP FILES
0091 C
0092 C      WRITE(LU,17)
0093 C      17 FORMAT('ENTER # OF TAPE FILES TO SKIP')
0094 C      READ(LU,*)NSKIP
0095 C      IF(NSKIP.GT.0)CALL SKIP(IANS,ITAPE,NWORDS)
0096 C
0097 C-----FILE NAME
0098 C
0099 C      WRITE(LU,20)
0100 C      20 FORMAT('ENTER A DISC FILE NAME - 6 ASCII CHARS')
0101 C      NAMCNT = NAMCNT + 1
0102 C      READ(LU,30)(NAME(I),NAMCNT),I=1,3)
0103 C      30 FORMAT(3A2)
0104 C      WRITE(LU,40)
0105 C      40 FORMAT('ENTER PREFERRED CARTRIDGE (0 IF NO PREFERENCE)')
0106 C      READ(LU,*)(ICR(NAMCNT))
0107 C
0108 C      DEFINE FILE PARAMETERS FOR EXCLUSIVE OPEN, STANDARD
0109 C      SEQUENTIAL ACCESS, WITH FILE TYPE DEFINED AT CREATION
0110 C      (OR DEFAULT TO TYPE 3)
0111 C
0112 C      ISIZE=-1
0113 C      IOPTH=0
0114 C      ITYPE = 3
0115 C      ISECU = 0
0116 C
0117 C-----CALL CREAT: CREATE DISC FILE USING INFO SUPPLIED BY USER
0118 C

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0119      CALL CREAT(IDC8,IERR,NAME(1,NANCNT),ISIZE,
0120      + ITYPE,ISECU,ICR(NANCNT),IDCB8)
0121      WRITE(LU,21)IERR
0122 21     FORMAT(/'*CREAT MESSAGE IER=',I6)
0123      IF(IERR.LT.0)CALL ERR(IERR)
0124      C
0125 C-----CALL OPEN: EXCLUSIVE OPEN, WITH STANDARDSEQUENTIAL ACCESS
0126 C      SEARCH ALL CARTRIDGES FOR FILE, RETURNING SUCCESS OF OPEN
0127 C      IN IER
0128 C
0129      CALL OPEN(IDC8,IERR,NAME(1,NANCNT),IOPTH,ISECU,ICR(NANCNT),
0130      + IDCB8)
0131      WRITE(LU,22)IERR
0132 22     FORMAT(/'*OPEN MESSAGE IER=',I3)
0133      IF(IERR.LT.0)CALL ERR(IERR)
0134      C
0135 C-----THIS LOOP WILL READ IN DATA FROM TAPE,
0136 C      TRANSFER IT TO THE DISC, AND TEST RECORD
0137 C
0138      IRNO = 0
0139      ITPNO = 8
0140      C
0141 C-----TYPE TAPE CHARACTER SET
0142 C
0143      ICHVRT=0
0144      IF (ITAPE.NE.1) GOTO 31
0145 28     WRITE(LU,29)
0146 29     FORMAT(' FOR SINGLE TAPE CHARACTER SET:'
0147      +/2X,"ENTER '0' FOR EBCIDIC "
0148      +/8X,"'1' FOR ASCII")
0149      READ(LU,*)ICHVRT
0150      IF((ICHVRT.NE.0).AND.(ICHVRT.NE.1))GOTO28
0151 31     WRITE(LU,86)
0152 86     FORMAT('**WAIT FOR TAPE READ')
0153      C
0154      C
0155      DO 97 LOOP=1,ITAPE
0156      IF(LOOP.EQ.2)ITPNO=18
0157      C
0158 C-----GET A RECORD OF SIZE IDCB8
0159 C
0160 44     CALL EXEC(1,ITPNO,IBUFR,NWORDS)
0161      C
0162 C-----CHECK IF END OF TAPE FILE
0163 C
0164      CALL EXEC(13,ITPNO,ISTAT)
0165      ISTAT = IAND(ISTAT,402048)
0166      IF(ISTAT.NE.2048)GO TO 47
0167      IF(ITAPE.EQ.1.OR.LOOP.EQ.2)GO TO 97
0168      CALL UNITF(IDC8,IERR,IBLANK,NWORDS)
0169      GO TO 97
0170      C
0171 C-----CONVERT SCAN TO ASCII
0172 C
0173 47     IF(ICHVRT.NE.0) GOTO 32
0174      CALL EBCAS(IBUFR,NWORDS)
0175 C-----CHECK IF RECORD IS A GOOD ONE
0176 C
0177 32     CALL CODE(NCHAR)
0178      READ(IBUFR,41)(ISCR(J),J=1,NINTEG)

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0179          CONTINUE
0180 41        FORMAT(13X,3(2I1,1X),20(2X,2I1,1X,6I1),1X)
0181          DO 14 K=1,NINTEG
0182            BAD=1
0183            DO 95 J=0,9
0184              IF(ISCR(K).EQ.J)BAD=0
0185 95          CONTINUE
0186 C          IF BAD=1, THROW AWAY SCAN
0187            IF(BAD.NE.1) GO TO 14
0188            WRITE(LU,50)(IBUFR(IJ),IJ=1,NWORDS)
0189 50          FORMAT('**BAD INPUT*LINE BEING DISCARDED',( ' ',249A2))
0190            GO TO 44
0191 14          CONTINUE
0192 C
0193 C
0194 C-----WRITE RECORD TO DISC FILE
0195 C
0196 60          CALL WRITF(IDCB,IERR,IBUFR,NWORDS)
0197            IF(IERR.LT. 0) CALL ERR(IERR)
0198            IRNO = IRNO + 1
0199            GO TO 44
0200 97          CONTINUE
0201 C
0202 C
0203 C-----CALL LOCF: EXECUTION OF THE NEXT STATEMENTS RELEASES THE UNUSED
0204 C      PORTION OF THE CR HELD BY THIS ROUTINE
0205 C
0206            CALL LOCF(IDCB,IERR,IREF,IRB,IOFF,JSEC)
0207            WRITE(LU,98)IERR
0208 98          FORMAT('**LOCF MESSAGE IER= ',I6)
0209            IF(IERR.LT.0)CALL ERR(IERR)
0210            ITRUN=JSEC/2-IRB-1
0211 C
0212 C-----CALL CLOSE: TRUNCATING THE UNUSED PORTION OF THE CR.
0213 C
0214            CALL CLOSE(IDCB,IERR,ITRUN)
0215            WRITE(LU,66)IERR
0216 66          FORMAT('**CLOSE MESSAGE IER= ',I6)
0217            IF(IERR.LT.0)CALL ERR(IERR)
0218 C
0219            WRITE(LU,65)IRNO,(NAME(N,NAMCNT),N=1,3)
0220 65          FORMAT('** ',I6,' RECORDS WRITTEN TO FILE ',J3A2)
0221 C
0222            WRITE(LU,70)
0223 70          FORMAT(' TRANSFER ANOTHER FILE ? (Y\N)')
0224            READ(LU,201)IANS
0225            IF(IANS.EQ.1HY)GO TO 7
0226 C
0227            GOT02
0228 200 IPAST(2)=1
0229 C-----C
0230 C      OLD MASTR C
0231 C      THIS SECTION ALLOWS THE USER TO SAVE DISC C
0232 C      FILES ONTO A MASTER TAPE. THIS MASTER TAPE C
0233 C      CAN LATER BE USED AS INPUT TO THIS PROGRAM. C
0234 C      DISC FILES NEED NOT HAVE BEEN CREATED DURING C
0235 C      THIS SCHEDULE OF BIGST. MASTER TAPE ASSUMED ASCII C
0236 C-----C
0237            IF(IPAST(1).EQ.0) GOTO 23

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0239 C
0240 WRITE(LU,3)
0241 7 FORMAT('TO TRANSFER DISC FILES MOUNT MASTER TAPE ON LU0'
0242 + ' /Y/N) AND ENTER AN INTEGER WHEN READY')
0243 READ(LU,*)IANS
0244 C
0245 C
0246 DO 101 I=1,NAMCNT
0247 C
0248 C-----PROMPT WITH NAMES OF FILES CREATED SO FAR
0249 C
0250 WRITE(LU,11)(NAME(I),I=1,3)
0251 11 FORMAT('TRANSFER FILE ',3A2,' ? (Y/N)')
0252 READ(LU,201)ANS
0253 IF(ANS.EQ.1NN) GOTO 101
0254 C
0255 C-----TRANSFER THE I' TH FILE ON THE LIST
0256 C
0257 CALL TRANS(I)
0258 C
0259 101 CONTINUE
0260 C
0261 C
0262 WRITE(LU,27)
0263 27 FORMAT('XFER A PREVIOUS FILE? (Y/N)')
0264 READ(LU,201)ANS
0265 201 FORMAT(A1)
0266 IF (ANS.NE.1NY) GOTO2
0267 C
0268 C-----TRANSFER FILES CREATED PREVIOUSLY OUTSIDE THIS SCHEDULE
0269 C FILES ARE ASSUMED ALL READY EDITED & CONVERTED
0270 C
0271 23 WRITE(LU,13)
0272 13 FORMAT(1X,'MASTER TAPE SHOULD BE ON LU 0')
0273 NAMCNT=NAMCNT+1
0274 WRITE(LU,24)
0275 24 FORMAT('ENTER FILE NAME--6 ASCII CHARACTERS')
0276 READ(LU,70)(NAME(I),I=1,3)
0277 WRITE(LU,25)
0278 25 FORMAT('ENTER CARTRIDGE #')
0279 READ(LU,*)ICR(NAMCNT)
0280 WRITE(LU,26)
0281 CALL TRANS(NAMCNT)
0282 26 FORMAT('TRANSFER ANOTHER FILE? (Y/N)')
0283 READ(LU,201)ANS
0284 IF(ANS.NE.1NN) GOTO 23
0285 C
0286 C
0287 GO TO 2
0288 300 IPAST(3)=1
0289 C-----
0290 C THIS SECTION ALLOWS THE USER TO MAKE A C
0291 C PROGA INPUT TAPE FROM DISC FILES CREATED C
0292 C DURING PAST AND CURRENT RUNS OF THE PROGRAM. C
0293 C THE USER MAY USE EITHER TAPE DRIVES FOR OUTPUT. C
0294 C THE USER MAY ALSO SIMPLY PRINT THE OUTPUT ON C
0295 C ANY TERMINAL OR PRINTER C
0296 C-----C
0297 WRITE(LU,4)
0298 4 FORMAT(' TO CREATE PROGA INPUT TAPE FROM DISC FILES: '

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0299      + /SX, 'MOUNT PROG4 TAPE ON A TAPE DRIVE 8'
0300      + /SX, 'ENTER THE LUN OF THE TAPE WHEN READY.'
0301      + /IX, 'TO LIST THE OUTPUT ELSEWHERE!'
0302      + /SX, 'ENTER THE LU NUMBER WHEN READY.'
0303      READ(LU,*)IOUTDV
0304      C
0305      IF((IPAST(1).EQ.0).AND.(IPAST(2).EQ.0)) GOTO 19
0306      39 DO 103 I=1,NAMCNT
0307      C
0308      C-----PROMPT WITH NAMES OF FILES CREATED SO FAR
0309      C
0310      WRITE(LU,6)(NAME(II,I),II=1,3)
0311      6   FORMAT('TRANSFER FILE ',3A2,' ? (Y\N)')
0312      READ(LU,201)ANS
0313      IF(ANS.EQ.1NN) GO TO 103
0314      C
0315      C-----WRITE OUT THE I'TH FILE ON THE LIST
0316      C
0317      CALL OUTPR(I,IOUTDV)
0318      C
0319      C-----OPEN & THEN PURGE THIS DISC FILE
0320      C
0321      CALL OPEN(IDC8,IERR,NAME(1,I),0,0,ICR(I))
0322      IF(IERR.LT.0)CALL ERR(IERR)
0323      CALL PURGE(IDC8,IERR,NAME(1,I),0,ICR(I))
0324      IF(IERR.LT.0) CALL ERR(IERR)
0325      C
0326      103 CONTINUE
0327      C
0328      C-----TRANSFER FILES WHICH WERE NOT CREATED DURING THIS
0329      C      SCHEDULE
0330      C
0331      19  NAMCNT=0
0332      WRITE(LU,34)
0333      34  FORMAT('TRANSFER PREVIOUSLY CREATED FILE? (Y\N)')
0334      READ(LU,201)ANS
0335      IF(ANS.EQ.1NN) GOTO 36
0336      NAMCNT=NAMCNT+1
0337      WRITE(LU,37)
0338      37  FORMAT('ENTER FILE NAME--6 ASCII CHARACTERS')
0339      READ(LU,30)(NAME(II,NAMCNT),II=1,3)
0340      WRITE(LU,38)
0341      38  FORMAT('ENTER CARTRIDGE #')
0342      READ(LU,*) (ICR(NAMCNT))
0343      GOTO 39
0344      C
0345      C
0346      36  IF ((IOUTDV.NE.8).AND.(IOUTDV.NE.18)) GOTO 2
0347      C
0348      C-----WRITE OUT 'END OF TAPE' MARK (WILL BE USED BY PROG4).
0349      C
0350      WRITE(IOUTDV,75)
0351      ENDFILE IOUTDV
0352      CALL EXEC(3,10,IOUTDV)
0353      75  FORMAT('XXXX')
0354      C
0355      GOTO 2
0356      C
0357      C
0358      C-----

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0359 C          END PROGRAM                                     C
0360 C-----C
0361 400 WRITE(LU,401)
0362 401 FORMAT('END OF BIGST')
0363 STOP
0364 END
0365 C
0366 C
0367 C-----C
0368 SUBROUTINE OUTPR(NUN,IOUTDV)
0369 C
0370 C THIS SUBROUTINE TRANSFERS THE NUN'TH FILE ON THE LIST
0371 C TO THE OUTPUT MEDIUM.
0372 C
0373 C
0374 C COMMON LU(5),NAME(3,20),NANCNT,ICR(20),IPAST(3)
0375 C INTEGER MTIME,NTIME,STIME,ICHAR(550),ICHAN(20)
0376 C INTEGER IDCB(272),ITITLE(40),KCHAN(20)
0377 C INTEGER IPON(20)
0378 C REAL STORE(20),OUT(20)
0379 C DATA IBLANK/384*2H /,IDCBS/256/
0380 C
0381 C INITIALIZE ARRAYS
0382 C
0383 DO 2 I = 1, 40
0384 2 ITITLE(I) = IBLANK
0385 C
0386 C OPEN THE FILE
0387 C
0388 CALL OPEN(IDCB,IERR,NAME(1,NUN),0.0,ICR(NUN),IDCBS)
0389 IF(IERR.LT.0) CALL ERR(IERR)
0390 C
0391 C GET INFORMATION ABOUT THE LOGGERS
0392 C
0393 9 WRITE(LU,10)
0394 10 FORMAT(' ENTER # OF CHANNELS, & CHANNEL #S (12)')
0395 READ(LU,3)NCHAN,(ICHAN(I),I=1,NCHAN)
0396 NCHAN=NCHAN+11+23
0397 3 FORMAT(21(I2,1X))
0398 IF(NCHAN.GT.20) GO TO 9
0399 C
0400 DO 4 I = 1, 20
0401 4 OUT(I) = 0.0
0402 C
0403 41 WRITE(LU,15)
0404 15 FORMAT('ENTER TITLE FOR THIS FILE (UP TO 60 CHARS)')
0405 READ(LU,20) (ITITLE(I), I = 1, 40)
0406 20 FORMAT(40A2)
0407 C
0408 C WRITE OUT THE HEADER TO OUTPUT LU
0409 C
0410 WRITE(IOUTDV,25) (ITITLE(I), I = 1, 40)
0411 WRITE(IOUTDV,30)(ICHAN(I),I=1,NCHAN)
0412 WRITE(IOUTDV,35)
0413 25 FORMAT(1X,40A2)
0414 30 FORMAT('0 CHANNELS ',20(7X,I2))
0415 35 FORMAT('0 TIME')
0416 C
0417 C READ A RECORD
0418 C

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0419 37 CALL READF(IDC8,IERR,ICAR,550,LEN)
0420 IF(IERR.LT.0)CALL ERR(IERR)
0421 IF(LEN.EQ.-1)GO TO 70
0422 C
0423 IF(ICAR.NE.IBLANK)GO TO 39
0424 C
0425 C WRITE(IOUTDV,75)
0426 C WRITE(LU,38)
0427 C38 FORMAT('SECOND GROUP OF CHANNELS WILL BE'
0428 C 1 ' PROCESSED NOW.'/'FOR SECOND GROUP OF'
0429 C 2 ' CHANNELS, PLEASE')
0430 C GO TO 9
0431 C
0432 C CONVERT ASCII STRING TO INTEGERS AND REALS
0433 C
0434 39 CONTINUE
0435 CALL CODE(2*LEN)
0436 READ(ICAR,40)NTIME,MTIME,STIME,(KCHAN(I),STORE(I),
0437 I IPOM(I), I = 1, NCHAN)
0438 40 FORMAT(13X,3(I2,1X),20(2X,I2,1X,F5.5,I1),1X)
0439 C
0440 C MULTIPLY BY APPROPRIATE POWER OF 10
0441 C
0442 DO 50 I = 1, NCHAN
0443 50 STORE(I) = STORE(I)*(10.0**((3-IPOM(I))))
0444 C
0445 C WRITE DATA OUT TO RIGHT LU
0446 C
0447 WRITE(IOUTDV,66)NTIME,MTIME,STIME,(STORE(JK), JK = 1, NCHAN)
0448 66 FORMAT(1H,2X,I2,' ',I2,' ',I2,20(3X,F7.1))
0449 C
0450 C
0451 70 WRITE(IOUTDV,75)
0452 75 FORMAT(1H1,110X)
0453 C
0454 CALL CLOSE(IDC8,IERR)
0455 IF(IERR.LT.0)CALL ERR(IERR)
0456 C
0457 RETURN
0458 END
0459 C*****C
0460 SUBROUTINE SKIP(NUM,ITAPE,MWDS)
0461 INTEGER NUM,ITAPE,IBUFR(384)
0462 C
0463 ITPNO = 8
0464 C
0465 DO 100 I = 1, ITAPE
0466 IF(I.EQ.2)ITPNO = 18
0467 DO 50 J = 1, NUM
0468 25 REG = EXEC(1,ITPNO,IBUFR,MWDS)
0469 REG = EXEC(13,ITPNO,ISTAT)
0470 ISTAT = IAND(ISTAT,040200B)
0471 IF(ISTAT.EQ.0) GO TO 25
0472 50 CONTINUE
0473 100 CONTINUE
0474 C
0475 RETURN
0476 END
0477 C*****C
0478 SUBROUTINE ERR(IERR)

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0479 C
0480 C   THIS SUBROUTINE PRINTS THE ERROR CODE PASSED TO IT
0481 C
0482 COMMON LU(5),NAME(3,20),NANCT,ICR(20),IPAST(3)
0483 INTEGER ANS
0484 WRITE(LU,10)IERR
0485 10  FORMAT(' IERR = ',16,'ABORT PROGRAM? (Y/N)')
0486 READ(LU,201) ANS
0487 201  FORMAT(A1)
0488 IF(ANS.NE.1NY) RETURN
0489 STOP
0490 END
0491 C
0492 C*****
0493 SUBROUTINE TRANS(NUM)
0494 C
0495 C   THIS SUBROUTINE TRANSFERS THE N'TH FILE ON THE
0496 C   LIST TO THE MASTER TAPE
0497 C
0498 DIMENSION IDCB(272),IBUFR(272),ISCR(166)
0499 COMMON LU(5),NAME(3,20),NANCT,ICR(20),IPAST(3)
0500 C
0501 C   OPEN THE FILE
0502 C
0503 CALL OPEN(IDCB,IERR,NAME(1,NUM),IDUM,IDUM,ICR(NUM),256)
0504 IF(IERR.LT.0) CALL ERR(IERR)
0505 C
0506 C   READ A RECORD
0507 C
0508 5  CALL READF(IDCB,IERR,IBUFR,256,LEN)
0509 IF(IERR.LT.0)CALL ERR(IERR)
0510 IF(LEN.LT.0) GOTO 50
0511 C
0512 C   CHECK IF RECORD IS GOOD
0513 C
0514 NCHAN=(LEN-23)/11
0515 NINTEG=NCHAN*8+6
0516 CALL CODE(LEN)
0517 READ(IBUFR,41)(ISCR(J),J=1,NINTEG)
0518 41  FORMAT(13X,3(2I1,1X),20(2X,2I1,1X,6I1),1X)
0519 DO 14 K=1,NINTEG
0520 IBAD=1
0521 DO 95 I=0,9
0522 IF(ISCR(K).EQ.I) IBAD=0
0523 95  CONTINUE
0524 IF (IBAD.EQ.1) GO TO 5
0525 14  CONTINUE
0526 C
0527 C   WRITE IT OUT
0528 C
0529 REC=EXEC(2,0,IBUFR,LEN)
0530 GOTO 5
0531 C
0532 C   WRITE EOF ON TAPE & AND CLOSE THE DISC FILE
0533 C
0534 50  REC=EXEC(3,01100)
0535 CALL CLOSE(IDCB)
0536 RETURN
0537 END
0538 C*****

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0539      SUBROUTINE EDCAS(ICAR,LEN)
0540      C
0541      C      THIS SUBROUTINE CONVERTS A BUFFER OF EDCIDIC
0542      C      CHARACTERS ( CONTAINED IN AN INTEGER ARRAY),
0543      C      FROM THE DATA LOGGER, INTO ASCII.
0544      C
0545      C      DIMENSION ICAR(550)
0546      C      INTEGER RCHAR,LCHAR
0547      C
0548      C
0549      C      DO 100 I = 1 , LEN
0550      C
0551      C          GET RIGHT BYTE & CONVERT IT
0552      C
0553      C          RCHAR = IAND(ICAR(I),077B)
0554      C          IF(RCHAR.EQ.0400)RCHAR = 055B
0555      C          IF(RCHAR.EQ.0)RCHAR = 040B
0556      C
0557      C          GET LEFT BYTE & CONVERT IT
0558      C
0559      C          LCHAR = IAND(ICAR(I),037400B)
0560      C          IF(LCHAR.EQ.020000B)LCHAR = 026400B
0561      C          IF(LCHAR.EQ.0)LCHAR = 020000B
0562      C
0563      C          PACK THE TWO BYTES BACK TOGETHER AGAIN
0564      C
0565      C          ICAR(I) = IOR(LCHAR , RCHAR)
0566      C
0567      C      100 CONTINUE
0568      C
0569      C      RETURN
0570      C
0571      C *****
0572      C      END

```



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SPRODF T=00003 IS ON CR00036 USING 00074 BLKS R=0000

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0001 FTM4
0002 C NOTE!! THIS IS A MODIFIED FORM OF PRODA TO HANDLE LONGER DUMP TIME
0003 C IT SHOULD BE USED WITH &CINFF AND &CINSF.
0004 C
0005 C THIS IS THE FIRST OF THREE PROGRAM FOR REDUCING
0006 C EXPERIMENTAL DATA. INPUT IS ON TAPE UNIT 18.
0007 C OUTPUT IS TO A DISK FILE. SOME OUTPUT IS ALSO
0008 C SENT TO THE LINE PRINTER AND TAPE UNIT 8
0009 C SIMULTANEOUSLY. THIS PROGRAM'S OUTPUT (DISK FILE)
0010 C IS USED AS INPUT TO CINFER.
0011 C THIS PROGRAM IS CONSTRUCTED TO HANDLE A MAXIMUM OF 20
0012 C CHANNELS WITH A TOTAL OF 350 SCANS OF DATA PER CHANNEL.
0013 C THIS IS AVERAGED DATA SO IT CORRESPONDS TO 350 SECONDS.
0014 C IN ORDER TO PUT THE FULL 350 SCANS INTO THE OUTPUT DISC FILE,
0015 C THE VARIABLE NTH MUST BE CHANGED(SEE LINE 725).
0016 C
0017 C NOTE!!!! THIS PROGRAM HAS TO BE MODIFIED DEPENDING WHETHER THE
0018 C DATA IS FROM THE 200 OR 10000 CU FT CHAMBER. SEE LINES
0019 C 296, 301 AND 306. THE LOGIC FUNCTION SWITCH, CHANNEL
0020 C 63 IS DIFFERENT, LINE 306. THE PRESSURE TRANSDUCERS
0021 C OUTPUT IS DIFFERENT IN THE TWO CHAMBERS.
0022 C
0023 C THE CONSTANTS FOR NOZZLE DIAMETER AND CHAMBER VOLUME
0024 C AN AND VT RESPECTIVELY MUST BE MODIFIED.
0025 C
0026 C DOCUMENTED BY ALAN BRODER 3/3/80
0027 C COMMENTED BY ANDREA HUNTER 7-30-80
0028 C MODIFIED BY FRED W WILLIAMS 810408
0029 C
0030 C PROGRAM PRODF
0031 C DOUBLE PRECISION AC
0032 C REAL NT1,NT2,N7(350)
0033 C INTEGER AK2(140)
0034 C DIMENSION AK(70),IBUF(144),NAME(3),ISIZE(2),X(350,20)
0035 C INTEGER AC(5),IOBUF(100)
0036 C DIMENSION A(40),NC(20),X1(20),X2(20),IS(50
0037 C 10),XT(20),NCT(20)
0038 C LOGICAL F,FLAG,F2
0039 C COMMON IPAR(5)
0040 C EQUIVALENCE (AK2,AK)
0041 C DATA XES/4HXXXX/
0042 C DATA IBLANK/2H /
0043 C
0044 C *****
0045 C* VARIABLE DEFINITIONS
0046 C* A-TITLE OF FILE
0047 C* AC-'CHANNEL'
0048 C* IS-FUNCTION SWITCH
0049 C* NAME-UNIQUE NAME ISSUED TO OUTPUT FILE
0050 C* NC-CHANNEL NUMBERS
0051 C* NT-TIMES FOR EACH SCAN
0052 C* NT1-BEGINNING TIME OF RUN
0053 C* NT2-TIME OF CURRENT SCAN
0054 C* X,X1,X2-DATA PER SCAN
0055 C*
0056 C*****
0057 C
0058 C

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0059      IOUT=8
0060 C
0061 C
0062 C
0063 C READ IN AND WRITE OUT FILE LABEL AND CHANNEL NUMBERS
0064 C
0065      CALL RMPAR(IPAR)
0066      WRITE(IPAR(1),1000)
0067 1000  FORMAT('GIVE CARTRIDGE #, OUTPUT FILE NAME
0068      1,'(15,H6))
0069      READ(IPAR(1),1002)ICR,NAME
0070 1002  FORMAT(15,1X,3W2)
0071      ISIZE(1) = -1
0072      ITYPE = 3
0073 C
0074 C CREATE A DISK FILE
0075 C
0076      CALL CREAT(IBUF,IERR,NAME,ISIZE,ITYPE,IDUM,ICR)
0077      IF(IERR.LE.0)CALL ERR(IERR,37)
0078      CALL OPEN(IBUF,IERR,NAME)
0079 1005  READ(18,1)(A(I),I=1,20)
0080 C
0081 C CHECK IF WE HAVE REACHED THE END OF FILE
0082 C
0083      IF(A(1) EQ XES)GO TO 9090
0084 1      FORMAT(20A4)
0085      READ(18,2)AC,(X1(I),I=1,10)
0086 2      FORMAT(1X,5A2,10F10.1)
0087      DO 3 I=1,10
0088 3      NC(I)=X1(I)
0089 C      WRITE(IOUT,4)(A(I),I=1,20),AC,(NC(I),I=1,10)
0090 4      FORMAT(1H1,20A4//1H,5A2,10F10/11H I TIME)
0091 C
0092 C SKIP A LINE OF INPUT
0093 C
0094      READ(18,55)CAR1,CAR2,CAR3
0095 55     FORMAT(3A4)
0096 C
0097 C READ IN TIME AND 1ST 10 COLUMNS OF DATA FOR THAT TIME
0098 C
0099      READ(18,5)MH,AM,NH,AM,MS,(X1(I),I=1,10)
0100 5      FORMAT(1X,14,A1,I2,A1,I2,10F10.1)
0101 C
0102 C CONVERT TIME TO TIME IN SECONDS
0103 C
0104      NT1=MS+MH*60 +NH*3600.
0105 C
0106 C F WILL BE SET WHEN THERE IS NO DATA LEFT
0107 C
0108      F= .FALSE.
0109 C
0110 C J WILL POINT TO CURRENT LINE OF DATA IN THE X ARRAY
0111 C
0112      J=0
0113 C
0114 C READ IN DATA, CONVERT TIME TO SECONDS
0115 C
0116 6      READ(18,5)MH,AM,NH,AM,MS,(X2(I),I=1,10)
0117      NT2=MS+MH*60. +NH*3600.
0118      IF(NT2 EQ 0.0)F= .TRUE.

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0119 C
0120 C IF BAD DATA GO BACK FOR MORE
0121 C
0122 C IF(NT2.GT.NT1+2.OR.(NT2.LT.NT1 AND .NOT.F))GO TO 6
0123 C
0124 C GO TO 8 IF YOU HAVE TO INTERPOLATE
0125 C
0126 C IF(NT2.NE.NT1)GO TO 8
0127 C
0128 C AVERAGE DATA AND GO BACK FOR NEXT LINE IF NOT EOF
0129 C
0130 C DO 7 I=1,10
0131 7 X1(I)=0.5*(X1(I)+X2(I))
0132 C IF(F)GO TO 100
0133 C GO TO 6
0134 C
0135 C STORE GOOD LINE OF DATA IN X ARRAY,CREATE NEXT GOOD LINE,
0136 C (INTERPOLATING IF NECESSARY), WRITE OUT LINE JUST STORED
0137 C IN X ARRAY THIS IS DATA ONLY, TIME IS STORED IN NT.
0138 C
0139 8 J=J+1
0140 C NT(J)=NT1
0141 C
0142 C DT=DIFFERENCE IN BEGINNING TIME AND CURRENT SCAN TIME
0143 C
0144 C DT=NT2-NT1
0145 C DO 9 I=1,10
0146 C X(J,I)=X1(I)
0147 9 X1(I)=X1(I)+(X2(I)-X1(I))/DT
0148 C NT1=NT1+1
0149 C WRITE(IOUT,10)J,NT(J),(X(J,I),I=1,10)
0150 10 FORMAT(1H,13,F7.0,10F6.1)
0151 C IF(NT2.GT.NT1)GO TO 8
0152 C IF(F)GO TO 100
0153 C GO TO 6
0154 C
0155 C NJ WILL POINT TO BOTTOM OF DATA IN X ARRAY
0156 C
0157 100 NJ=J
0158 C
0159 C NOW DO SAME THINGS TO 2ND 10 COLUMNS OF DATA FOR
0160 C THE SAME TIMES.
0161 C
0162 C READ(10,1)(A(I),I=21,40)
0163 C READ(10,2)AC,(X1(I),I=11,20)
0164 C DO 101 I=11,20
0165 101 NC(I)=X1(I)
0166 C WRITE(IOUT,4)(A(I),I=21,40),AC,(NC(I),I=11,20)
0167 C
0168 C SKIP A LINE OF INPUT
0169 C
0170 C READ(10,55)CAR1,CAR2,CAR3
0171 C
0172 C READ IN TIME AND 2ND 10 COLUMNS OF DATA FOR THAT TIME
0173 C
0174 102 READ(10,5)MH,MH,AN,MH,AN,MS,(X1(I),I=11,20)
0175 C
0176 C CONVERT TIME TO TIME IN SECONDS
0177 C
0178 C NT1=MS+MH*60.+MH*3600.

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0179          IF(NT1.LT.NT(1))GO TO 102
0180 C
0181 C      F WILL BE SET WHEN THERE IS NO DATA LEFT ALSO F2
0182 C      F=.FALSE.
0183 C      F2 = .FALSE.
0184 C      J=NT1-NT(1)
0185 C      NJ0=J+1
0186 C
0187 C      READ IN DATA , CONVERT TIME TO SECONDS
0188 C
0189 C      103 READ(18,5)MH,AM,MN,AM,MS,(X2(I),I=11,20)
0190 C      NT2=MS+MM*60.+MH*3600.
0191 C      IF(NT2.GT.NT1+2)GO TO 103
0192 C      IF(NT2.EQ.0)F2=.TRUE.
0193 C
0194 C      GO TO 105 IF YOU HAVE TO INTERPOLATE
0195 C
0196 C      IF(NT2.NE.NT1)GO TO 105
0197 C
0198 C      AVERAGE DATA AND GO BACK FOR NEXT LINE IF NOT EOF
0199 C
0200 C      DO 104 I=11,20
0201 C      104 X1(I)=0.5*(X1(I)+X2(I))
0202 C      GO TO 103
0203 C
0204 C      STORE GOOD LINE OF DATA IN X ARRAY, CREATE NEXT GOOD LINE,
0205 C      (INTERPOLATING IF NECESSARY), WRITE OUT LINE JUST STORED
0206 C      IN X ARRAY.
0207 C
0208 C      105 J=J+1
0209 C      IF(J.GT.NJ)F=.TRUE.
0210 C      NT(J)=NT1
0211 C      DT=NT2-NT1
0212 C      DO 106 I=11,20
0213 C      X(J,I)=X1(I)
0214 C      106 X1(I)=X1(I)+(X2(I)-X1(I))/DT
0215 C      NT1=NT1+1
0216 C      WRITE(IOUT,10)J,NT(J),(X(J,I),I=11,20)
0217 C      IF(NT2.GT.NT1)GO TO 105
0218 C      IF(.NOT.(F.OR.F2))GO TO 103
0219 C      IF(F2)GO TO 108
0220 C      107 READ(18,5)MH,AM,MN,AM,MS
0221 C      IF(MH.NE.0.OR.MM.NE.0.OR.MS.NE.0)GO TO 107
0222 C
0223 C      NJM WILL NOW POINT TO BOTTOM OF LAST COMPLETE SET OF DATA
0224 C      (COMPLETE = ALL 20 COLUMNS OF DATA). IT IS DETERMINED WHETHER CHANNELS
0225 C      60-69 OR 70-79 HAS THE LEAST NUMBER OF SCANS AND IS RETURNED TO NJM.
0226 C
0227 C      108 NJM=NJ
0228 C      IF(J.LT.NJ)NJM=J
0229 C
0230 C      PRINT OUT HEADINGS AND COLUMN HEADINGS WITH
0231 C      CHANNEL NUMBERS REARRANGED.
0232 C
0233 C *****
0234 C THIS IS THE ARRANGEMENT OF CHANNEL NUMBERS IN ONE ARRAY, THE *
0235 C SECOND ARRAY CONTAINS THE CHANNEL NUMBERS REARRANGED IN A *
0236 C PRE-DETERMINED ORDER. *
0237 C ----- *
0238 C DEFINITION OF HEADERS *

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0239 C* CHANNEL NUMBERS-CHANNELS 60-79
0240 C* ARRAY #1-(NC) THE ORIGINAL ORDER OF CHANNEL NUMBERS IN
0241 C* ASCENDING ORDER
0242 C* ARRAY #2-(NCT) ALTERED ORDER OF CHANNEL NUMBERS
0243 C* LOCATION- THE POSITION OF PURPOSE OF CHANNEL NUMBERS
0244 C* -----
0245 C* -----
0246 C* ARRAY #1      CHANNEL NUMBER      ARRAY #2      LOCATION
0247 C* -----
0248 C*      NC(1)          60          NCT(1)      PRESSURE
0249 C*      NC(2)          61          NCT(3)      PRESSURE
0250 C*      NC(3)          62          NCT(10)     TEMPERATURE(C)
0251 C*      NC(4)          63          *          FUNCTION
0252 C*      NC(5)          64          NCT(16)     TEMPERATURE(C)
0253 C*      NC(6)          65          NCT(15)     TEMPERATURE(C)
0254 C*      NC(7)          66          NCT(14)     TEMPERATURE(C)
0255 C*      NC(8)          67          NCT(13)     TEMPERATURE(C)
0256 C*      NC(9)          68          NCT(12)     TEMPERATURE(C)
0257 C*      NC(10)         69          NCT(11)     TEMPERATURE(C)
0258 C*      NC(11)         70          NCT(2)      NOZZLE ENTRANCE
0259 C*      NC(12)         71          NCT(6)      TEMPERATURE(C)
0260 C*      NC(13)         72          *          TANK 1 EXIT
0261 C
0262 C*      NC(14)         73          *          NOZZLE THROAT
0263 C*      NC(15)         74          NCT(7)      TEMPERATURE(C)
0264 C*      NC(16)         75          NCT(5)      TEMPERATURE(C)
0265 C*      NC(17)         76          NCT(8)      TEMPERATURE(C)
0266 C*      NC(18)         77          NCT(4)      TEMPERATURE(C)
0267 C*      NC(19)         78          NCT(9)      TEMPERATURE(C)
0268 C*      NC(20)         79          *          TANK 1
0269 C* -----
0270 C* NOTE: *****
0271 C* (*) INDICATES NO CORRESPONDENCE TO THIS LOCATION
0272 C* -----
0273 C* -----
0274 C
0275 C      NCT(1)=NC(1)
0276 C      NCT(2)=NC(11)
0277 C      NCT(3)=NC(2)
0278 C      NCT(4)=NC(18)
0279 C      NCT(5)=NC(16)
0280 C      NCT(6)=NC(12)
0281 C      NCT(7)=NC(15)
0282 C      NCT(8)=NC(17)
0283 C      NCT(9)=NC(19)
0284 C      NCT(10)=NC(3)
0285 C      NCT(11)=NC(10)
0286 C      NCT(12)=NC(9)
0287 C      NCT(13)=NC(8)
0288 C      NCT(14)=NC(7)
0289 C      NCT(15)=NC(6)
0290 C      NCT(16)=NC(5)
0291 C      WRITE(IOUT,200)(A(I),I=1,20),(NCT(I),I=1,16),(I,I=1,16)
0292 C      200  FORMAT(1H1,1X,20A4/18HCHANNEL OF ORIGIN,14,15I6/1H,5XINT,9X,16I6
0293 C      1,6H VALVE/10H J TIME)
0294 C
0295 C REARRANGE THE ORDER OF THE COLUMNS OF DATA.
0296 C ALSO MOVE THE FIRST GOOD ROW OF DATA TO THE
0297 C TOP OF THE ARRAY THEN DUMP OUT DATA TO THE
0298 C LINE PRINTER (THE DO 202 LOOP SCALES

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0299 C CHANNELS 60 AND 61 AND SETS ARRAY IS(N) WHEN
0300 C THE NOZZLE IS ON.)
0301 C
0302 C
0303 C WRITE THE VALUE OF NJ0
0304 C
0305 WRITE(IPAR(1),1111)NJ0,NJM
0306 1111 FORMAT("NJ0=",I8,"NJM=",I8)
0307 DO 206 K=NJ0,NJM
0308 J=K+1-NJ0
0309 N(IJ)=NT(K)
0310 IS(J)=0
0311 DO 202 I=1,20
0312 C
0313 C CONVERT TANK 1 (CHANNEL 60) TRANSDUCER TO PASCAL'S
0314 C PER SQUARE METER PRESSURE, FOR THE 200 CU FT CHAMBER THE MULT
0315 C FACTOR IS 0.15 WHERE AS FOR THE 10,000 CU FT CHAMBER THE FACTOR
0316 C IS 0.1
0317 C
0318 IF(NC(I).EQ.60)X(K,I)=X(K,I)*0.15/14.7
0319 C
0320 C CONVERT CHAMBER(CHANNEL 61) TRANSDUCER TO PASCAL'S
0321 C PER SQUARE METER PRESSURE, FOR THE 200 CU FT CHAMBER THE MULT
0322 C FACTOR IS 0.05 WHERE AS FOR THE 10,000 CU FT CHAMBER THE FACTOR
0323 C IS 0.001
0324 C
0325 IF(NC(I).EQ.61)X(K,I)=X(K,I)*0.050/14.7
0326 C
0327 C DETERMINE IF THE FUNCTION SWITCH(CHANNEL 63) IS
0328 C ON OR OFF FOR THE 200 CU FT CHAMBER THE TRIGGER LEVEL SHOULD BE
0329 C 5.0 WHERE AS FOR THE 10,000 CU FT CHAMBER THE LEVEL IS 1000.0.
0330 C
0331 IF(NC(I).EQ.63 AND ABS(X(K,I)).GT.5.0000)IS(J)=1
0332 C
0333 C THE FIRST SUBSCRIPT OF X ARRAY J=THE NTH SCAN 0
0334 C AND THE SECOND SUBSCRIPT HOLD THE CHANNEL NUMBER
0335 C
0336 202 X(J,I)=X(K,I)
0337 XT(1)=X(J,1)
0338 XT(2)=X(J,11)
0339 XT(3)=X(J,2)
0340 XT(4)=X(J,18)
0341 XT(5)=X(J,16)
0342 XT(6)=X(J,12)
0343 XT(7)=X(J,15)
0344 XT(8)=X(J,17)
0345 XT(9)=X(J,19)
0346 XT(10)=X(J,3)
0347 XT(11)=X(J,10)
0348 XT(12)=X(J,9)
0349 XT(13)=X(J,8)
0350 XT(14)=X(J,7)
0351 XT(15)=X(J,6)
0352 XT(16)=X(J,5)
0353 DO 204 I=1,16
0354 204 X(J,I)=XT(I)
0355 C WRITE(1OUT,208)J,NT(J),(X(J,I),I=1,16),IS(J)
0356 206 CONTINUE
0357 208 FORMAT(1H,13,F7.0,6X,F6.3,F6.3,F6.3,13F6.1,16)
0358 C

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0359 C WRITE OUT NEW PAGE HEADERS, AND DUMP OUT CHART OF DATA
0360 WRITE(1007,700)(A(I),I=1,20),(I,I=1,13)
0361 700 FORMAT(1H1,20A4//7X10HPRESSURANT FILL-,5X13THERMOCOUPLES/6X12HFL
0362 1H4 - TOTAL INSTANTANEOUS LOCATION 1,7X11COORDINATES/1X4TIME,3X1
0363 2H0 5X147 2X1H1 7X2HT(DEG K) 74X16H1 8 THETA 2/1X24H(SEC)(BAR)
0364 3XDEG K) (BAR),2X1316,10X14H(M) (DEG) (M))
0365 CALL CODE
0366 C
0367 C INITIALIZE TABLE OF OUTPUT CONSTANTS
0368 C
0369 WRITE(AK2,209)
0370 209 FORMAT(10H 1 0.000 ,10H 00 -0.586,10H 2 0.000 ,10H 00 -0.293,10
0371 1H 3 0.000 ,10H 00 0.000,10H 4 0.000 ,10H 00 0.293,10H 5 0.000
0372 2 ,10H 00 0.596,10H 6 0.000 ,10H 00 0.878,10H 7 0.000 ,10H 00
0373 12,10H 8 0.000 ,10H 00 2.342,10H 9 0.000 ,10H 00 2.635,10H 1
0374 40 0.000 ,10H 00 2.928,10H 11 0.000 ,10H 00 3.220,10H 12 0.000 ,
0375 510H 00 3.513,10H 13 0.000 ,10H 00 3.806,5(4H ))
0376 DATA AC/6H *** /
0377 701 FORMAT(12,14,F6 3,F6 1,F8 3,4X,13F6 1,4X,5A4)
0378 702 FORMAT(1X 14,240,F8 3,4X,13F6 1,4X,5A4)
0379 FLAG=.TRUE.
0380 C
0381 C FIND WHERE NOZZLE WAS TURNED ON AND OFF.
0382 C KP POINTS TO ON POSITION
0383 C KP POINTS TO OFF+1 POSITION
0384 C
0385 DO 300 K=1,J
0386 IF (IS(K).EQ.1 AND FLAG)K0=K
0387 IF (IS(K).EQ.1 AND FLAG)FLAG=.FALSE.
0388 IF (IS(K).EQ.0 AND .NOT FLAG)KP=K
0389 300 IF (IS(K).EQ.0 AND .NOT FLAG)FLAG=.TRUE.
0390 T0=10
0391 TP=T0+KP-K0+1
0392 C
0393 C SHOW EVERY SECOND OF DATA TILL KP+10 SECONDS
0394 C THEN SHOW EVERY 5 SECONDS OF DATA TILL KP+60 SECONDS
0395 C THEN SHOW EVERY 10 SECONDS OF DATA PAST KP+60 SECONDS
0396 C NOTE: THIS SECTION MAY TAKE A LITTLE WORK TO GET ALL THE
0397 C SCANS OUT.
0398 C
0399 K1=K0-10
0400 K2=K1+49
0401 JMAX=NJM-K1
0402 J=K1+4
0403 D WRITE(IPAR(1),606) JMAX,KP,K0,K1,K2
0404 606 FORMAT(" JMAX=",I4,"KP=",I4,"K0=",I4,"K1=",I4,"K2=",I4)
0405 L=0
0406 710 L=L+1
0407 IF(L GT JMAX)GO TO 725
0408 J=J+1
0409 IF(J LE KP+10)GO TO 715
0410 J=J+4
0411 IF(J LE KP+60)GO TO 715
0412 J=J+5
0413 715 IF(J GT JMAX)GO TO 725
0414 ITM=NT(J)-NT(K0)
0415 ST(1)=X(J,1)
0416 ST(2)=X(J,2)+273.2
0417 ST(3)=X(J,3)
0418 GO 717 I=4,16

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```

0419 717 XT(I)=X(J,1)+273.2
0420 IF(J.LT.K0.OR.J.GT.KP+2)GO TO 720
0421 L2=5*L-4
0422 IF(L.GT.13)L2=66
0423 WRITE(IOUT,701)ITN,(XT(I),I=1,16),(AK(I),I=L2,L2+4)
0424 GO TO 710
0425 720 L2=5*L-4
0426 IF(L.GT.13)L2=66
0427 WRITE(IOUT,702)ITN,AG,AG,(XT(I),I=3,16),(AK(I),I=L2,L2+4)
0428 GO TO 710
0429 C
0430 C DUMP OUT DATA TO DISK THAT WILL BE USED AS INPUT
0431 C TO CINFER
0432 C
0433 C NOTE!! IF NTH IS SET TO JMAX ALL THE DATA THAT IS ON THE PRODA
0434 C TAPE WILL OUTPUT TO THE PRODA OUTPUT DISC FILE THE TAPE OUTPUT
0435 C REFLECTS ALL THE DATA, BUT FOR THE LONGER TIMES, NOT ALL THE DATA
0436 C IS SHOWN AS SOME SCANS ARE SKIPPED.
0437 C OTHERWISE SET NTH TO A SPECIFIC NUMBER, REMEMBER TO MODIFY THE NEXT
0438 C PROGRAM FOR THE PROPER NUMBER OF SCANS.
0439 C
0440 725 FLAG= TRUE.
0441 NTH=JMAX
0442 IF(JMAX.GE. 149) NTH=149
0443 C NTH REPRESENTS NT IN PROGRAM CINFER
0444 C NTI= NUMBER OF THERMOCOUPLES
0445 C DT= TIME SERIES NOMINAL INCREMENT (SEC)
0446 C AN= NOZZLE NOMINAL AREA(CM**2)
0447 C VT= TANK VOLUME(CM**3)
0448 C CF= FLOW COEFFICIENT (SEE NOTES IN CINFR)
0449 C GA= SPECIFIC HEAT RATIO(" " " " )
0450 C WA= MOL WT OF AIR (" " " " )
0451 C WP= MOL WT OF PRESSURANT(" " " " )
0452 C
0453 NTI=13
0454 DT=1.0
0455 AN=0.010
0456 VT=5.1
0457 CF=0.0
0458 GA=0.0
0459 WA=0.0
0460 WP=0.0
0461 NUM=40
0462 C
0463 C POSITION RECORD IN REFERENCE TO FILE
0464 C
0465 CALL WRITF(IBUF,IERR,A,NUM)
0466 IF(IERR.LT.0)CALL ERR(IERR,304)
0467 CALL CODE
0468 C
0469 C WRITE DATA TO DISK
0470 C
0471 WRITE(IOBUF,302)NTI,NTH,DT,TO,TP,AN,VT,CF,GA,WA,WP
0472 302 FORMAT(2I4,9F7.3,1H )
0473 NUM = 36
0474 CALL WRITF(IBUF,IERR,IOBUF,NUM)
0475 IF(IERR.LT.0)CALL ERR(IERR,310)
0476 C NOTE!!! THIS STATEMENT MAY STILL NEED WORK!!!!
0477 K4=NTH+K1-1
0478 DO 303 J=K1,K4

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0479      CALL CODE
0480      C
0481      C      WRITE OUT DATA TO DISK
0482      C
0483      WRITE(IOBUF,304)X(J,3),X(J,1),X(J,2),(X(J,I),I=4,16)
0484      304  FORMAT(F8.3,F7.3,14F5.1,' ')
0485      NUM = 43
0486      CALL WRITE(IOBUF,IERR,IOBUF,NUM)
0487      IF(IERR.LT.0)CALL ERR(IERR,317)
0488      303  CONTINUE
0489      C
0490      C      CHECK TO SEE IF EOF
0491      C
0492      GO TO 1005
0493      9090  DO 9091 I=1,100
0494      C
0495      C      WRITE OUT A LINE OF BLANKS
0496      C
0497      9091  IOBUF(I)=IDBLANK
0498      C
0499      C      LOOKING FOR THE EOF MARKER
0500      C
0501      CALL WRITE(IOBUF,IERR,XES,2)
0502      IF(IERR.LT.0)CALL ERR(IERR,323)
0503      DO 9092 I=1,4
0504      CALL WRITE(IOBUF,IERR,IOBUF,100)
0505      9092  IF(IERR.LT.0)CALL ERR(IERR,326)
0506      C
0507      C      DETERMINE THE ACTUAL LOCATION OF THE RECORD POINTER
0508      C
0509      CALL LOC(IOBUF,IERR,IDUM,IRB,IDUM,JSEC)
0510      IF(IERR.LT.0)CALL ERR(IERR,328)
0511      ITRUN = JSEC/2 - (IRB + 1)
0512      C
0513      C      CLOSE THE DISK FILE
0514      C
0515      CALL CLOSE(IOBUF,IERR,ITRUN)
0516      IF(IERR.LT.0)CALL ERR(IERR,331)
0517      C
0518      WRITE(IPAR(1),2000)NAME
0519      2000  FORMAT ('AT THIS POINT PRODA IS FINISHED WITH ',3A2)
0520      STOP
0521      1919  FORMAT ('DANGER IERR=',I6)
0522      END
0523      C
0524      C*****
0525      C      SUBROUTINE TO PRINT OUT FMP ERRORS AS THEY OCCUR
0526      C      FMP ERROR DESCRIPTIONS ARE LOCATED IN
0527      C      'APE 40 PROGRAMMER'S PET SPOOLING MANUAL'
0528      C
0529      SUBROUTINE ERR(IER,LINE)
0530      COMMON IPAR(5)
0531      WRITE (IPAR(1),9999)IER,LINE
0532      9999  FORMAT ('IER=',I8,'LINE NUMBER =',I8)
0533      RETURN
0534      END
0535      C*****
0536      ENDS
0537

```

## **APPENDIX B**

**Program CINFR accepts data from PRODF and produces the B-tables [6].**

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&CINFF 7=00004 IS ON CR00056 USING 00062 BLKS R=0000

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0001 FTH4
0002 PROGRAM CINFR
0003 C
0004 C NOTE!!! THIS IS A MODIFIED FORM OF CINFR TO HANDLE LONGER DUMP TI
0005 C IT SHOULD BE USED WITH &PRODF AND &CINSF.
0006 C THIS PROGRAM IS THE SECOND OF THREE IN THE SERIES OF DATA
0007 C REDUCING PROGRAMS. INPUT IS THE OUTPUT DISC FILE
0008 C FROM PROGRAM PRODA AND OUTPUT IS TO A DISC FILE.
0009 C
0010 C IF THE NUMBER OF INPUT SCANS FOR THIS PROGRAM CHANGES, THE FOLLO
0011 C BUFFERS MUST BE REVISED, TI(NTI,NT),TIN(NT),P(NT),PS(NT),TS(NT),
0012 C FLIN(NT),TB(NT),CN(NT),BTA(NT),TAIR(NT),TPRS(NT),PB(NT),BTT(NT),
0013 C
0014 C NOTE!!!! THE AREA OF THE NOZZLES MUST BE VARIED ALONG WITH THE
0015 C VOLUME OF THE CHAMBER IF IT IS CHANGED.
0016 C PROGRAM WRITTEN BY PROF R. C. CORLETT
0017 C ADAPTED FOR USE AT NRL BY ALLEN BRODER
0018 C MODIFIED AND COMMENTED BY F.W. WILLIAMS 810408
0019 C
0020 C DIMENSION TI(13,150),TIN(150),P(150),PS(150),TS(150),A(10),XP(20),
0021 C IFLIN(150),TB(150),CN(150),BTA(150),TAIR(150),TPRS(150),XPB(150),B1
0022 C 2TS(150)
0023 C INTEGER IPAR(5),IBUF(144),OBUF(144),IOBUF(100),ISIZE(2)
0024 C INTEGER NAME(3),NAME2(3)
0025 C INTEGER CBUF1(32),CBUF2(61),CBUF3(12),CBUF4(9),CBUF5(12),CBUF6(10)
0026 C LOGICAL FI
0027 C DATA XES/4HXXXX/
0028 C DATA IBLANK/2H /
0029 C
0030 C CALL RHPAR(IPAR)
0031 1011 FORMAT('O TIME TEMP(DEG C)',9X,'BETA BETA'
0032 C 1,'/TSTAR PRESSURANT FRACTION ')
0033 CC1012 FORMAT('OMAXIMUM OVERESTIMATE OF PRESSURANT FRACTION',
0034 C 1' DUE TO PLACEMENT IN INLET JET IS (TMEAN - TPRESS)/'
0035 C 2'(TAIR - TPRESS) * 3/20. ')
0036 1013 FORMAT('OCONNENCE VALVE OPENING ')
0037 1014 FORMAT(' VALVE FULLY OPEN ')
0038 1015 FORMAT(' CONNENCE VALVE CLOSURE ')
0039 1016 FORMAT(' VALVE FULLY CLOSED ')
0040 C
0041 C WRITE OUT HEADINGS TO DISC
0042 C
0043 C CALL CODE
0044 C WRITE(CBUF1,1011)
0045 CC CALL CODE
0046 CC WRITE(CBUF2,1012)
0047 C CALL CODE
0048 C WRITE(CBUF3,1013)
0049 C CALL CODE
0050 C WRITE(CBUF4,1014)
0051 C CALL CODE
0052 C WRITE(CBUF5,1015)
0053 C CALL CODE
0054 C WRITE(CBUF6,1016)
0055 C WRITE(IPAR(1),1000)
0056 C
0057 C INPUT NAME IS THE PRODA OUTPUT FILE NAME
0058 C

```

```

0059      CALL CINAV(IBUF,TBUF)
0060      C
0061      C REWIND TEMPORARY FILE SO THAT IT CAN BE USED FOR
0062      C INPUT BY CINFV
0063      C
0064      CALL RUMDF(TBUF,IERR)
0065      IF(IERR.LT.0)CALL ERR(IERR)
0066      C
0067      C CINFV IS A SUBROUTINE THAT AVERAGES THE CASES FOR THE STATISTICAL
0068      C ANALYSIS AND PERFORMS THE STATISTICS, MEAN VALUE OF ALL QUANTITIES
0069      C NORMALIZED MEAN LOCAL PRESSURANT FRACTIONS, VARIANCES OF MEAN
0070      C LOCAL PRESSURANT FRACTIONS AND DEVIATIONS OF MEAN LOCAL PRESSURANT
0071      C FRACTIONS.
0072      C
0073      CALL CINFV(TBUF,OBUF)
0074      C
0075      C DELETE TEMPORARY FILE
0076      C
0077      CALL PURGE(TBUF,IERR,THANE)
0078      IF(IERR.LT.0)CALL ERR(IERR)
0079      C
0080      C INITIALIZE AND WRITE OUT PADDING BUFFER TO END OF OUTPUT FILE
0081      C
0082      CC      TBUF(101)=13
0083      DO 5 I=1,100
0084      5      TBUF(I)=IBLANK
0085      DO 10 I=1,4
0086      CALL WRITE(OBUF,IERR,TBUF,100)
0087      10      IF(IERR.LT.0) CALL ERR(IERR)
0088      C
0089      C CLOSE AND TRUNCATE OUTPUT FILE TO CORRECT SIZE
0090      C
0091      CALL LOCF(OBUF,IERR,IDUN,IRB,IDUN,ISEC)
0092      IF(IERR.LT.0)CALL ERR(IERR)
0093      ITRUN = ISEC/2 - (IRB + 1)
0094      CALL CLOSE(OBUF,IERR,ITRUN)
0095      IF(IERR.LT.0)CALL ERR(IERR)
0096      C
0097      C WRITE OUT MESSAGE THAT CINST HAS FINISHED.
0098      C
0099      WRITE(IPAR(1),2000) ONAME
0100      2000  FORMAT(" AT THIS POINT CINST IS FINISHED WITH ",3A2)
0101      STOP
0102      END
0103      C
0104      CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
0105      C
0106      SUBROUTINE ERR(IERR,LINE)
0107      C THIS SUBROUTINE WRITES OUT THE ERROR # PASSED TO
0108      C IT, AND THEN HALTS THE PROGRAM. THESE ERRORS ARE FOR FMP
0109      C CALLS. IN SOME CASES THE LINE NUMBER IS GIVEN.
0110      C
0111      INTEGER IERR,IPAR(5)
0112      COMMON IPAR
0113      WRITE(IPAR(1),10)IERR,LINE
0114      10  FORMAT(' IERR = ',I6,' LINE NUMBER=',I8)
0115      STOP
0116      END
0117      C
0118      CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC

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0119 C
0120 SUBROUTINE CINAV(INBUF,OUTBUF)
0121 INTEGER INBUF(144),OUTBUF(144),IOBUF(100)
0122 DIMENSION D(101,25),DI(50,21)
0123 DATA IBLANK/2H /
0124 DATA NC/99/
0125 DATA IXES/2HXX/
0126 DATA ICO/2H V/
0127 C READ IN THE FIRST RECORD FROM OPEN INPUT DISC FILE
0128 C THE LARGEST INPUT RECORD IS CONTROLLED BY THE SIZE OF IOBUF,
0129 C WHICH CURRENTLY IS 100,SEE DIMENSION STATEMENT.
0130 1 CALL READF(INBUF,IERR,IOBUF)
0131 IF(IERR.LT.0)CALL ERR(IERR,1)
0132 C SET THE DATA ARRAY EQUAL TO 0'S
0133 DO 3 NTK=1,50
0134 DO 3 I=1,21
0135 DI(NTK,I)=0.0
0136 3 CONTINUE
0137 C TEST TO SEE IF YOU ARE AT THE END OF THE FILE(LOOKING FOR "XX")
0138 IF(IOBUF(1).EQ.IXES)GO TO 9090
0139 C READ THE NEXT THREE RECORDS FROM THE OPEN INPUT DISC FILE
0140 DO 101 I=1,3
0141 CALL READF(INBUF,IERR,IOBUF,101)
0142 101 IF(IERR.LT.0)CALL ERR(IERR)
0143 C READS IN 101 LINES OF DATA, STORING ONLY DATA AND DISREGUARDING
0144 C TITLE LINES. TO CHANGE THE AMOUNT OF DATA INPUT THE DIMENSION
0145 C STATEMENT D(101,25) MUST BE CHANGED ALONG WITH DO LOOP 20,30
0146 C LINE AFTER 210.
0147 DO 10 NT=1,101
0148 9 CALL READF(INBUF,IERR,IOBUF)
0149 IF (IERR.LT.0)CALL ERR(IERR,9)
0150 IF(IOBUF(1).EQ.ICO)NTC=NT-1
0151 C TEST THIRD CHARACTER TO BE A NUMBER
0152 ITEST=(IAND(IOBUF(2),177B))-600
0153 IF(ITEST.LT.0.OR.ITEST.GT.9) GOTO 9
0154 CALL CODE
0155 READ(IOBUF,110)(D(NT,I),I=1,20)
0156 D 110 WRITE(6,110)(D(NT,I),I=1,20)
0157 110 FORMAT(4F6.1,F0.1,F0.4,F12.3,F0.3,12F6.3)
0158 10 CONTINUE
0159 C
0160 C CREATE A NEW COLUMN OF DATA(25TH) WHICH IS DERIVED FROM N/HO
0161 C WHERE N=NO. OF HOLES AT TIME T AND HO= INITIAL NO. OF HOLES.
0162 C
0163 DO 20 NT=1,101
0164 D(NT,25)=1.0/(1.0-D(NT,7))
0165 20 CONTINUE
0166 C
0167 C CALCULATE TC CONSIDERING TAU 7 AND TAU 5 . NTC=9
0168 C
0169 TC=2.0/ALOG(D(NTC-2,25)/D(NTC-4,25))
0170 C CALCULATE A TAU, CREATES A NEW COLUMN OF DATA(24TH) WHICH IS TIME
0171 C NORMALIZED. IT IS NORMALIZED TO FULL VALVE CLOSURE AS 1.00.
0172 C TAU=XBAR/XBAR SUB C.
0173 C
0174 DO 30 NT=1,101
0175 D(NT,24)=D(NT,7)/D(35,7)
0176 DTC=NT-NTC-1
0177 IF(NT.GT.NTC)D(NT,24)=1.0+DTC/TC
0178 30 CONTINUE

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0179 C
0180 C  CREATES A NEW ARRAY,DI(50,21)
0181 C
0182      DO 200 I=1,20
0183          DI(1,I)=D(1,I)
0184 200  CONTINUE
0185 C
0186 C  CONSTANTS
0187 C
0188      NT=1
0189      NTK=2
0190      TAU=0.05
0191 210  NT=NT+1
0192      IF(NT.GT.101)GO TO 300
0193 215  IF(D(NT,24).LT.TAU)GO TO 210
0194 C
0195 C  SIZE OF THE TIME INCREMENT IN THE TAU TABLE.
0196 C
0197      DD24=D(NT,24)-D(NT-1,24)
0198 C
0199 C  INTERPOLATES FOR THE NEW TABLE NORMALIZED TO TAU AND
0200 C  BUILDS A NEW ARRAY, DI(50,21)
0201 C
0202      DO 220 I=1,20
0203          DI(NTK,I)=D(NT-1,I)
0204          IF(DD24.GT.0.0001)DI(NTK,I)=DI(NTK,I)+(D(NT,I)-D(NT-1,I))
0205              *(TAU-D(NT-1,24))/DD24
0206 220  CONTINUE
0207      IF(NTK.GE.50)GO TO 300
0208      NTK=NTK+1
0209      TAU=TAU+0.05
0210      GO TO 215
0211 300  TAUKN=TAU-0.05
0212  D  WRITE(6,150)TC,TAUKN,NC,NTC
0213 C  WRITE      VALUES TO THE TEMPORARY DISC FILE
0214 150  FORMAT(1H1,2F10.2,2I10,1H )
0215 C
0216 C  WRITE OUT SELECTED VALUES TO THE TEMPORARY DISC FILE,TMPBUF:
0217 C      TC=
0218 C      TAUKN=
0219 C      NC=
0220 C      NTC= SCAN WHERE THE VALVE IS FULLY CLOSED.
0221 C
0222      CALL CODE
0223      WRITE(IOBUF,150)TC,TAUKN,NC,NTC
0224      CALL WRITE(OUTBUF,IERR,IOBUF,21)
0225      IF(IERR.LT.0)CALL ERR(IERR,160)
0226 C  WRITE THE DATA TO THE TEMPORARY DISC FILE "TMPBUF"
0227      DO 310 NTK=1,50
0228          DNTK=NTK-1
0229          DI(NTK,21)=0.05*DNTK
0230 160  FORMAT(1H ,F5.1,3F6.1,F8.1,F8.4,F6.3,F8.3,12F6.3,F5.2,1H )
0231      CALL CODE
0232      WRITE(IOBUF,160)(DI(NTK,I),I=1,21)
0233      CALL WRITE(OUTBUF,IERR,IOBUF,66)
0234      IF(IERR.LT.0)CALL ERR(IERR,310)
0235 310  CONTINUE
0236 C
0237 C  PICK UP THE NEXT CASE TO PROCESS
0238 C

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0239      GO TO 1
0240      C
0241      C WRITE OUT A LINE OF BLANKS AT THE END OF TEMPORARY FILE.
0242      C
0243      9090      IOBUF(101)=13
0244              DO 9091      I=1,100
0245      9091      IOBUF(I)=IBLANK
0246              CALL WRITE(OUTBUF,IERR,IOBUF,101)
0247              IF(IERR.LT.0)CALL ERR(IERR,9091)
0248      RETURN
0249      END
0250      C
0251      CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
0252      C
0253      SUBROUTINE CINFV(INBUF,OUTBUF)
0254      INTEGER INBUF(144),OUTBUF(144),IOBUF(100),CBUF1(65),CBUF2(63)
0255      DIMENSION S1(50,21),S2(50,21),SG(50,21),DS(50,21)
0256      C
0257      C ZEROS ALL THE ARRAYS WHERE S1 WILL BE SUMS,S2 SUM OF SQUARES,SG
0258      C ,AND DS
0259      C
0260      1      DO 10 NT=1,50
0261              DO 10 I=1,21
0262                  S1(NT,I)=0.0
0263                  S2(NT,I)=0.0
0264                  SG(NT,I)=0.0
0265                  DS(NT,I)=0.0
0266      10      CONTINUE
0267      C
0268      C COUNTER FOR THE NUMBER OF CASES PROCESSED
0269      C
0270      CN=-1.0
0271      12      CN=CN+1.0
0272      C
0273      C READ IN THE FIRST LINE OF DATA FROM TEMPORARY FILE.
0274      C
0275      CALL READF(INBUF,IERR,IOBUF)
0276      IF(IERR.LT.0)CALL ERR(IERR,12)
0277      CALL CODE
0278      READ(IOBUF,100)TC,TAUN,NC
0279      100      FORMAT(2F10.2,I10)
0280      IF(NC.EQ.0)GO TO 500
0281      C
0282      C READ IN 50 LINES OF DATA FROM THE TEMPORARY FILE, WRITE THEM INTO
0283      C BUFFER SG(NT,I) AND ADD THEM TO BUFFER S1 AND STORE IN BUFFER S1.
0284      C ALSO SQUARE SG,AND ADD TO BUFFER S2 AND STORE IN S2.
0285      C
0286      DO 20 NT=1,50
0287          CALL READF(INBUF,IERR,IOBUF)
0288          IF(IERR.LT.0)CALL ERR(IERR,110)
0289          CALL CODE
0290          READ(IOBUF,110)(SG(NT,I),I=1,21)
0291      110      FORMAT(4F6.1,F8.1,F8.4,F6.3,F8.3,12F6.3,F5.2)
0292          DO 20 I=1,21
0293              S1(NT,I)=S1(NT,I)+SG(NT,I)
0294              S2(NT,I)=S2(NT,I)+SG(NT,I)**2
0295      20      CONTINUE
0296      C
0297      C REPEAT FOR ALL THE CASES IN THE TEMPORARY FILE.
0298      C

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0299      GO TO 12
0300      C
0301      C CALCULATE THE AVERAGE MEAN PRESSURANT AT THE 21ST TIME FROM
0302      C WELL AFTER VALVE CLOSURE.
0303      C
0304      500  XBARAV=S1(23,7)/CN
0305      C
0306      C CALCULATE THE AVERAGE VALUES FOR THE X NO. OF CASES FOR ARRAY S1
0307      C (SUMS), S2(SUM OF SQUARES), AND SSG(SUM OF DIFFERENCE OF SQUARES)
0308      C
0309      DO 520 NT=1,50
0310      DO 510 I=1,21
0311          S1(NT,I)=S1(NT,I)/CN
0312          S2(NT,I)=S2(NT,I)/CN
0313      C REINITIALIZE ARRAY SG
0314          SG(NT,I)=0.0
0315          SGG=S2(NT,I)-S1(NT,I)**2
0316          IF(SGG.GT.0.0)SG(NT,I)=SQRT(SGG)
0317          IF(I.GT.7.AND.I.LT.21)DS(NT,I)=S1(NT,I)-S1(NT,7)
0318          S2(NT,I)=0.0
0319          IF(I.GT.7.AND.I.LT.21)S2(NT,I)=S1(NT,I)/XBARAV
0320          DS(NT,I)=DS(NT,I)/XBARAV
0321          IF(I.GT.7.AND.I.LT.21)SG(NT,I)=SG(NT,I)/XBARAV
0322          IF(I.EQ.21)S2(NT,I)=S1(NT,I)
0323          IF(I.EQ.21)SG(NT,I)=S1(NT,I)
0324          IF(I.EQ.21)DS(NT,I)=S1(NT,I)
0325      510  CONTINUE
0326          IF(NT.GT.20.OR.NT.LT.5)GO TO 520
0327          TBAR=S1(NT,2)+273.2
0328          TO=S1(1,2)+273.2
0329          DTBAR=S1(NT,2)-S1(NT-1,2)
0330          SN=1.0/(1.0-S1(NT,7))
0331          SN1=1.0/(1.0-S1(NT-1,7))
0332          DLN=ALOG(SN/SN1)
0333          IF(DLN.LE.0.00001)GO TO 520
0334          BETA=S1(NT,5)
0335          TS=(0.4*BETA*(TBAR-TO)+TBAR+DTBAR/DLN)/1.4
0336          S2(NT,2)=TS-273.2
0337          S2(NT,6)=(S1(NT,4)-S2(NT,2))/(S1(NT,3)-S1(NT,4))/XBARAV
0338      D  WRITE(6,997)TBAR,TO,DTBAR,SN,SN1,DLN,BETA,TS
0339      D997  FORMAT(1H,3F8.1,3F8.4,2F8.1)
0340      520  CONTINUE
0341      120  FORMAT(/(1H,3F5.1,3F6.1,F8.1,F8.4,F6.3,F8.3,12F6.3,F5.2))
0342      D  WRITE(6,120)((S1(NT,I),I=1,21),NT=1,50)
0343      C
0344      C WRITE A HEADING FOR THE FIRST STAT TABLE,S1
0345      C
0346      CALL CODE
0347      WRITE(IOBUF,65)
0348      65  FORMAT('0 MEAN VALUES OF ALL QUANTITIES ',/)
0349      CALL WRITE(OUTBUF,IERR,IOBUF,17)
0350      IF(IERR.LT.0)CALL ERR(IERR,65)
0351      CALL CODE
0352      WRITE(CBUF1,1010)
0353      1010  FORMAT('0 TIME',1X,'TMP,C',1X,'TMP,C',1X,'TMP,C',3X,'BETA',
0354      1 2X,'BETA/',3X,' X ',20X,'MEAN PRESSURANT FRACTIONS AT'
0355      2  " LOCATIONS 1",22X,'TAU')
0356      CALL CODE
0357      WRITE(CBUF2,1020)
0358      1020  FORMAT(' SEC',2X,'INIT',2X," ",1X," ",.9X,'THETA',

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0359      1      3X,"BAR",6X,"1",5X,"2",5X,"3",5X,"4",5X,"5",5X,"6",
0360      2      5X,"7",5X,"8",5X,"9",5X,"10",4X,"11",4X,"12",4X,"13 " )
0361      CALL WRITE(OUTBUF,IERR,CBUF1,65)
0362      IF(IERR.LT.0) CALL ERR(IERR)
0363      CALL WRITE(OUTBUF,IERR,CBUF2,63)
0364      IF(IERR.LT.0) CALL ERR(IERR)
0365      CALL WRITE(S1,OUTBUF)
0366      C
0367      C WRITE A HEADING FOR THE SECOND STAT TABLE,S2
0368      C
0369      CALL CODE
0370      WRITE(IOBUF,70)
0371      70  FORMAT('1 NORMALIZED MEAN LOCAL'
0372      1,' PRESSURANT FRACTIONS ',/)
0373      CALL WRITE(OUTBUF,IERR,IOBUF,23)
0374      IF(IERR.LT.0)CALL ERR(IERR)
0375      CALL WRITE(S2,OUTBUF)
0376      C
0377      C WRITE A HEADING FOR THE THIRD STAT TABLE,SG
0378      C
0379      C
0380      CALL CODE
0381      WRITE(IOBUF,75)
0382      75  FORMAT('1 STANDARD DEVIATION OF MEAN LOCAL'
0383      1,' PRESSURANT FRACTIONS ',/)
0384      CALL WRITE(OUTBUF,IERR,IOBUF,29)
0385      IF(IERR.LT.0)CALL ERR(IERR)
0386      CALL WRITE(SG,OUTBUF)
0387      C
0388      C WRITE A HEADING FOR THE FORTH STAT TABLE,DS
0389      C
0390      CALL CODE
0391      WRITE(IOBUF,80)
0392      80  FORMAT('1 DEVIATIONS OF MEAN LOCAL'
0393      1,' PRESSURANT FRACTIONS ',/)
0394      CALL WRITE(OUTBUF,IERR,IOBUF,24)
0395      IF(IERR.LT.0)CALL ERR(IERR)
0396      CALL WRITE(DS,OUTBUF)
0397      C
0398      C WRITE THE MUNNER OF CASES TREATED
0399      C
0400      NCH=CN
0401      CALL CODE
0402      WRITE(IOBUF,130)NCH
0403      CALL WRITE(OUTBUF,IERR,IOBUF,5)
0404      IF(IERR.LT.0)CALL ERR(IERR)
0405      130  FORMAT('12,7N CASES ')
0406      RETURN
0407      END
0408      C
0409      CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
0410      C
0411      SUBROUTINE WRITE(CR,OUTBUF)
0412      C
0413      C THIS IS A SUBROUTINE THAT OUTPUTS THE DATA TO A DISC FILE,ONANE
0414      C FROM ACHIST FOR THE MEAN VALUES OF ALL QUANTITIES.
0415      C
0416      REAL CR(50,21)
0417      INTEGER IOBUF(100),OUTBUF(144)
0418      C

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0419      DO 20 NT=1,50
0420          CALL CODE
0421          WRITE(CBUF,120)(AR(NT,I),I=1,21)
0422      100  FORMAT(1H,1F5.1,1F6.1,F8.1,F8.4,F8.3,F8.3,12F6.3,F5.2,1H )
0423          CALL WRITE(OUTBUF,1ERR,1CBUF,66)
0424      20  IF(ERR.LT.0)CALL ERR(1ERR)
0425          RETURN
0426      END
0427
0428      C
0429      C
0430      C
0431      C
0432      C  THIS IS A SUBROUTINE THAT PUTS THE DATA TO A DISC FILE,OWNE
0433      C  FROM FIRST FOR NORMAL,14 THEN STANDARD DEVIATION AND DEVIATION
0434      C  OF MEAN
0435      C
0436          REAL AR(50,21)
0437          INTEGER IOUTBUF(100),OUTBUF(144),CBUF1(21),CBUF2(43)
0438      C
0439      C  WRITE OUT THE FILE HEADINGS
0440      C
0441          CALL CODE
0442          WRITE(CBUF1,1010)
0443      1010  FORMAT(1H,100"LOCATIONS 1")
0444          CALL CODE
0445          WRITE(CBUF2,1020)(I,I=1,13)
0446      1020  FORMAT(1H,13(2X,14)," YAU ")
0447          CALL WRITE(OUTBUF,1ERR,CBUF1,21)
0448          IF(1ERR.LT.0)CALL ERR(1ERR)
0449          CALL WRITE(OUTBUF,1ERR,CBUF2,43)
0450          IF (1ERR.LT.0) CALL ERR(1ERR)
0451      C
0452      C  WRITE OUT THE DATA TO THE DISC
0453      C
0454          DO 20 NT=1,50
0455              CALL CODE
0456              WRITE(CBUF,120)(AR(NT,I),I=1,21)
0457      120  FORMAT(2H,12F6.3,F5.2,1H )
0458              CALL WRITE(OUTBUF,1ERR,1CBUF,66)
0459              IF (1ERR.LT.0)CALL ERR(1ERR)
0460          20  CONTINUE
0461              RETURN
0462          END
0463      ENDS

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NAVAL RESEARCH LAB - WASHINGTON DC

F/G 13/12

NRL 324-CU M CHAMBER PRESSURIZATION EXPERIMENT: PRESSURANT CONC--ETC(U)

MAR 82 J P STONE, J I ALEXANDER, T T STREET

UNCLASSIFIED

NRL-8523

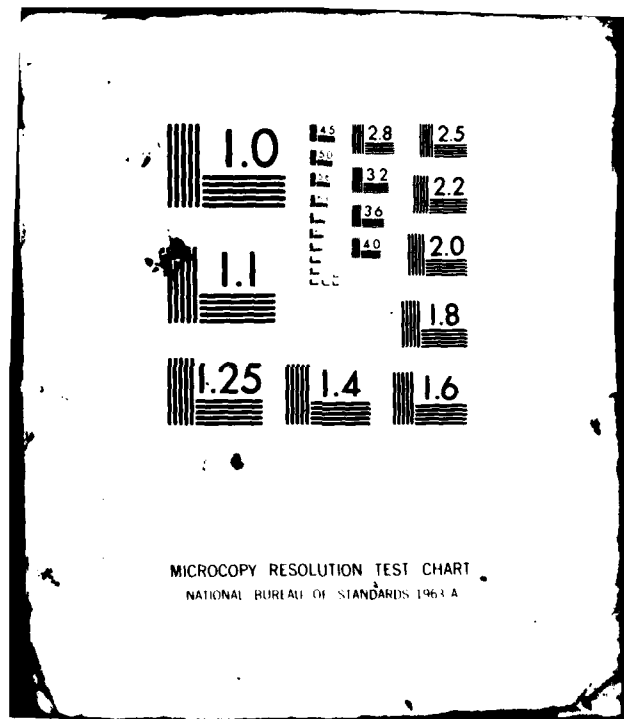
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## **APPENDIX C**

**Program CINST accepts data from CINFR and produces the C-, D-, and E-tables [6].**

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LCINBF T=00004 IS ON CR00056 USING 00060 BLKS R=0000

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0001 FTH4
0002 C
0003 C NOTE!!!! THIS IS A MODIFIED FORM OF CIN87 TO HANDLE LONGER DUMP
0004 C TIMES. IT DOES NOT CHANGE THE NONDIMENSIONAL TIME TAU AT 2.5.
0005 C PROGRAM CIN87(4.99), FNU VERSION 810213 N002
0006 C
0007 C
0008 C THIS PROGRAM DOES STATISTICS ON THE DATA FROM CINFR
0009 C THE RUNS FROM CINFR ARE GROUPED ACCORDING TO A PARTICULAR
0010 C TEST CONFIGURATION. THE INPUT DATA IS FROM DISC FILES THAT
0011 C WERE CREATED FROM CINFR. THE OUTPUT DATA FROM THIS PROGRAM
0012 C IS STORED IN DISC FILES AND MAYBE TRANSFERRED TO MAGNETIC TAPE
0013 C WITH STORE COMMANDS FROM THE FILE MANAGER.
0014 C
0015 C
0016 C THIS PROGRAM WAS WRITTEN BY PROF. R. C. CONLETT, UNIV OF
0017 C WASHINGTON, SEATTLE WASHINGTON.
0018 C THIS PROGRAM WAS ADAPTED FOR USE ON THE NRL COMPUTER, CODE
0019 C 6100 BY A. BRODER AND D. INDRITZ.
0020 C IT HAS BEEN COMMENTED BY F. W. WILLIAMS.
0021 C PROGRAM MODIFIED BY F.W.WILLIAMS 810404
0022 C
0023 C
0024 C INTEGER INAME(3), ISIZE(2), OBUF(144), IBUF(144)
0025 C INTEGER TBUF(144), ONAME(3), TNAME(3), IPAR(5)
0026 C COMMON IPAR
0027 C DATA TNAME/2HTN,2HPB,2HUF/
0028 C DATA IBLANK/2H /
0029 C CALL RNPAC(IPAR)
0030 C WRITE(IPAR,1)
0031 1 FORMAT('CARTRIDGE 0, INPUT FILE NAME '(15,A6)')
0032 C READ(IPAR,2)ICR, INAME
0033 2 FORMAT(15,1X,3A2)
0034 C WRITE(IPAR,3)
0035 3 FORMAT('CARTRIDGE 0, OUTPUT FILE NAME '(15,A6)')
0036 C READ(IPAR,2)ICR2, ONAME
0037 C ISIZE(1)=-1
0038 C ITYPE=3
0039 C
0040 C CREATE OUTPUT FILE
0041 C
0042 C CALL CREAT(OBUF, IERR, ONAME, ISIZE, ITYPE, IDUN, ICR2)
0043 C IF(IERR.LT.0)CALL ERR(IERR)
0044 C
0045 C OPEN INPUT FILE
0046 C
0047 C CALL OPEN(IBUF, IERR, INAME, IDUN, ICR)
0048 C IF(IERR.LT.0)CALL ERR(IERR)
0049 C
0050 C CREATE TEMPORARY FILE FOR S.O. INTERMEDIATE RESULTS
0051 C FROM CINAV
0052 C
0053 C CALL CREAT(TBUF, IERR, TNAME, ISIZE, ITYPE, IDUN)
0054 C IF(IERR.LT.0)CALL ERR(IERR)
0055 C
0056 C CINAV IS A SUBROUTINE WHICH INTERPOLATES THE DATA, CREATES A
0057 C NONDIMENSIONAL TIME AND NORMALIZES THE DATA TO IT.
0058 C

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0059 1000 FORMAT('GIVE CARTRIDGE #, NAME FOR INPUT FILE'
0060 1, '(15,A6)')
0061 READ(IPAR(1),1002)ICR,NAME
0062 1002 FORMAT(15,1X,3A2)
0063 WRITE(IPAR(1),1004)
0064 1004 FORMAT('GIVE CARTRIDGE #, NAME FOR OUTPUT FILE'
0065 1, '(15,A6)')
0066 READ(IPAR(1),1002)ICR2,NAME2
0067 ISIZE(1)=-1
0068 ITYPE = 3
0069 C
0070 C CREATE A DISK FILE
0071 C
0072 CALL CREAT(GBUF,IERR,NAME2,ISIZE,ITYPE,IDUM,ICR2)
0073 IF(IERR.LT.0)CALL ERR(IPAR(1),IERR)
0074 C
0075 C OPEN INPUT FILE
0076 C
0077 CALL OPEN(GBUF,IERR,NAME,IDUM,IDUM,ICR)
0078 IF(IERR.LT.0)CALL ERR(IPAR(1),IERR)
0079 C
0080 10 DO 9 I=1,100
0081 C
0082 C CONSTRUCT A LINE OF BLANKS
0083 C
0084 9 IGBUF(I) = IBLANK
0085 CALL READF(GBUF,IERR,A)
0086 IF(IERR.LT.0)CALL ERR(IPAR(1),IERR)
0087 C
0088 C CHECK FOR EOF
0089 C
0090 IF(A(1).EQ.XES)GO TO 9090
0091 CALL READF(GBUF,IERR,IOBUF)
0092 IF(IERR.LT.0) CALL ERR(IPAR(1),IERR)
0093 CALL CODE
0094 READ(IOBUF,20)NTI,NT,DT,TO,TP,AN,VT,CF,CA,UA,UP
0095 C
0096 C DESCRIPTION OF VARIABLE MEANING
0097 C
0098 C NTI= NO. OF THERMOCOUPLES, NT=NO. OF POINTS IN DATA TIME SERIES,
0099 C DT=TIME SERIES NOMINAL INCREMENT (SEC), TO AND TP RESPECTIVELY
0100 C EQUAL TIMES OF VALVE OPENING AND CLOSURE (SEC), AN=NOZZLE NOMINAL
0101 C AREA (CM**2), VT=TANK VOLUME (M**3), CF=FLOW COEFFICIENT -
0102 C IF CF IS INPUT AS ZERO AND NTI EXCEEDS 9 CF IS DEFAULT CALCULATED
0103 C USING MEAN OF TC DATA AS ESTIMATE OF MEAN TANK TEMPERATURE,
0104 C CA=SPEC. HEATS RATIO - IF INPUT AS ZERO ASSIGNED 1.4 DEFAULT,
0105 C UA=MOL. WT. OF AIR, - IF INPUT AS ZERO ASSIGNED 28.97 DEFAULT,
0106 C UP=MOL. WT. OF PRESSURANT - IF INPUT AS ZERO DEFAULT SET =UA.
0107 C
0108 20 FORMAT(214,9F7.3)
0109 C
0110 C IF THERE ARE NO THERMOCOUPLES THE PROGRAM IS FINISHED
0111 C AND A MESSAGE INDICATING COMPLETION WILL BE PRINTED
0112 C
0113 IF(NTI.GT.0.0)GO TO 20
0114 WRITE(IPAR(1),2000)NAME2
0115 2000 FORMAT ('AT THIS POINT CINFR IS FINISHED WITH ',3A2)
0116 STOP
0117 C
0118 C INITIALIZING HEAT RATIO, MOL. WEIGHT OF AIR, AND

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0119 C      NGL. WEIGHT OF PRESSURE TO DEFAULT IF APPROPRIATE
0120 C
0121 30      IF(GA.EQ.0.0)GA=1.4
0122          IF(UA.EQ.0.0)UA=20.94
0123          IF(WP.EQ.0.0)WP=UA
0124 C
0125 C      WRITES TO LINE PRINTER
0126 C
0127 0      WRITE(6,40)NTI,NT,DT,TO,TP,AN,VT,GA,UA,WP
0128 040      FORMAT(1H120X14HPROGRAM CINFER/71H0 NTI NT DT TO TP
0129 D 1      AN VT GA UA WP/1H 14,15,F7.3,7F8.3)
0130 C
0131 C      IF NUMBER OF THERMOCOUPLES ARE LESS OR EQUAL TO 5
0132 C      OR IF FLOW COEFFICIENT EQUALS 0, PRINT MESSAGE INDICATING
0133 C      SO AND ALSO PRINT A MESSAGE INDICATING PROGRAM IS
0134 C      COMPLETED.
0135 C
0136          IF(NTI.GT.5.OR.CF.NE.0.0)GO TO 60
0137          WRITE(IPAR(1),50)
0138 50      FORMAT(20HNO FLOW COEFFICIENT)
0139          WRITE(IPAR(1),2000)NAME2
0140          STOP
0141 C
0142 C
0143 C      PRINT OUT FLOW COEFFICIENT IF ANY
0144 C
0145 60      IF(CF.NE.0.0)WRITE(IPAR(1),70)CF
0146 70      FORMAT(20HFLOW COEF. INPUT ASF7.4)
0147 C
0148 C      PRINT OUT NUMBERS UP TO THE TOTAL NUMBER OF
0149 C      THERMOCOUPLES
0150 C
0151 0      WRITE(6,80) (I,I=1,NTI)
0152 040      FORMAT(21HORAN TIME SERIES DATA/30H TIME P PS TS TI/
0153 D 11H ,26X2HI=11,815/1H ,129,815)
0154          DO 100 J=1,NT
0155              RJ=J-1
0156              TIM(J)=RJ*DT
0157 C
0158 C      MUST BE NATED TO NRL DATA RECORD.
0159 C
0160          CALL READF(IOBUF,IERR,IOBUF)
0161          IF(IERR.LT.0) CALL ERR(IPAR(1),IERR)
0162          CALL CODE
0163          READ(IOBUF,90)P(J),PS(J),TS(J),(TI(I,J),I=1,NTI)
0164 90      FORMAT(F8.3,F7.3,14F5.1)
0165 C
0166 C      DESCRIPTION OF VARIABLES
0167 C      TIM=TIME(SEC), P=TANK PRESS. (ATM), PS=NOZZLE PRESS. (ATM),
0168 C      TS=NOZZLE TOTAL TEMP. (DEG C), AND TI=TEMP. (DEG C) OF ITH TC.
0169 C
0170 0      WRITE(6,110)TIM(J),P(J),PS(J),TS(J),(TI(I,J),I=1,NTI)
0171 0110      FORMAT(1H0,F6.2,2F6.3,F6.1,9F5.1/1H ,F29.1,8F5.1)
0172 100      CONTINUE
0173 C
0174 C
0175 C      CONVERT TEMP. DATA TO DEG. K AND PRESS. DATA TO NEWTONS/M**2.
0176 C
0177          DO 120 J=1,NT
0178          P(J)=P(J)*101322.0

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0179      PS(J)=PS(J)+101322.0
0180      TS(J)=TS(J)+273.2
0181      DO 120 I=1,NTI
0182      120  TI(I,J)=TI(I,J)+273.2
0183      C
0184      C      CONVERT AN TO N=2, NOZZLE NOMINAL AREA
0185      C
0186      AN=AN*0.0001
0187      C
0188      C      ALTER TIME SERIES TO INCLUDE TO AND TP.
0189      C
0190      L=TO/DT
0191      L=L+1
0192      N=TP/DT
0193      N=N+1
0194      IF(N-L.GT.4)GO TO 140
0195      C
0196      C      IF (N-L) IS LESS OR EQUAL TO 4 PRINT OUT
0197      C      MESSAGE AND STOP PROGRAM
0198      C
0199      WRITE(IPAR(1),130)
0200      130  FORMAT(52HNOT ENOUGH FILLING DATA TO EVALUATE PRESSURANT FLOW)
0201      WRITE(IPAR(1),2000)NAME2
0202      STOP
0203      C
0204      140  CONTINUE
0205      DO 916 J=1,NT
0206      916  WRITE(6,917)TIN(J),P(J),PS(J),TS(J),(TI(I,J),I=1,NTI)
0207      917  FORMAT(1H0,F7.2,2F10.1,F7.1/1H ,13F7.1)
0208      C
0209      C      ADJUST TANK TEMPS. TO UNIFORM VALUE AT TIME TO.
0210      C      CALCULATE MEAN TEMPERATURE.
0211      C
0212      NTEF=NTI
0213      CNTI=NTEF
0214      TB(L)=0.0
0215      DO 160 I=1,NTI
0216      C
0217      TB(L)=TB(L)+TI(I,L)/CNTI
0218      160  CONTINUE
0219      DO 170 I=1,NTI
0220      TCR=TB(L)-TI(I,L)
0221      DO 170 J=1,NT
0222      170  TI(I,J)=TI(I,J)+TCR
0223      C
0224      C      GAS CONST. RG (JOULE/KGH-MOL/DEG K) AND CRIT. PRESS. RATIO RP
0225      C
0226      RG=8314.5
0227      RP=(2.0/(GA+1.0))*((GA/(GA-1.0)))
0228      C
0229      C      CALCULATE NOMINAL FLOW INTEGRAL ( ARRAY FLIN), MEAN TEMP. ( ARRAY TB),
0230      C      AND NO. HOLES IN TANK (ARRAY CH).
0231      C
0232      DO 190 J=1,NT
0233      PRAT=AN*PI(P(J)/PS(J))
0234      VEL=SQRT(2.0*GA*RG/UP*TS(J)/(GA-1.0)*((1.0-PRAT)*((GA-1.0)/GA)))
0235      DENS=PS(J)/RG/TS(J)*PRAT*((1.0/GA))
0236      FLIN(J)=AN*VEL*DENS
0237      TB(J)=0.0
0238      DO 180 I=1,NTI

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0239      TB(J)=TB(J)+TI(I,J)/CNTI
0240      180  CONTINUE
0241      C
0242      CN(J)=P(J)+VT/TB(J)/RG
0243      D      WRITE(6,919)J,PRAT,VEL,DENS,FLIN(J)
0244      D919  FORMAT(1H,15,4F15.4)
0245      190  CONTINUE
0246      IF(CF.NE.0.0)GO TO 240
0247      C
0248      C      CALCULATE FLOW DATA FROM NOMINAL MEAN TEMP. DATA (THAT IS, FROM
0249      C      MEAN TC. DATA) AS ESTIMATE OF MEAN TANK TEMP. (INPUT VALUE OF CF
0250      C      IS ZERO.) THIS IS BETWEEN TO AND TP.
0251      C      EVALUATE FLOW INTEGRAL FLINT.
0252      C
0253      FLINT=0.0
0254      N1=N-1
0255      DO 200 J=L,N1
0256      200  FLINT=FLINT+(FLIN(J)+FLIN(J+1))/2.0*(TIN(J+1)-TIN(J))
0257      CF=(CN(N)-CN(L))/FLINT
0258      D      WRITE(6,210)CF
0259      D210  FORMAT(4H0CF=F6.4,61H -INFERRED USING MEAN OF TC. DATA TO APPROX.
0260      D      1 MEAN TANK TEMP.)
0261      C
0262      C      DEVELOP CONSISTENT VALUES FOR MEAN TEMP. TB AND NO. MOLS. CN
0263      C      FOR NON-FILLING PERIODS.
0264      C
0265      DO 220 J=1,L
0266      CN(J)=CN(L)
0267      220  TB(J)=P(J)+VT/CN(J)/RG
0268      DO 230 J=N,NT
0269      TBJ=0.0
0270      DO 225 I=J,NTI
0271      TBJ=TBJ+TI(I,J)/CNTI
0272      225  CONTINUE
0273      CN(J)=CN(N)
0274      TB(J)=P(J)+VT/CN(J)/RG
0275      DO 228 I=1,NTI
0276      228  TI(I,J)=TI(I,J)+TB(J)-TBJ
0277      230  CONTINUE
0278      GO TO 260
0279      C
0280      C      INTEGRATE FLOW INTO TANK USING INPUT VALUE OF CF.
0281      C
0282      240  DO 250 J=1,NT
0283      IF(J.LT.L)CN(J)=CN(L)
0284      IF(J.GT.L.AND.J.LE.N)CN(J)=CN(J-1)+CF*(FLIN(J-1)+FLIN(J))/2.0*(TIN
0285      1(J)-TIN(J-1))
0286      IF(J.GT.N)CN(J)=CN(N)
0287      250  TB(J)=P(J)+VT/CN(J)/RG
0288      C
0289      C      INTEGRATION OF TAIR AND TPRS
0290      C
0291      260  CONTINUE
0292      D      WRITE(6,270)L,N
0293      D270  FORMAT(50H1SUMMARY OF CALCULATIONS THRU ARRAYS TAIR AND TPRS/3H J=
0294      D      112,2X6AND N=13/50H0 J   TIME   TAIR   TPRS   TSTAR   BETA   NPOAR
0295      D      2 BETA/TSTAR/)
0296      D280  FORMAT(1H,13,5F7.1,F8.3,E10.2)
0297      NTN1=NT-1
0298      DO 460 J=L,NTN1

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0299      T1=TB(L)
0300      TAIR(J)=T1
0301      TPRS(J)=TS(L)
0302      TSTAR=CH(L)/(CH(L+1)-CH(L))
0303      IF(J.GT.L.AND.TB(J).GT.T1)GO TO 420
0304      TB2=T1
0305      TA2=T1
0306      TS2=TS(J)
0307      P2=P(J)
0308      CN2=CH(J)
0309      GN1=GA-1.0
0310      DLTP=(TB(J+2)-T1)/(0.5*(TB(J+2)+T1))/ALOG(P(J+2)/P(L))
0311      CHU2=GN1*T1/(GA*(T1-TS(L))+GA*TS(L)-T1)
0312      BTA(J)=(1.00*GA*TS2-TB2-CN2+1.00*(TB(J+2)-T1)/(CH(J+2)-CH(L)))/
0313      1*(GN1+1.00+0.5*(TB(J+2)-T1))
0314      D      WRITE(6,410)J,DLTP,CHU2
0315      D410  FORMAT(3H0J=13,10X5HDLTP=F6.3,10X4HCHU=F6.3)
0316      GO TO 450
0317      420  TB1=TB2
0318      TS1=TS2
0319      P1=P2
0320      CN1=CN2
0321      TA1=TA2
0322      CHU1=CHU2
0323      TS2=TS(J)
0324      TB2=TB(J)
0325      P2=P(J)
0326      CN2=CH(J)
0327      TBB=0.5*(TB1+TB2)
0328      TSB=0.5*(TS1+TS2)
0329      PB=0.5*(P1+P2)
0330      CNB=0.5*(CN1+CN2)
0331      TAB=TA1
0332      CHUB=CHU1
0333      DP=P2-P1
0334      DN=CN2-CN1
0335      DTB=TB2-TB1
0336      FI=.FALSE.
0337      430  DTA=CH1/GA+TAB+DP/PB-CHUB/GA*((GA+TSB-TBB)/CNB+DN-DTB)
0338      TA2=TA1+DTA
0339      TAB=0.5*(TA1+TA2)
0340      CHU2=(TA2-T1)/(TB2-T1)
0341      CHUB=0.5*(CHU1+CHU2)
0342      IF(FI)GO TO 440
0343      FI=.TRUE.
0344      GO TO 430
0345      440  TAIR(J)=TA2
0346      IF(J.LE.N-2)TSTAR=CNB/DN+DT
0347      BTA(J)=(1.00*GA+TSB-TBB)*DN/CNB+DTB)/CH1/(TB2-T1)*TSTAR/DT
0348      TPRS(J)=(CN2+TB2-CH(L)+TA2)/(CN2-CH(L))
0349      TSAV=0.5*(TS2+TS(L))
0350      IF(TPRS(J).GE.TSAV)GO TO 445
0351      TPRS(J)=TSAV
0352      TAIR(J)=TSAV+CH2/CH(L)*(TB2-TSAV)
0353      445  CONTINUE
0354      D      WRITE(6,440)J,TB1,TS1,P1,CN1,TA1,CHU1,TB2,TS2,P2,CN2,TA2,CHU2,TBB,
0355      D      1TSB,PB,CNB,TAB,CHUB,DP,DTB,DN,DTA,DT,TSTAR,TAIR(J),TPRS(J),BTA(J),
0356      D      2TSAV
0357      D440  FORMAT(3H0J=13,10X17HTB,TB,P,CH,TA,CHU/
0358      D      15X1H1,2F0.1,F0.0,F0.4,F0.1,F0.4/

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0359 D 25X1H2,2F8.1,F8.0,F8.4,F8.1,F8.4/
0360 D 35X1H8,2F8.1,F8.0,F8.4,F8.1,F8.4/
0361 D 44H DP=F8.0,5X4HDTB=F8.1,5X3HON=F8.4,5X4HDTA=F8.1,5X3HDT=F8.3/
0362 D 57H TSTAR=F8.1,5X5HTAIR=F8.1,5X5HTPRS=F8.1,5X5HBETA=F8.1,5X5HTSAV=F
0363 D 68.1)
0364 450 XPB(J)=0.0
0365 IF(TAIR(J).NE.TPRS(J))XPB(J)=(TAIR(J)-TB(J))/(TAIR(J)
0366 1-TPRS(J))
0367 BTTS(J)=BTAC(J)/TSTAR
0368 D WRITE(6,280)J,TIN(J),TAIR(J),TPRS(J),TSTAR,BTAC(J),XPB(J),BTTS(J)
0369 460 CONTINUE
0370 C
0371 DO 926 J=1,NT
0372 D WRITE(6,925)TIN(J),TB(J),CH(J),(TI(I,J),I=1,NTI)
0373 925 FORMAT(1H0,F10.3,F10.2,F15.4/(1H ,7F10.2))
0374 926 CONTINUE
0375 C
0376 C CALCULATION AND DISPLAY OF PRESSURANT FRACTIONS
0377 C
0378 800 CALL CODE
0379 WRITE(IOBUF,802)(AC(I),I=1,10)
0380 802 FORMAT(36H1INFERRED PRESSURANT DISTRIBUTION - ,1044)
0381 CALL WRITE(IOBUF,IERR,IOBUF,38)
0382 IF(IERR.LT.0)CALL ERR(IPAR(1),IERR)
0383 CALL WRITE(IOBUF,IERR,CBUF1,32)
0384 IF(IERR.LT.0)CALL ERR(IPAR(1),IERR)
0385 CALL CODE
0386 WRITE(IOBUF,803)(I,I=1,13)
0387 803 FORMAT(28H (SEC) MEAN AIR PRESSURANT,20X9HMEAN I = 11,1216)
0388 CALL WRITE(IOBUF,IERR,IOBUF,65)
0389 IF(IERR.LT.0)CALL ERR(IPAR(1),IERR)
0390 C
0391 C CONSTRUCT A LINE OF BLANKS
0392 C
0393 DO 804 I=1,100
0394 804 IOBUF(I) = IBLANK
0395 C
0396 C
0397 806 FORMAT(1H ,F5.1,3F6.1,F8.1,F8.4,F12.3,F8.3,12F6.3)
0398 THE=0.0
0399 XPI=0.0
0400 TB(L)=TB(L)-273.2
0401 CALL WRITE(IOBUF,IERR,CBUF3,12)
0402 IF(IERR.LT.0)CALL ERR(IPAR(1),IERR)
0403 CALL CODE
0404 WRITE(IOBUF,806)THE,TB(L),TB(L),BTAC(L),BTTS(L),XPB(L),(XPI,I=1,13)
0405 CALL WRITE(IOBUF,IERR,IOBUF,66)
0406 IF(IERR.LT.0)CALL ERR(IPAR(1),IERR)
0407 C
0408 C NOTE!!!! THIS HAS TO BE CHANGED TO COINCIDE WITH WHAT IS AVAILABLE
0409 C IN SCANS AND WHAT CINST IS EXPECTING. THE KB=L+100 THE 100 HAS TO
0410 C BE CHANGED.
0411 C
0412 C
0413 KA=L+1
0414 KB=L+100
0415 C
0416 DO 850 K=KA,KB
0417 THE=TIN(K)-TIN(L)
0418 C

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0419      DO 830 I=1,13
0420      XP(I)=0.0
0421      IF(TAIR(K).NE.TB(K))XP(I)=1.D0*XPB(K)*(TAIR(K)-TI(I,K))/
0422      1(TAIR(K)-TB(K))
0423      830 CONTINUE
0424      TB(K)=TB(K)-273.2
0425      TAIR(K)=TAIR(K)-273.2
0426      TPRS(K)=TPRS(K)-273.2
0427      IF(K.NE.L+2)GO TO 831
0428      CALL WRITE(0BUF,IERR,CBUF4,9)
0429      IF(IERR.LT.0) CALL ERR(IPAR(1),IERR)
0430      831 IF(K.NE.M-2)GO TO 832
0431      CALL WRITE(0BUF,IERR,CBUF5,12)
0432      IF(IERR.LT.0)CALL ERR(IPAR(1),IERR)
0433      832 IF(K.NE.N)GO TO 833
0434      CALL WRITE(0BUF,IERR,CBUF6,10)
0435      IF(IERR.LT.0)CALL ERR(IPAR(1),IERR)
0436      833 CALL CODE
0437      WRITE(10BUF,606)TME,TB(K),TAIR(K),TPRS(K),MTAK(K),MTTS(K),XPB(K),
0438      1(XP(I),I=1,13)
0439      CALL WRITE(0BUF,IERR,10BUF,66)
0440      850 IF(IERR.LT.0)CALL ERR(IPAR(1),IERR)
0441      C
0442      CC CALL WRITE(0BUF,IERR,CBUF2,61)
0443      CC IF(IERR.LT.0) CALL ERR(IPAR(1),IERR)
0444      C
0445      C RETURN TO BEGINNING OF PROGRAM
0446      C
0447      GO TO 10
0448      C
0449      C CONSTRUCT LINE OF BLANKS
0450      C
0451      9090 DO 9091 I=1,100
0452      9091 10BUF(I)=1BLANK
0453      C
0454      C CHECK FOR EOF MARKER
0455      C
0456      CALL WRITE(0BUF,IERR,XES,2)
0457      IF(IERR.LT.0)CALL ERR(IPAR(1),IERR)
0458      C
0459      DO 9092 I=1,4
0460      CALL WRITE(0BUF,IERR,10BUF,100)
0461      9092 IF(IERR.LT.0)CALL ERR(IPAR(1),IERR)
0462      C
0463      C DETERMINE THE ACTUAL LOCATION OF THE RECORD POINTS
0464      C
0465      CALL LOCF(0BUF,IERR,IDUM,IRB,IDUM,ISEC)
0466      IF(IERR.LT.0)CALL ERR(IPAR(1),IERR)
0467      ITRUN = ISEC/2 - (IRB - 1)
0468      C
0469      C CLOSE THE DISK FILE
0470      C
0471      CALL CLOSE(0BUF,IERR,ITRUN)
0472      IF(IERR.LT.0)CALL ERR(IPAR(1),IERR)
0473      C
0474      C PRINT ENDING MESSAGE
0475      C
0476      WRITE(IPAR(1),2000)NAME2
0477      STOP
0478      END

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0479 C
0480 C*****
0481 C SUBROUTINE TO PRINT OUT FMP ERRORS AS THEY OCCUR
0482 C FMP ERROR DESCRIPTIONS ARE LOCATED IN 'RTE 48
0483 C PROGRAMMERS' RET SPOOLING MANUAL'
0484 C
0485 C      SUBROUTINE ERR(LU,IERR)
0486 C      INTEGER LU,IERR
0487 C      WRITE(LU,10)IERR
0488 C      10 FORMAT(' IERR = ',I6)
0489 C      STOP
0490 C      END
0491 C*****
0492 C      ENDS
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